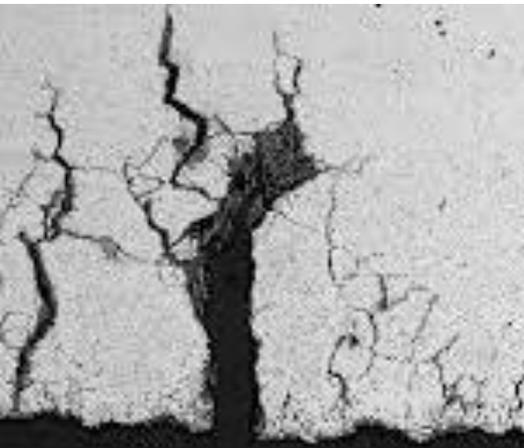


PASSIVE FILM EVOLUTION OVER 2.5 YEARS OF LEAN-DUPLEX STAINLESS STEEL REINFORCEMENTS EMBEDDED IN MORTAR CONTAINING CHLORIDES

1st Corrosion and Materials Degradation Web Conference

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DEPARTMENT OF CHEMICAL, BIOMOLECULAR AND CORROSION
ENGINEERING



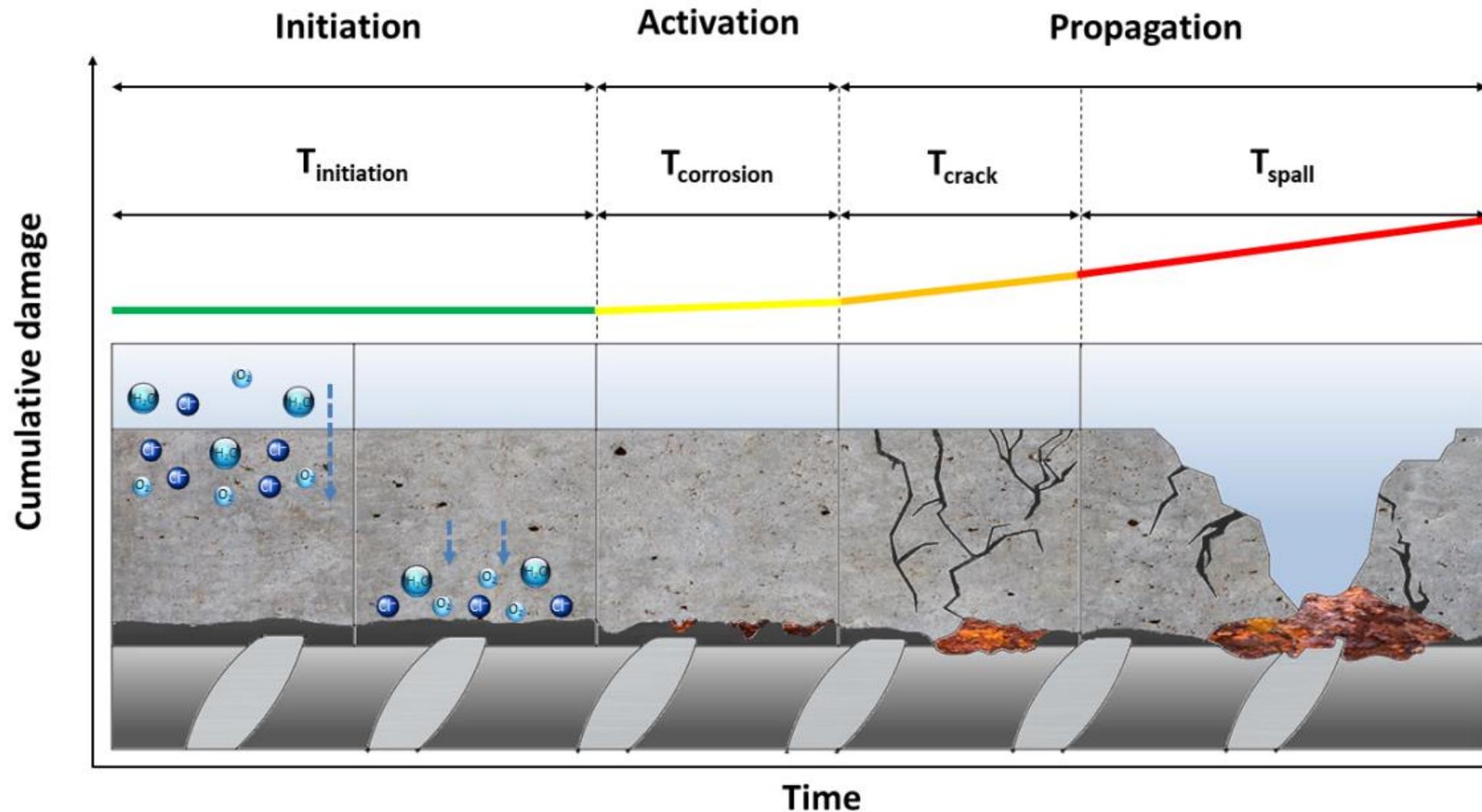
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- **Passive film of Stainless Steels**
- **Materials and Techniques**
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Introduction to Corrosion of Reinforced Concrete Structures

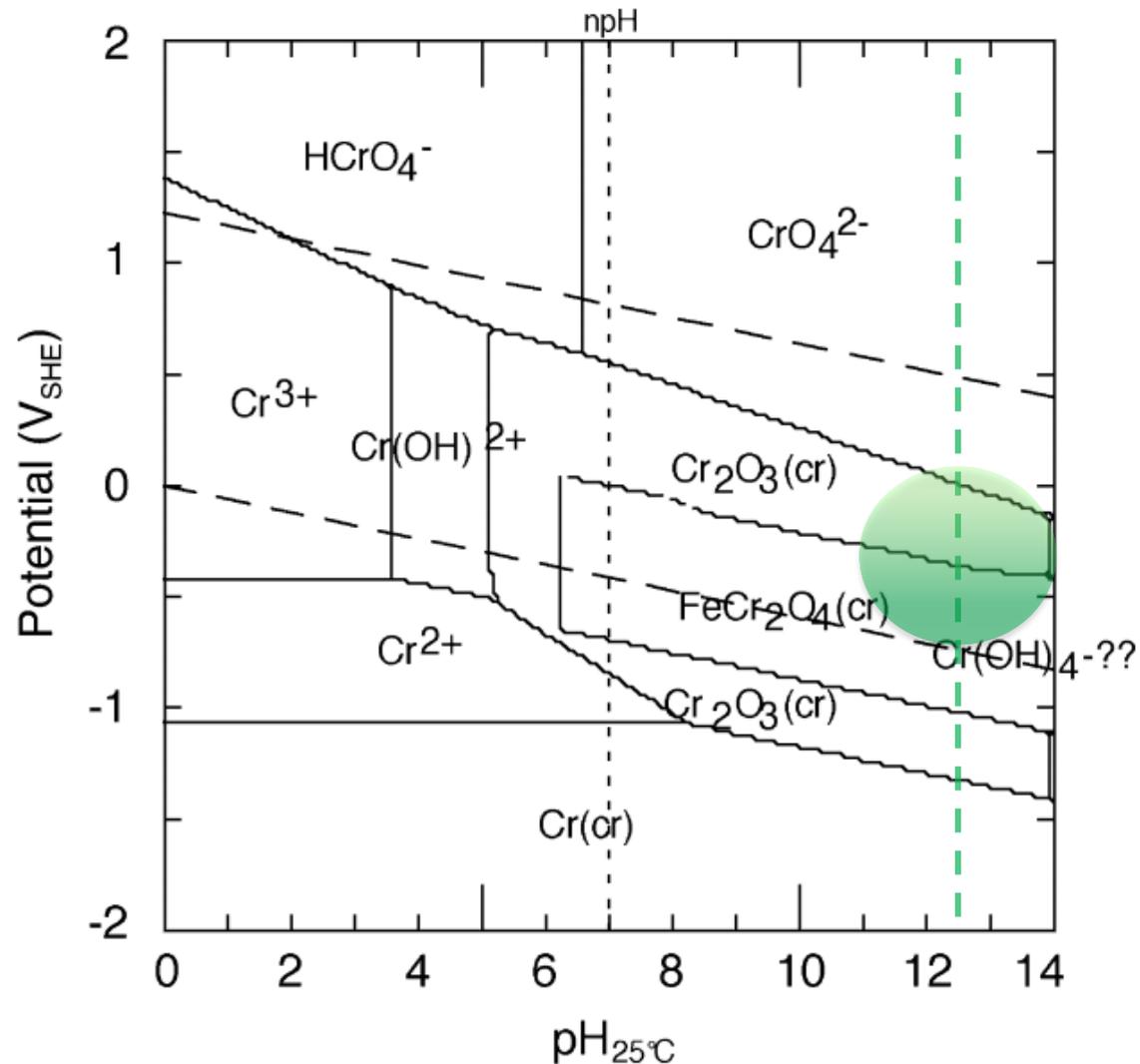


- Stages for the corrosion of RCS:

- **Initiation** → Ingress of chlorides, carbonation,...
- **Activation** → First dissolution of the passive film, pit nucleation
- **Propagation** → Pit growth, cracking of concrete cover, spallation

Tuutti model for the corrosion of RCS

Passive film of Stainless Steels

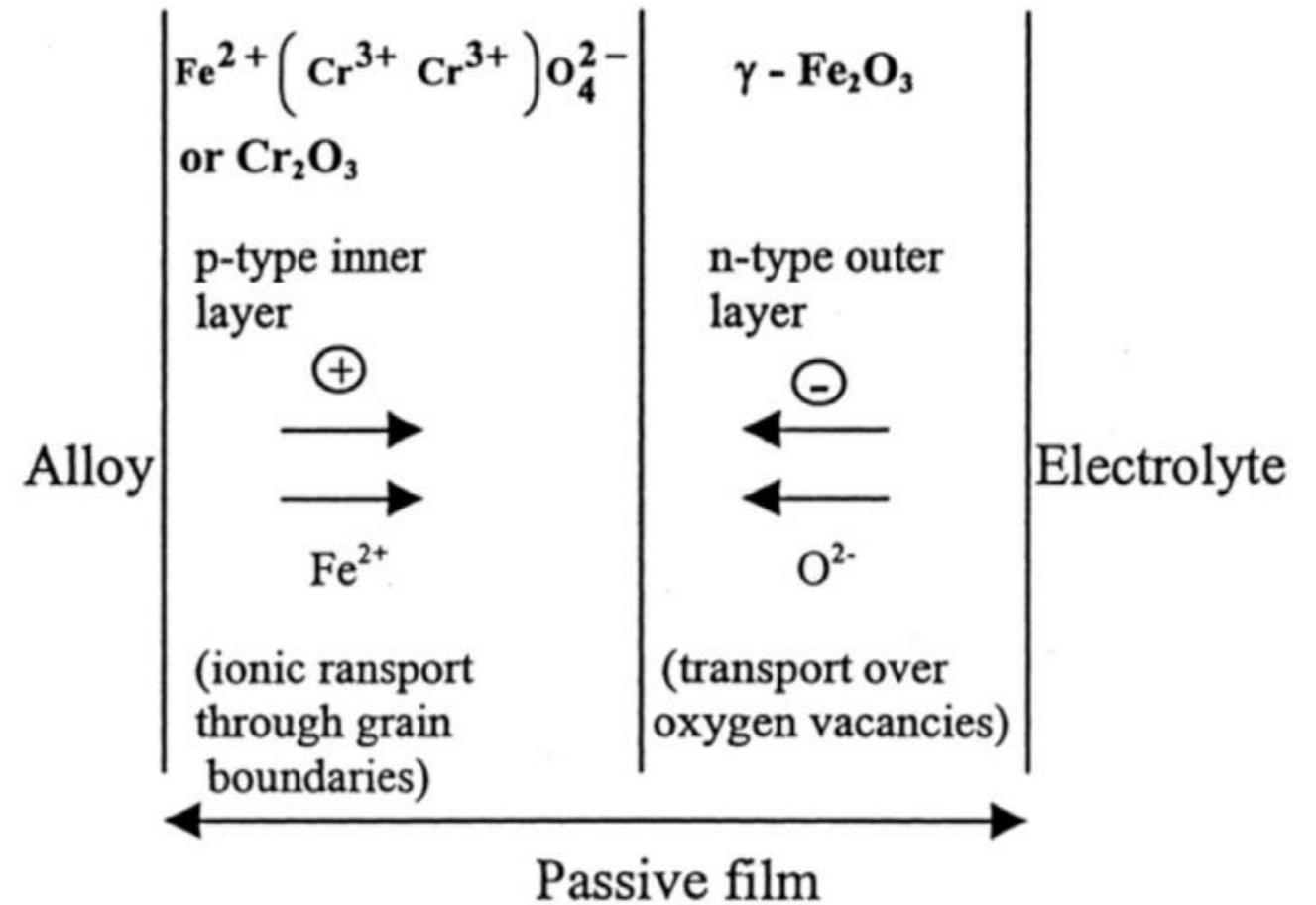
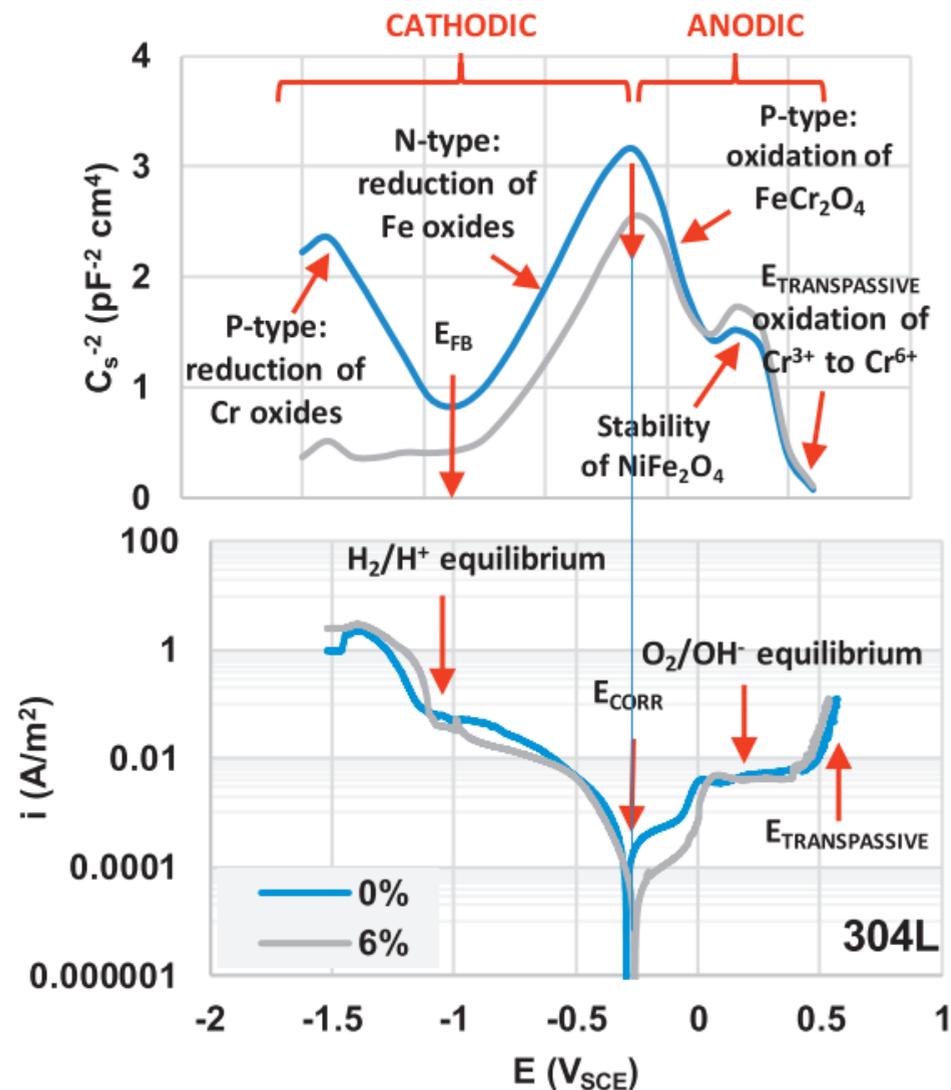


Pourbaix diagrams for chromium species in the ternary system of Fe-Cr-Ni at 25 °C from Puigdomenech et al.

Concrete has a **12.6 pH**

- Formation of **$Cr_2O_3 + FeCr_2O_4$** **p-type** semiconductors, reducing the defects inside the passive film as electrons flow from the solution to the film

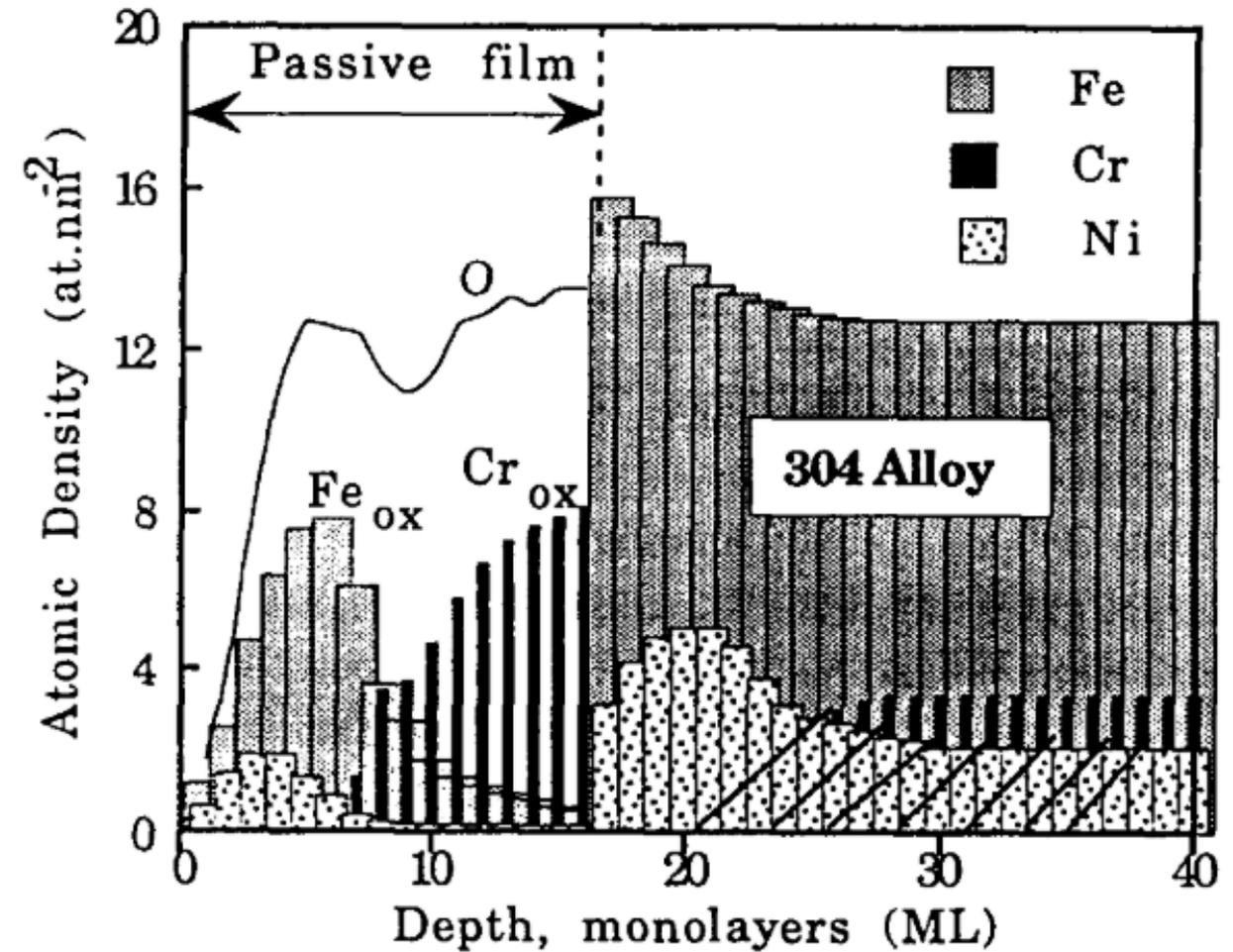
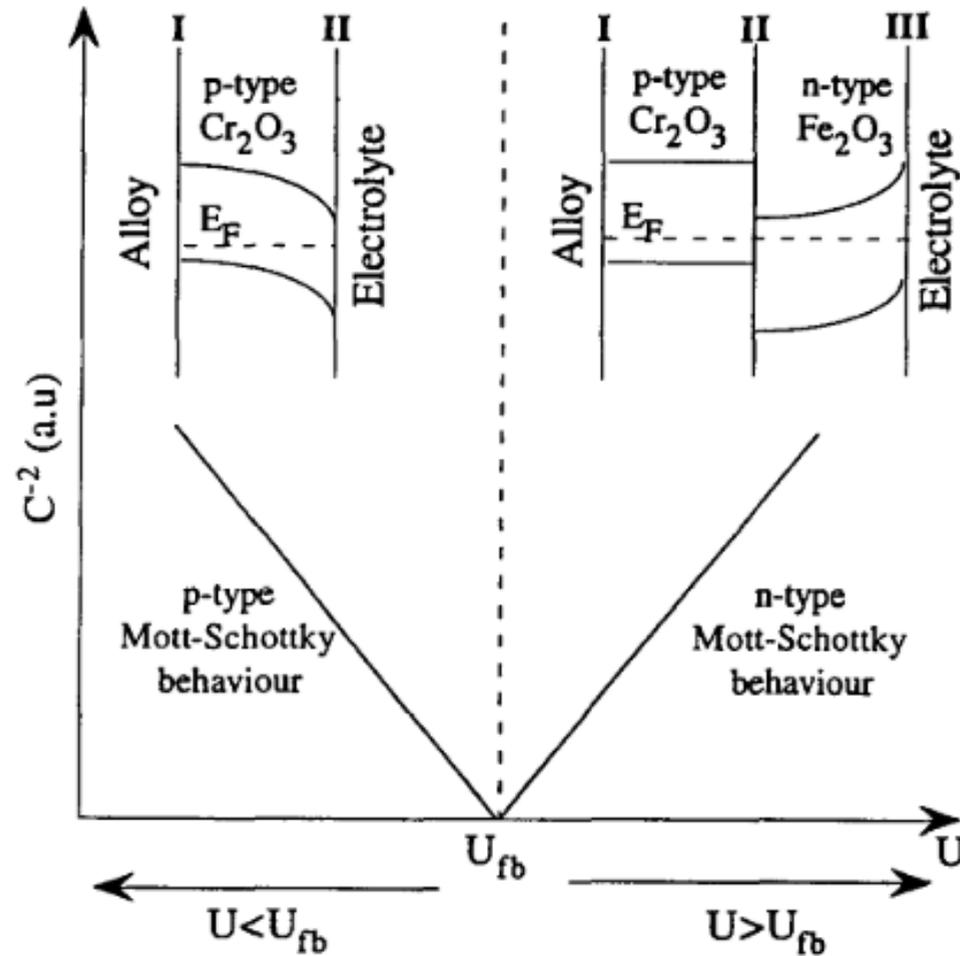
Passive film of Stainless Steels



Ogunsanya, I.G.; Hansson, C.M. The semiconductor properties of passive films and corrosion behavior of stainless steel reinforcing bars in simulated concrete pore solution. *Materialia* **2019**, *6*, 100321, doi:10.1016/j.mtla.2019.100321.

Hakiki, N.E.; Montemor, M.F.; Ferreira, M.G.S.; Da Cunha Belo, M. Semiconducting properties of thermally grown oxide films on AISI 304 stainless steel. *Corros. Sci.* **2000**, *42*, 687–702, doi:10.1016/S0010-938X(99)00082-7.

Passive film of Stainless Steels



Hakiki, N.B.; Boudin, S.; Rondot, B.; Da Cunha Belo, M. The electronic structure of passive films formed on stainless steels. *Corros. Sci.* **1995**, *37*, 1809–1822, doi:10.1016/0010-938X(95)00084-W.

Materials and Techniques

Materials

Sample	C	Si	Mn	P	S	Cr	Ni	Cu	N	Mo
LDSS 2001	0.028	0.65	4.19	0.023	0.010	20.07	1.78	0.08	0.129	0.22
LDSS 2304	0.019	0.35	0.81	0.029	0.010	22.75	4.32	0.31	0.138	0.29
AISI 304	0.023	0.28	1.41	0.034	0.023	18.07	7.93	0.33	0.050	0.22

Ordinary Portland Cement (OPC) with 0, 0.2, 2 and 4 wt.% Cl⁻

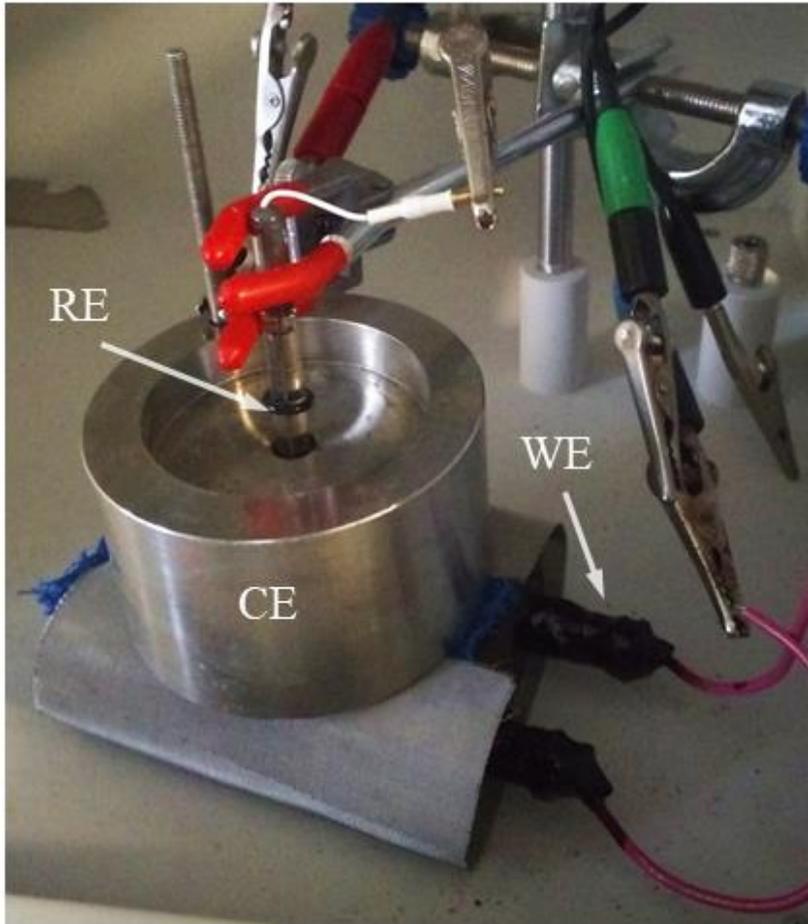
Electrochemical setting

LPR, EIS, CPP, Mott-Schottky

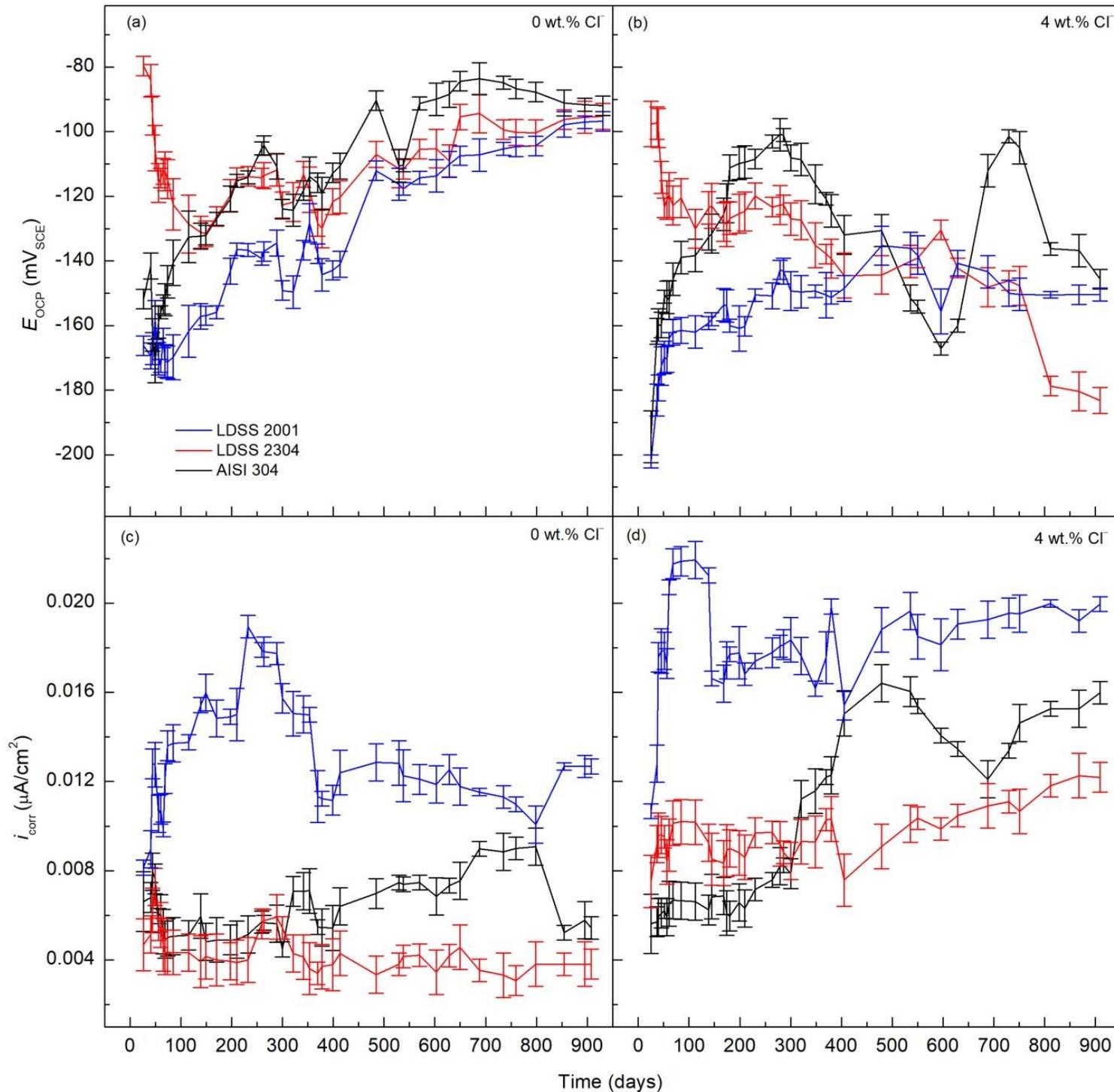
Equipment: Potentiostat/galvanostat Gamry Reference 600. Three-electrode configuration cell setup. Saturated calomel electrode (SCE) as RE, and stainless steel mesh plus guard ring as CE.

Electrochemical standards: ASTM G-1-03, ASTM G61-86 and ASTM G3-14

Martin, U.; Bosch, J.; Ress, J.; Bastidas, D.M. Long-term stability and electronic properties of passive film of lean-duplex stainless steel reinforcements in chloride containing mortar. *Constr. Build. Mater.* **2021**, *291*, 123319, doi:10.1016/j.conbuildmat.2021.123319



Results and Discussion



E_{corr} and i_{corr} monitoring over 912 days.

All SS reinforcements **improve** their E_{corr} **over time**, increasing the potential towards more positive values, as the **passive film is growing**.

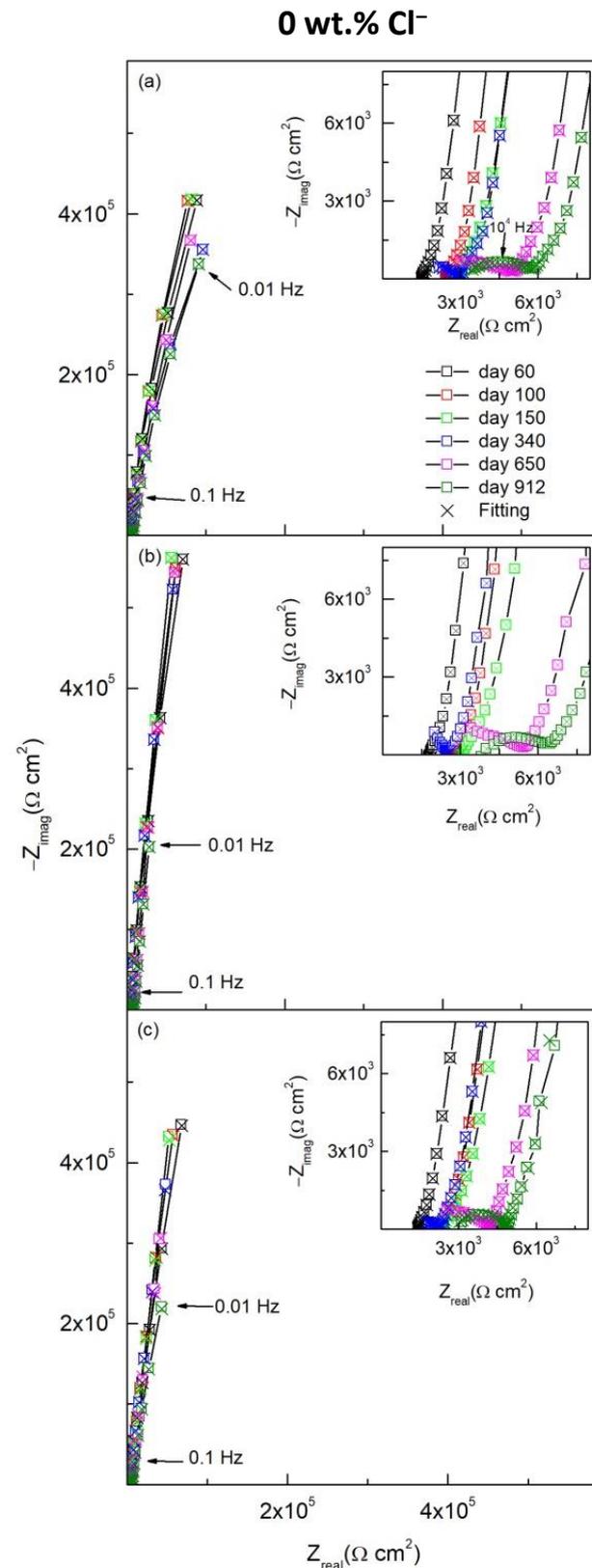
Similarly, the i_{corr} **decreases or stabilizes** and **does not** considerably **change** over the entire testing.

Results and Discussion

Nyquist plot of all SS reinforcements for **0** and **4 wt.% Cl⁻**.

The **0 wt.% Cl⁻** does not change the shape regardless of the time of exposure, only some minor decrease in impedance

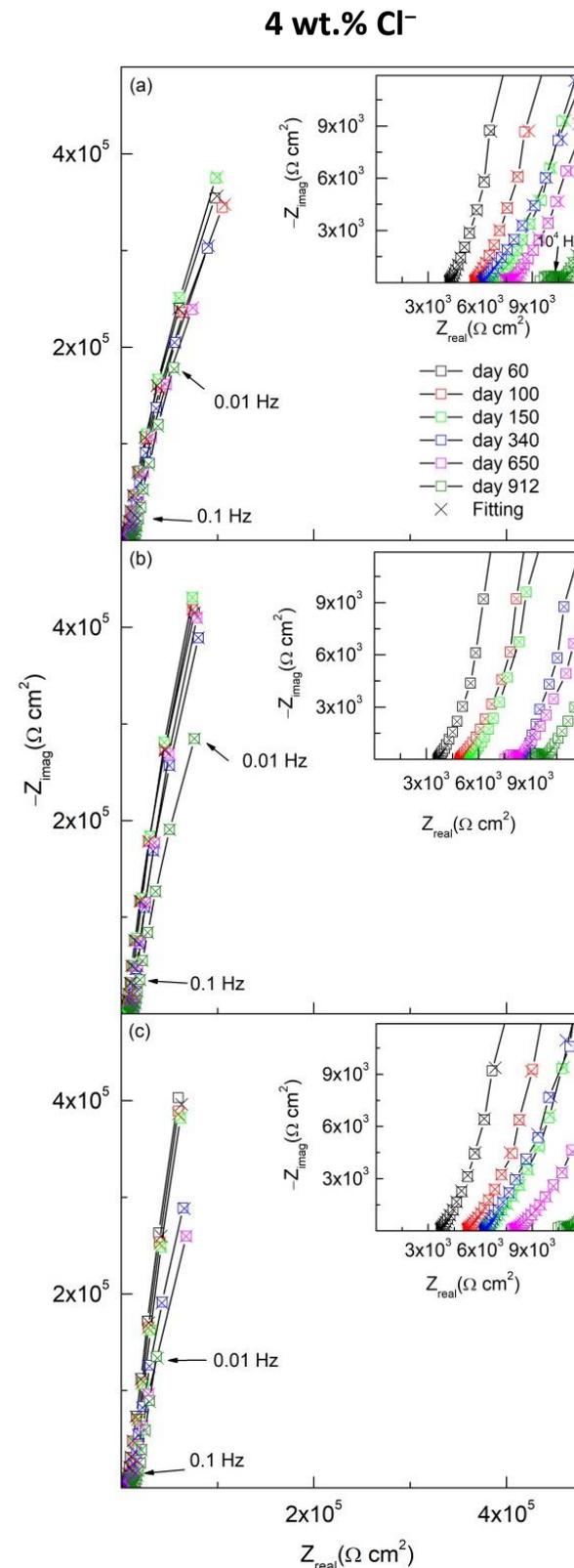
The **4 wt.% Cl⁻** experiences some small decrease in the impedance with time. However, the impedance values remain in the same order of as the **0 wt.% Cl⁻**.



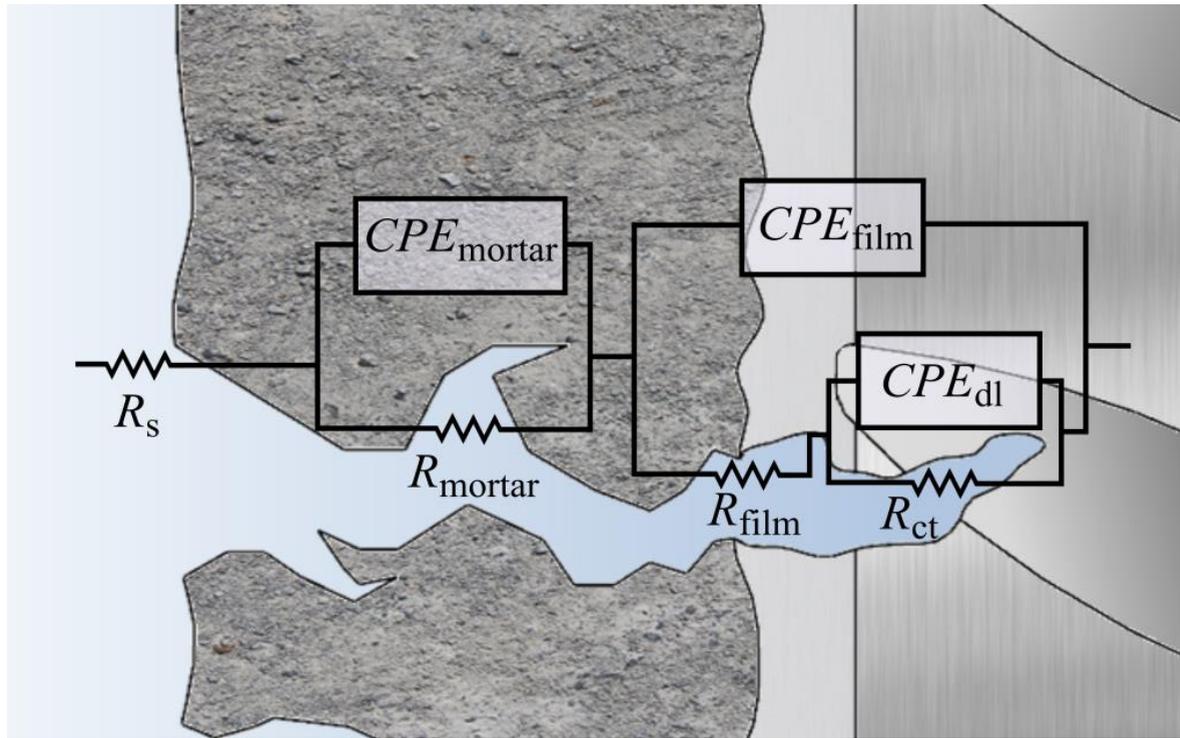
LDSS 2001

LDSS 2304

AISI 304



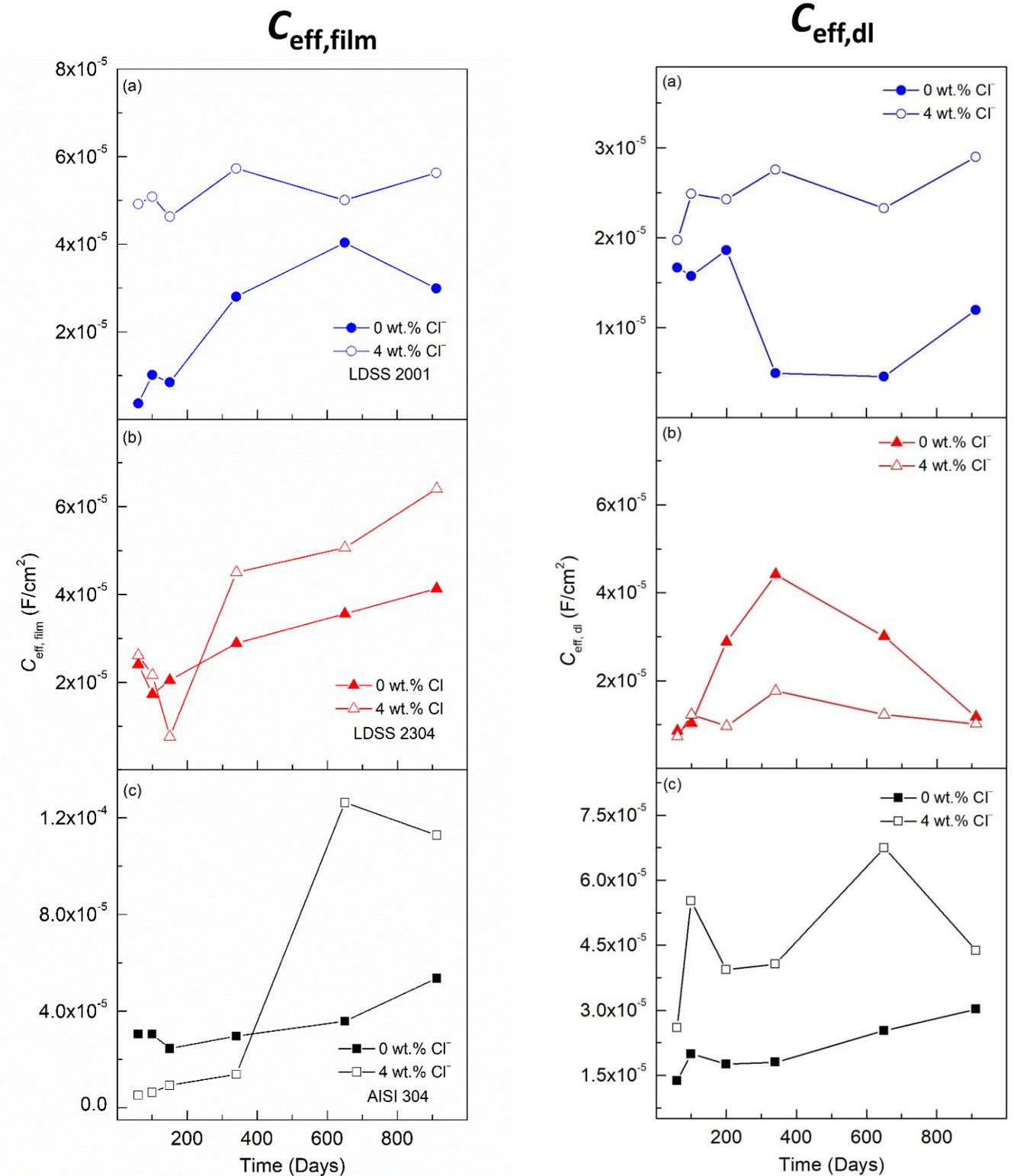
Results and Discussion



Electric equivalent circuit (EEC) with **three times constants** and effective capacitance of the film ($C_{\text{eff,film}}$) and double layer ($C_{\text{eff,dl}}$).

$$C_{\text{eff,film}} = Y_{\text{film}} (\omega_m)''^{n_{\text{film}}-1}$$

$$C_{\text{eff,dl}} = \left[Y_{\text{dl}} \left(\frac{1}{R_s} + \frac{1}{R_{\text{ct}}} \right) (n_{\text{dl}}-1) \right]^{\frac{1}{n_{\text{dl}}}}$$



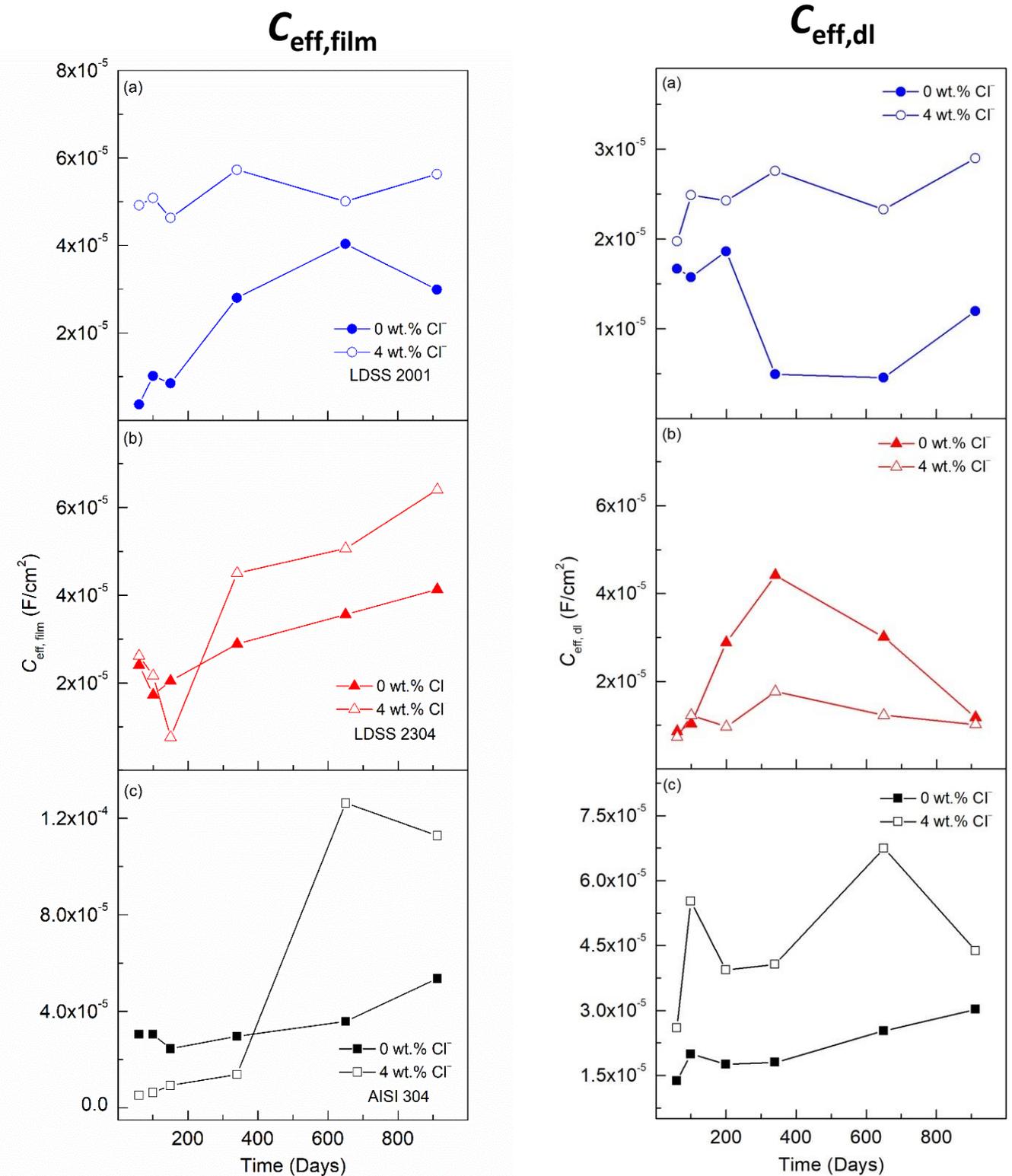
Results and Discussion

Thickness of the electrochemical double layer (d , nm)

Day	LDSS 2001		LDSS 2304		AISI 304	
	0 wt.% Cl ⁻	4 wt.% Cl ⁻	0 wt.% Cl ⁻	4 wt.% Cl ⁻	0 wt.% Cl ⁻	4 wt.% Cl ⁻
60	0.83	0.70	1.60	1.88	1.00	0.53
100	0.88	0.55	1.33	1.12	0.69	0.25
150	0.74	0.57	0.48	1.43	0.78	0.35
340	2.81	0.50	0.31	0.78	0.76	0.34
650	3.05	0.59	0.46	1.13	0.55	0.20
912	1.15	0.48	1.18	1.35	0.46	0.32

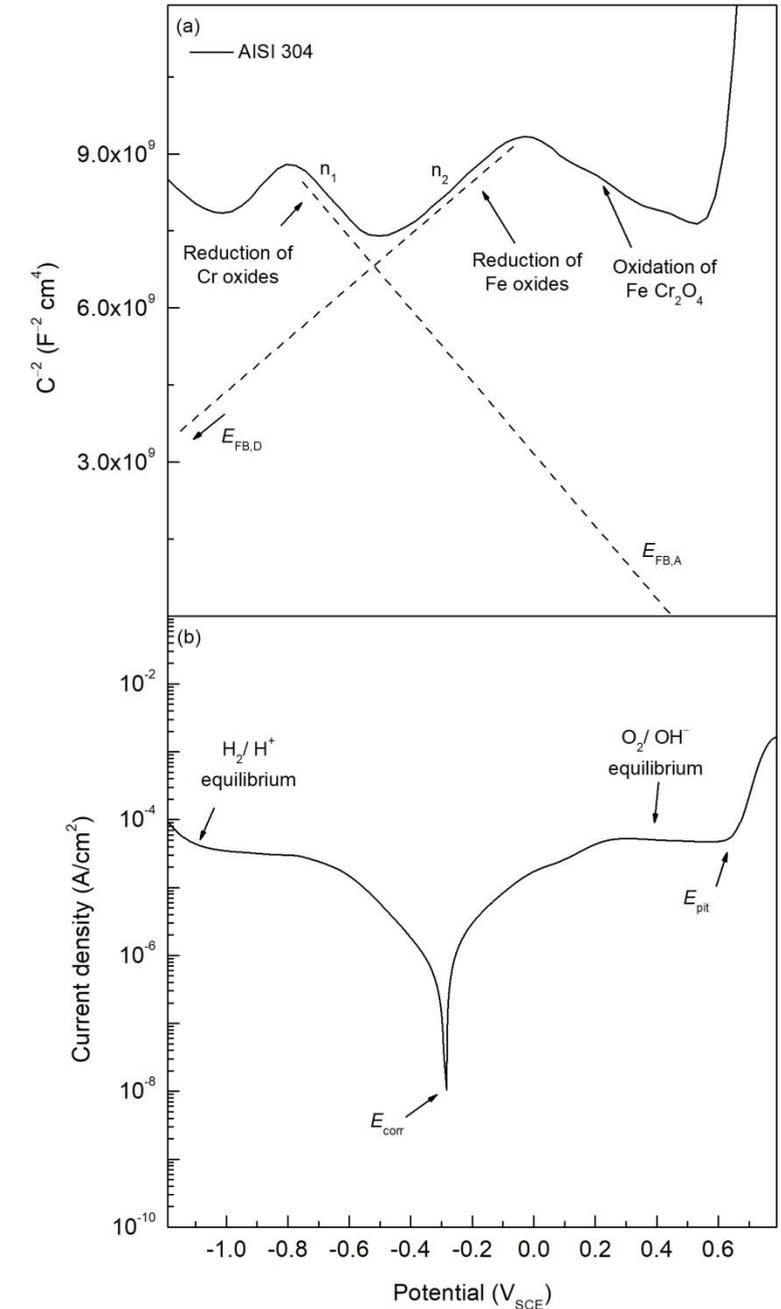
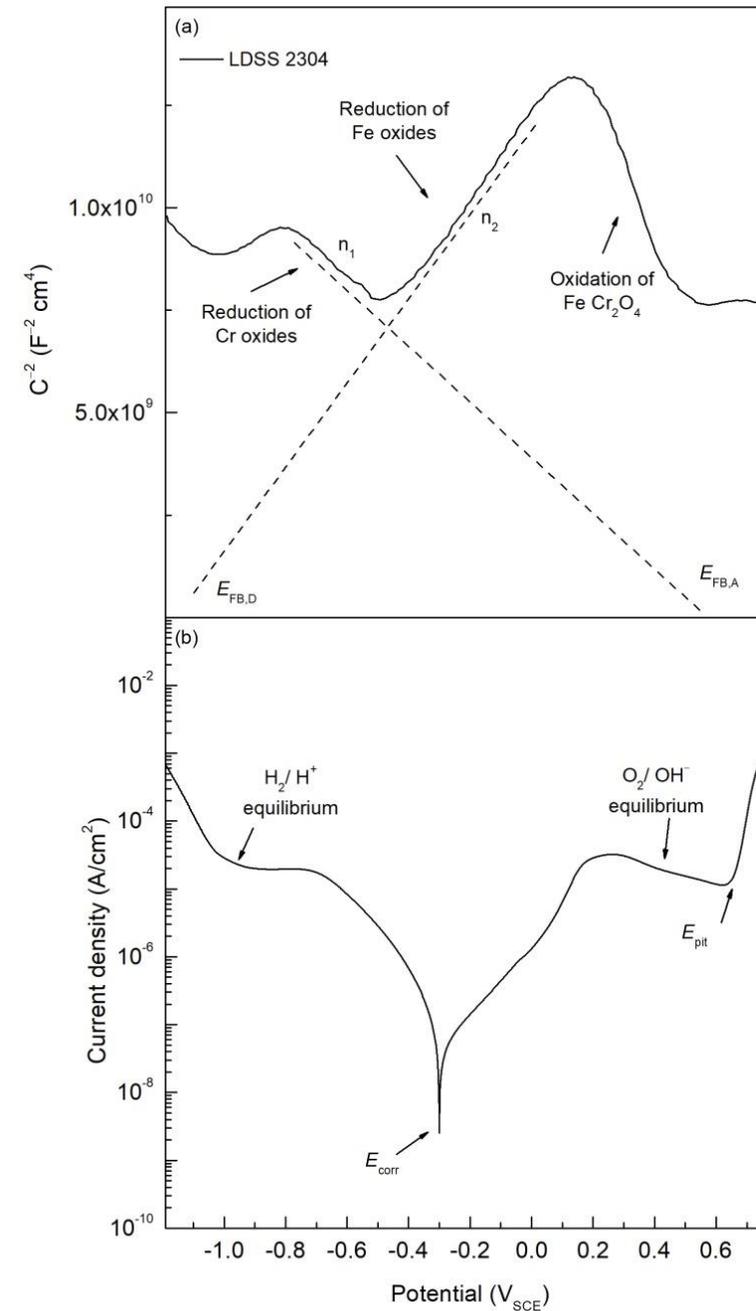
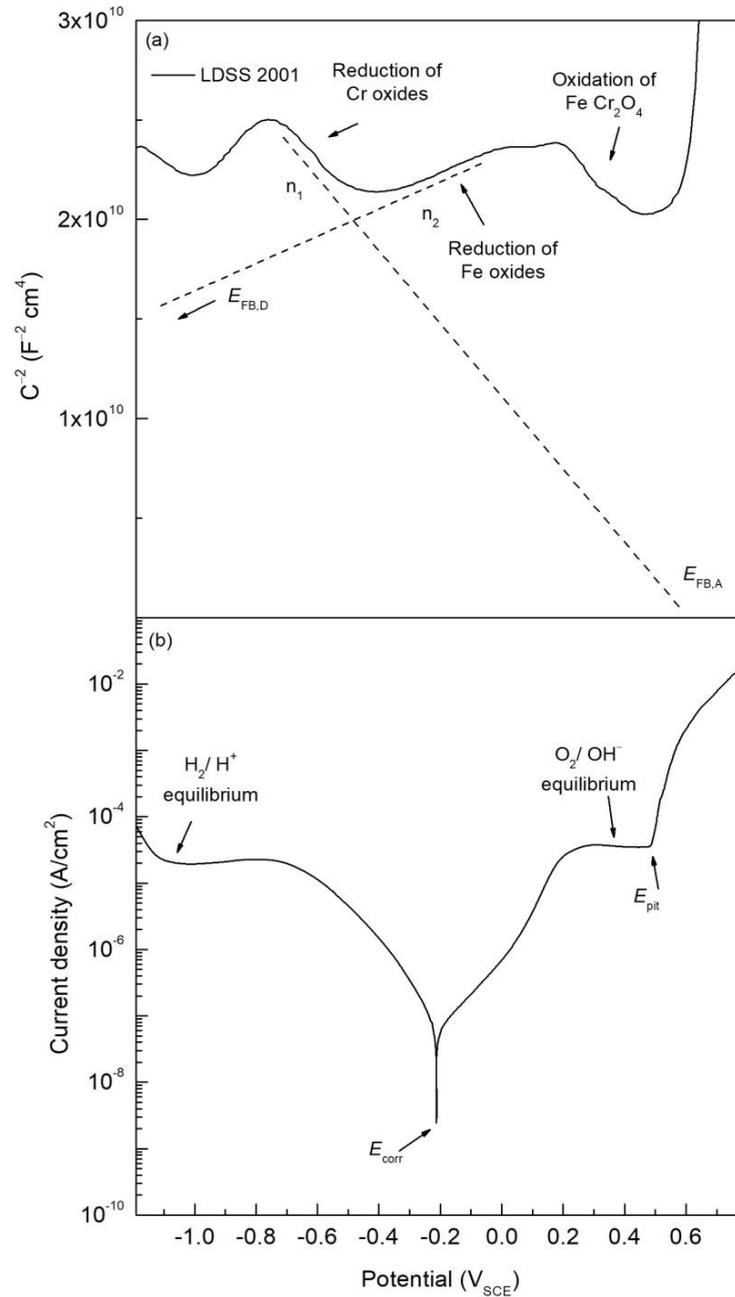
Thickness of the **double layer** based on the fitting parameters.

$$C_{\text{eff,dl}} = \frac{\epsilon_0 \epsilon_{\text{film}} A}{d}$$



Results and Discussion

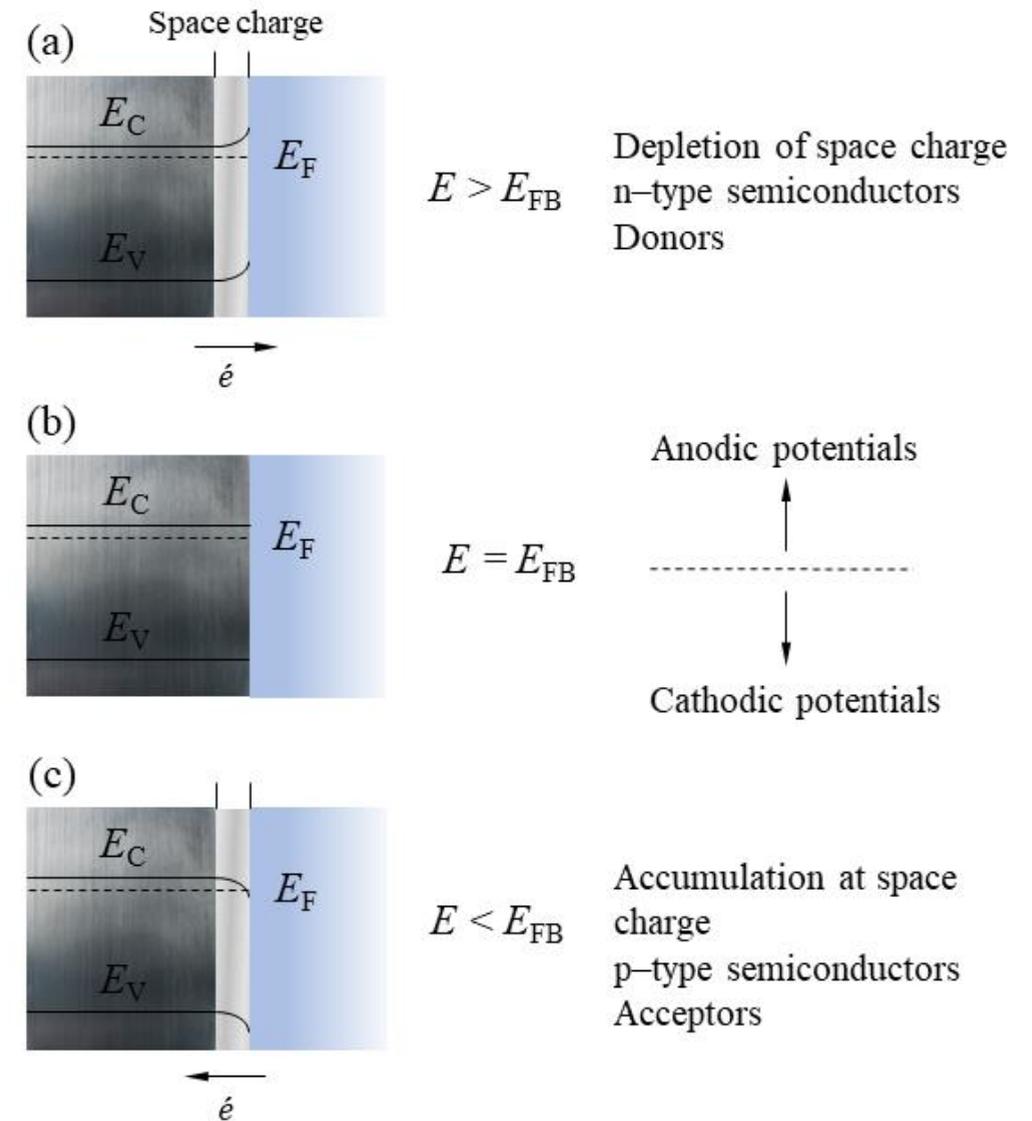
Mott-Schottky and CPP plots of OPC with 4 wt.% Cl⁻ after 912 days for all SS reinforcements.



Results and Discussion

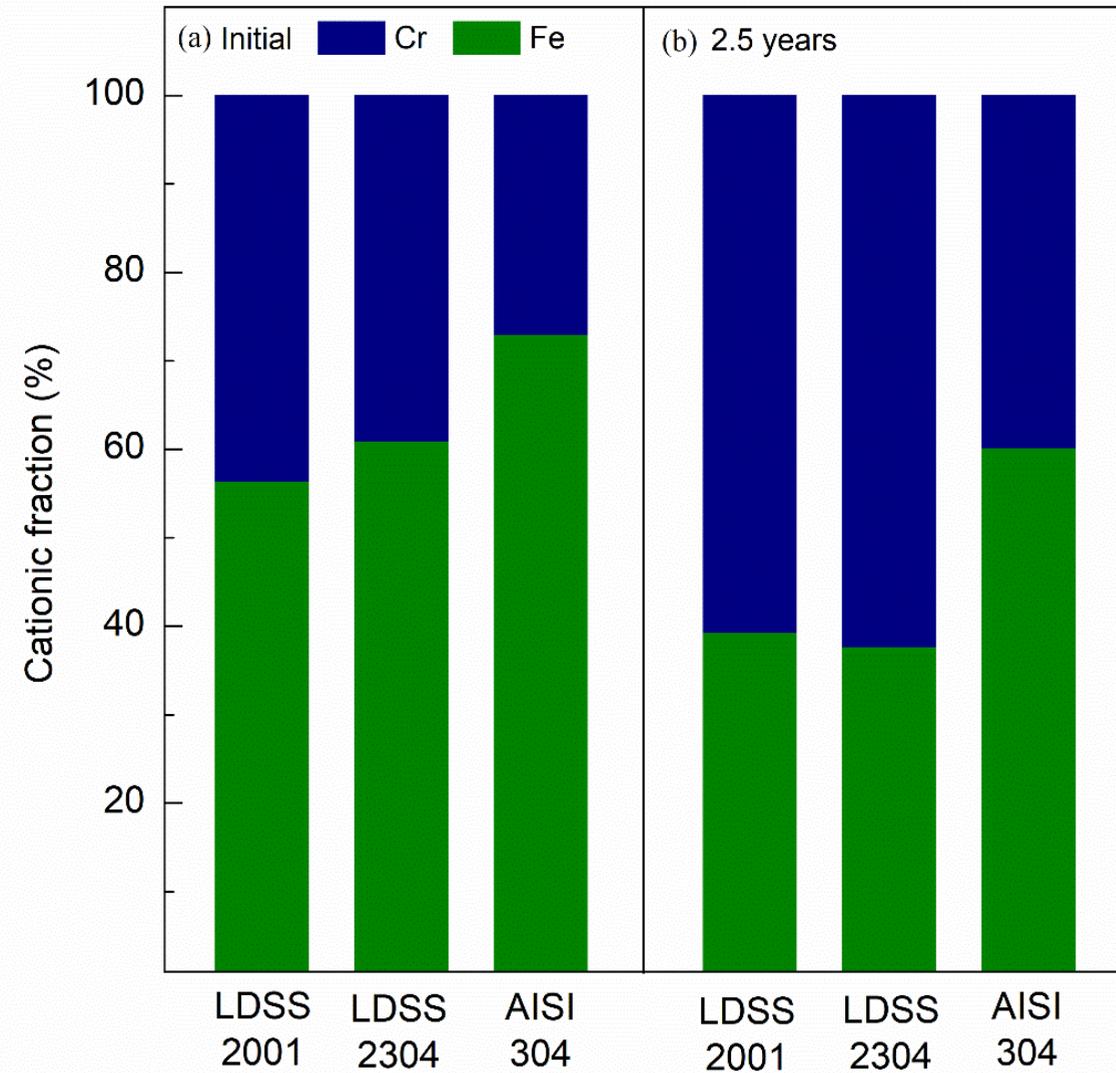
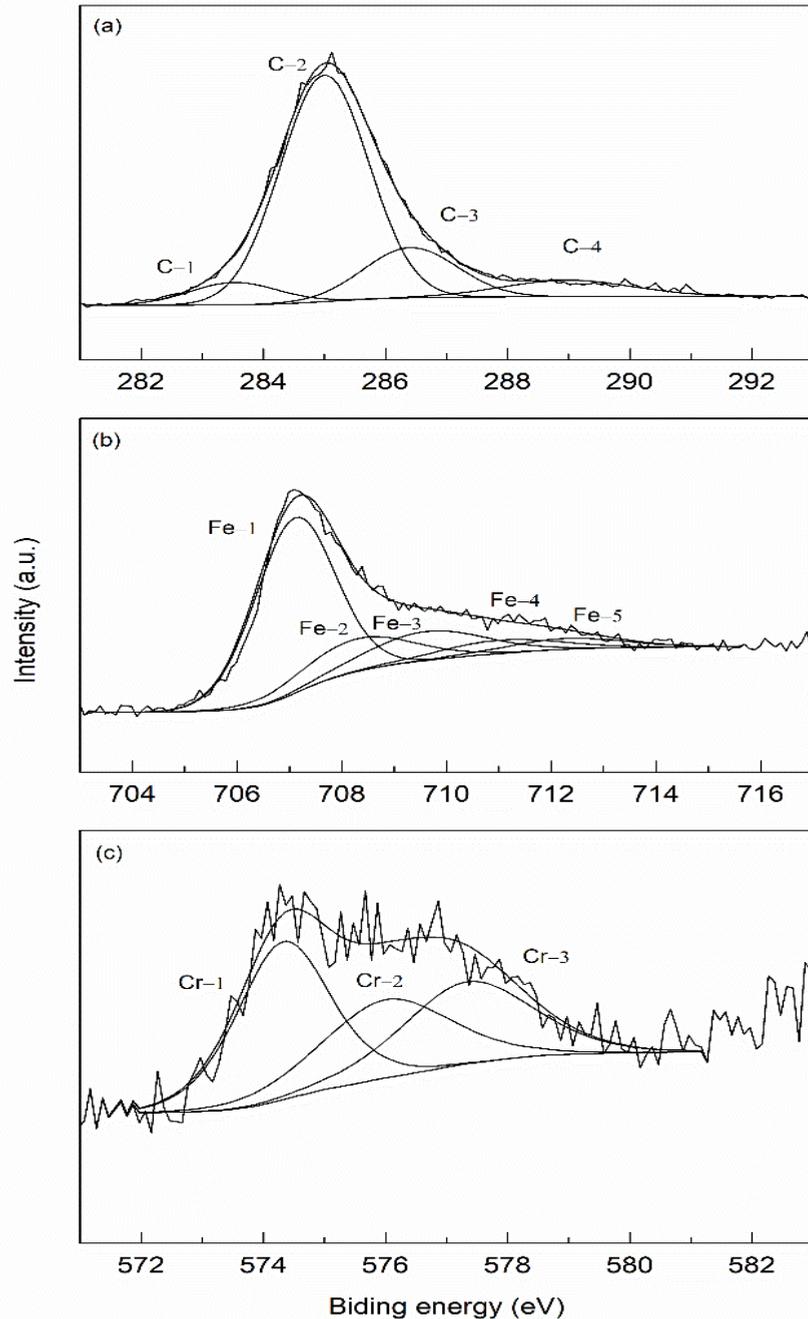
Mott-Schottky results of OPC with 4 wt.% Cl⁻ after 912 days c.

	Cl ⁻ wt. %	$E_{FB,A}$ V_{SCE}	$E_{FB,D}$ V_{SCE}	N_A cm^{-3}	N_D cm^{-3}
	0	-0.51	-0.18	1.50×10^{15}	4.52×10^{15}
LDSS	0.4	-0.10	-0.22	9.05×10^{15}	1.13×10^{17}
2001	2	0.07	-0.42	1.29×10^{18}	1.29×10^{19}
	4	0.86	-3.61	1.51×10^{18}	2.26×10^{19}
	0	-0.31	-0.53	4.51×10^{16}	9.05×10^{16}
LDSS	0.4	-0.11	-0.50	4.52×10^{17}	1.13×10^{18}
2304	2	0.25	-1.20	1.50×10^{19}	1.51×10^{19}
	4	0.45	-1.17	9.05×10^{19}	2.26×10^{19}
	0	-0.32	-0.25	4.52×10^{15}	1.29×10^{16}
AISI	0.4	-0.19	-0.36	2.26×10^{17}	3.01×10^{17}
304	2	0.52	-0.42	4.52×10^{18}	3.02×10^{18}
	4	0.62	-1.81	1.13×10^{19}	1.01×10^{19}



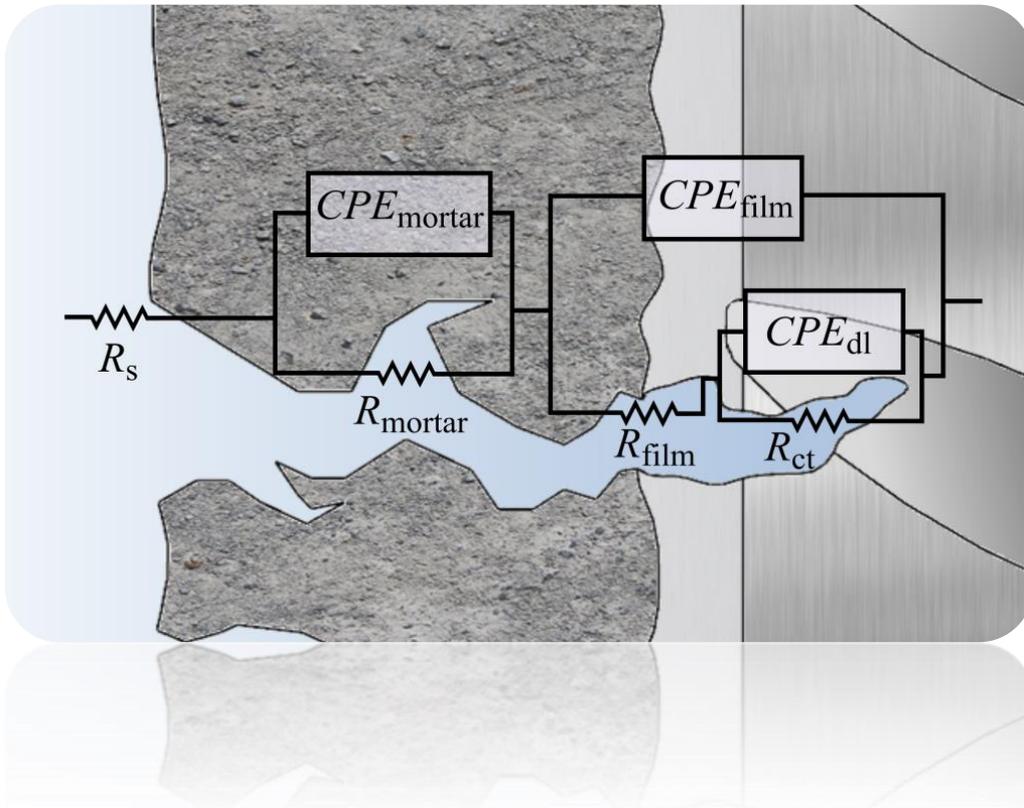
Results and Discussion

XPS and cationic fraction section for all SS reinforcements.

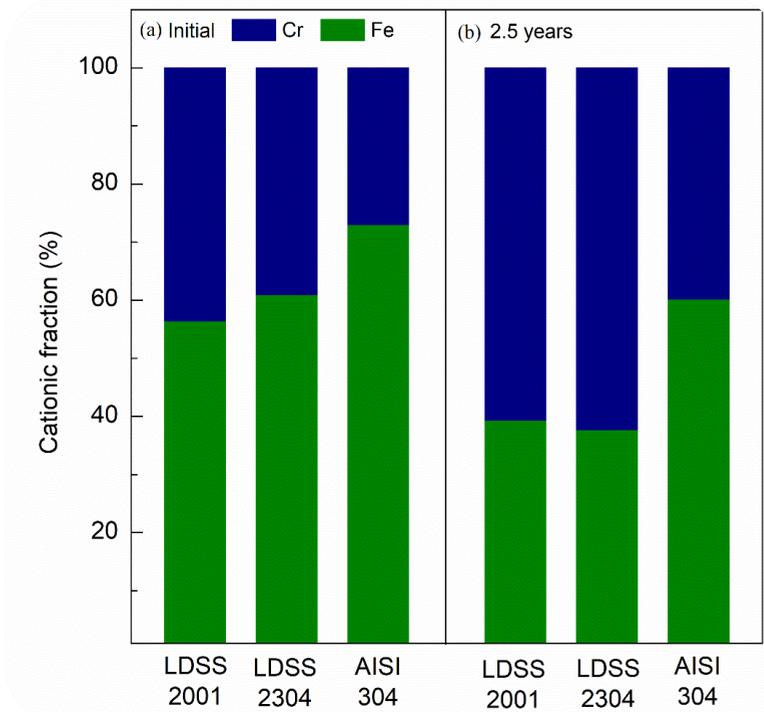


Conclusions

- The i_{corr} values of all SS reinforcements were far **below** the corrosion **limit** threshold of $0.1 \mu\text{A}/\text{cm}^2$. Proving the **outstanding corrosion performance** of LDSS 2001 despite **having the smallest Ni content**
- The **impedance** for all SS reinforcements remained **above $100 \text{ k}\Omega \text{ cm}^2$** during the **912 days**, hence **no passivity breakdown** was shown.



- **After 912 days** both LDSS, 2304 and 2001, had **Cr enrichment in their passive film**, from 40 to 63% and from 44 to 61% cationic fraction respectively.
- The $E_{\text{FB,D}}$ of LDSS 2001 rapidly **shifts towards negative potentials**, **generating** more **oxygen vacancies** and worsening the corrosion properties, as the **Cl^- concentration increases**.



**Thank you for
your time!!**