



 POLITECNICO DI MILANO



Towards the development of a MEMS-based health monitoring system for lightweight structures

Francesco Caimmi, Matteo Bruggi, Stefano Mariani

Politecnico di Milano

Paolo Bendiscioli

STMicroelectronics



MEMS accelerometers for structural health monitoring (SHM): why?

PROS

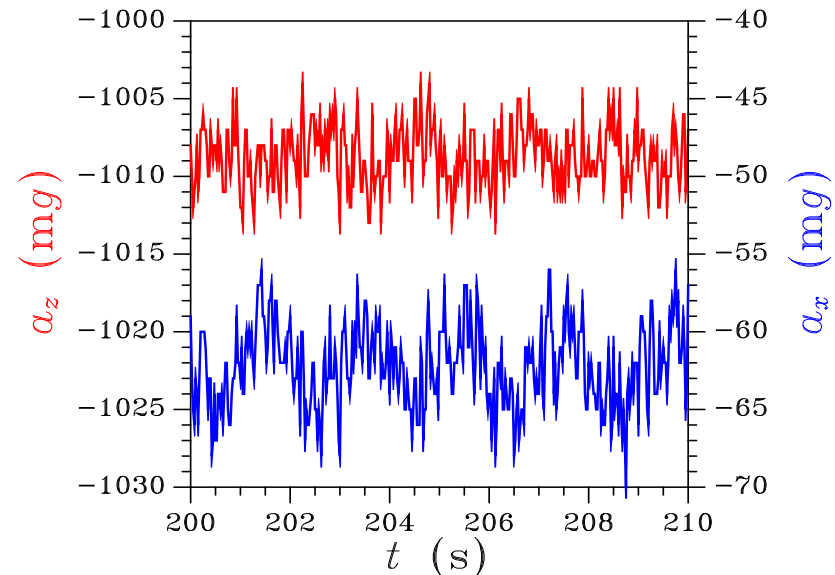


- lightweight (0.2 g) → no impact on dynamics
 - low power consumption
 - cheap (0.50\$ each!) → deploy in large numbers
- use redundancy to increase the quality of information

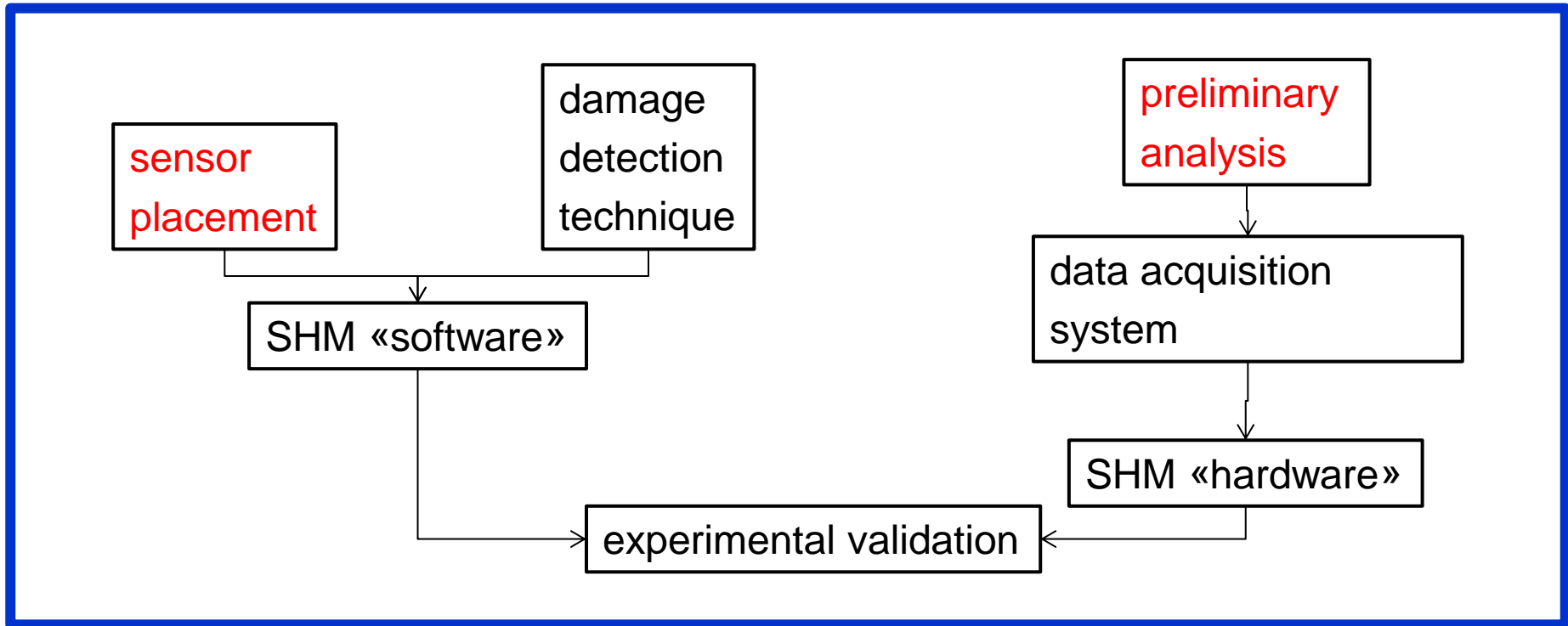
CONS



- noisy signals, low precision



Aim: a **SHM system** using MEMS



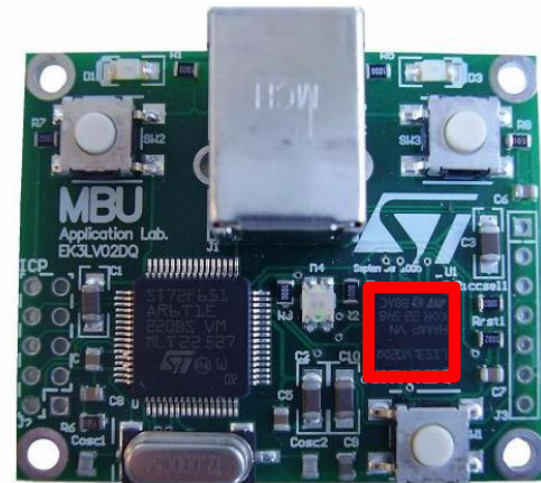
Focus of the presentation

- assessment of MEMS applicability
- sensor placement strategy



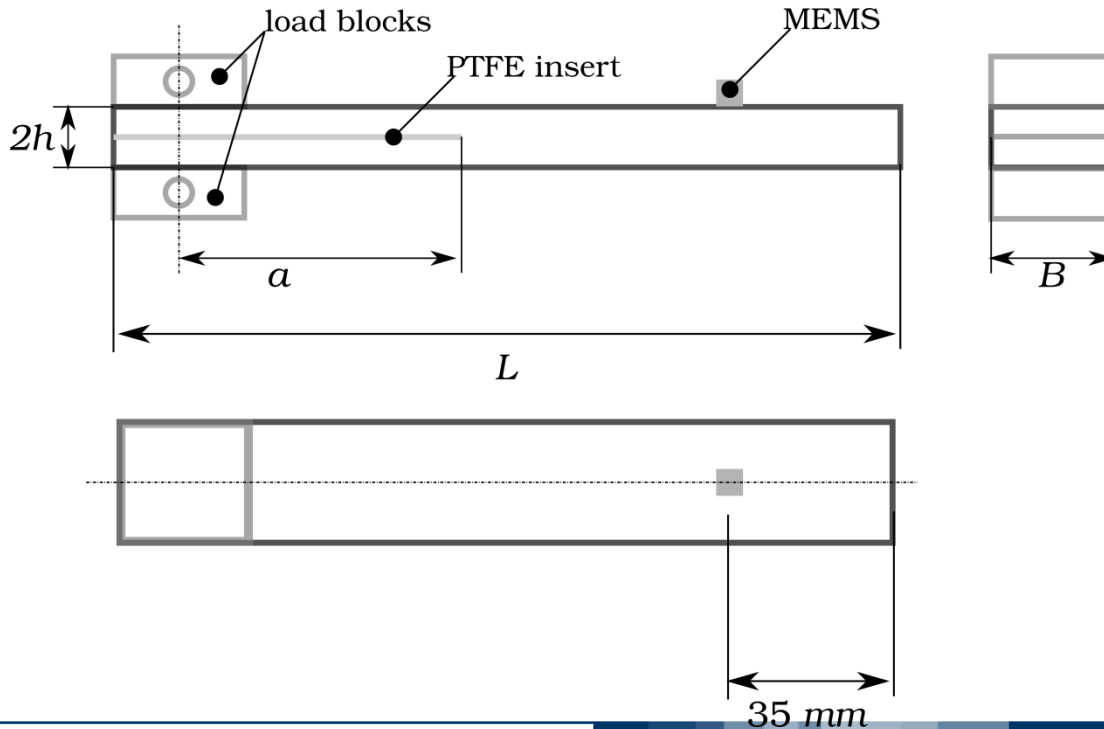
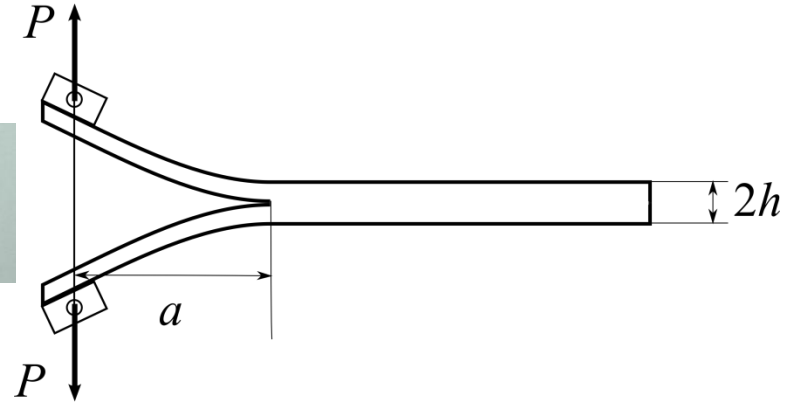
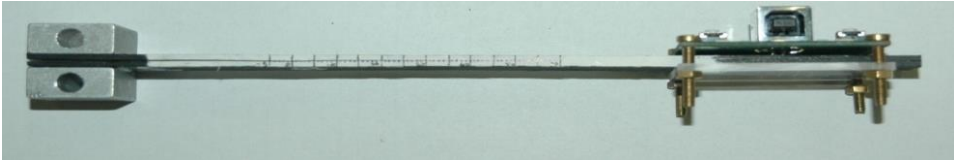
Features of 3-axis, digital output **MEMS** (micro electro-mechanical sensor) accelerometer **LIS3LV02DQ** (STMicroelectronics):

- full scale $\pm 2g$
- bandwidth 640 Hz
- sensitivity 1,000 LSb(Least_Significant_bit)/g
- resolution 1 mg
- weight 0.2 grams
- side: ~ 5 mm



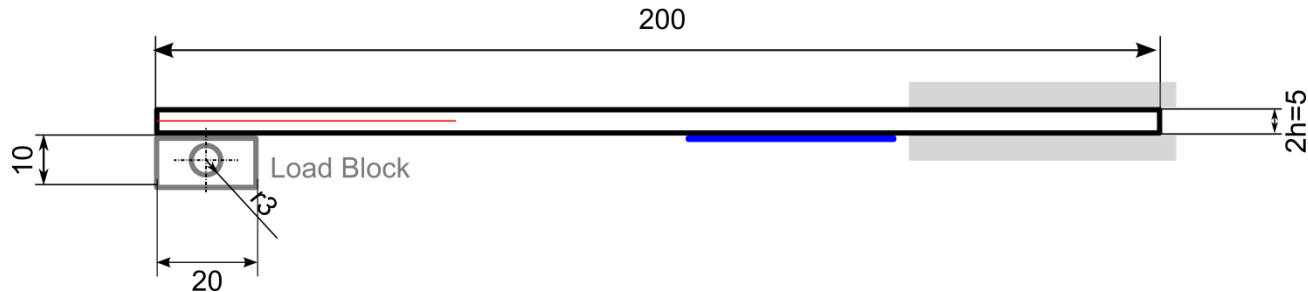
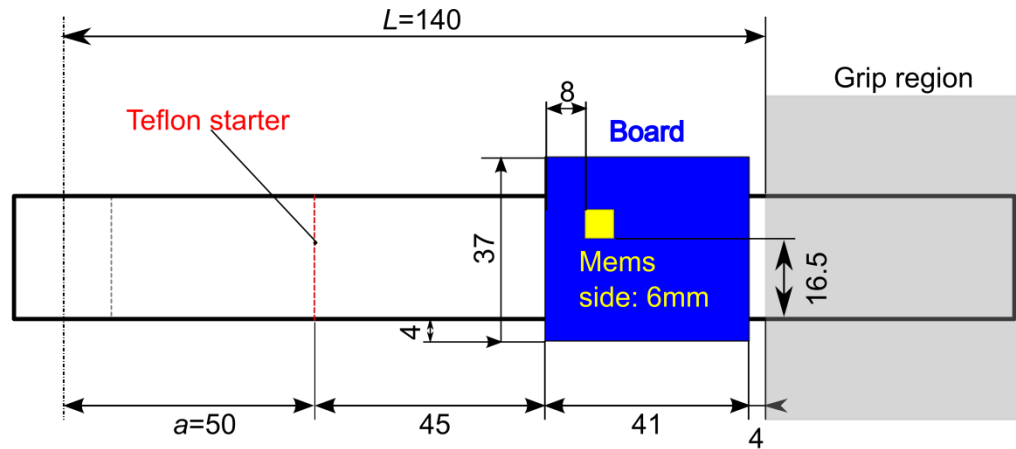
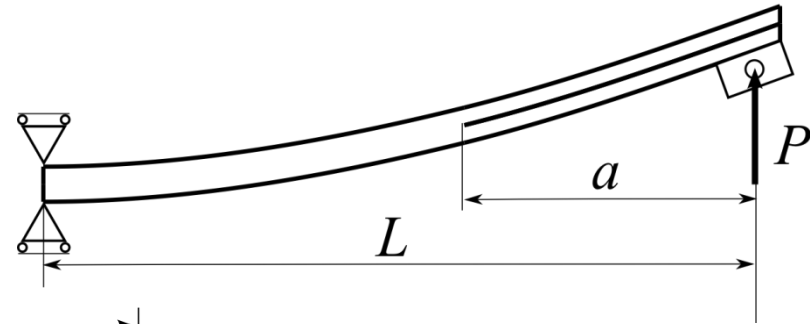


Standard DCB ...



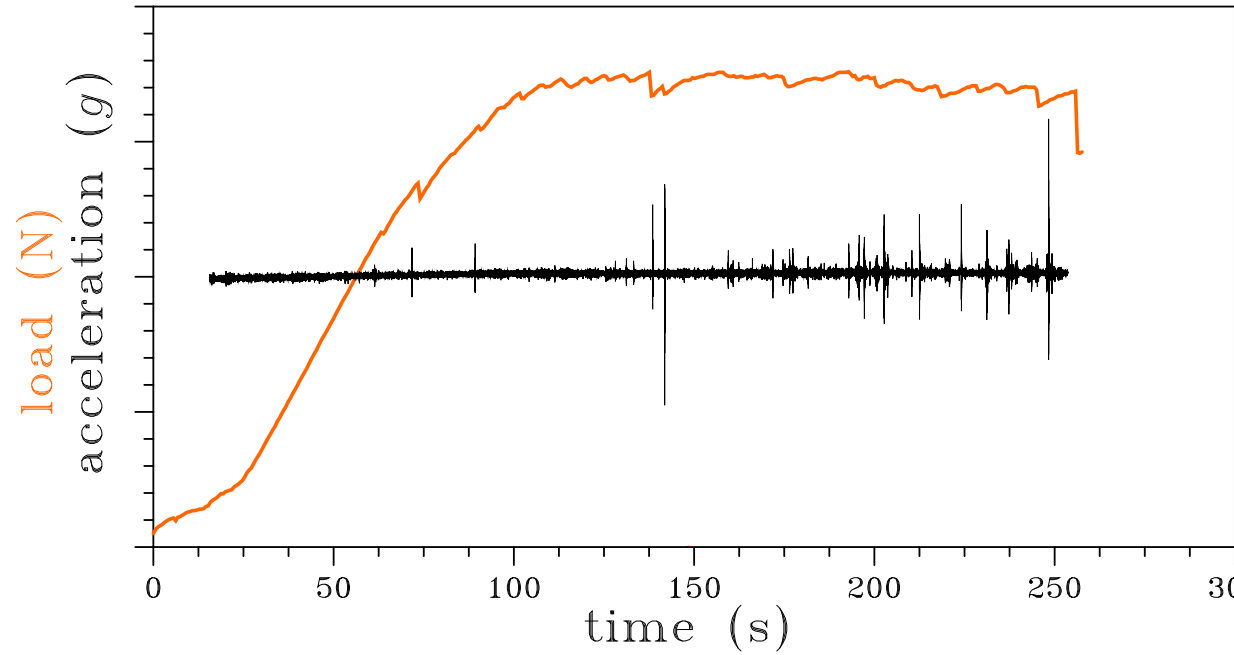
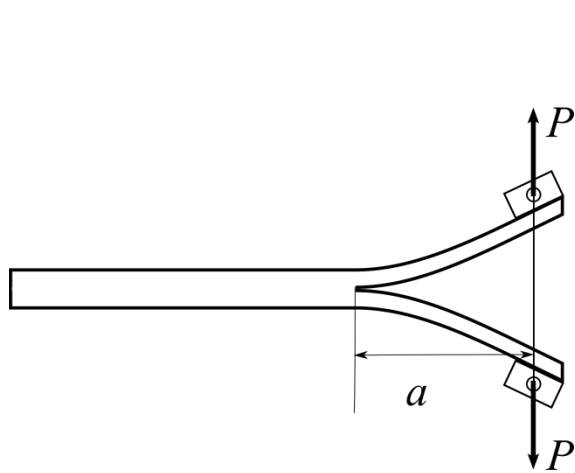


...and ELS test specimens





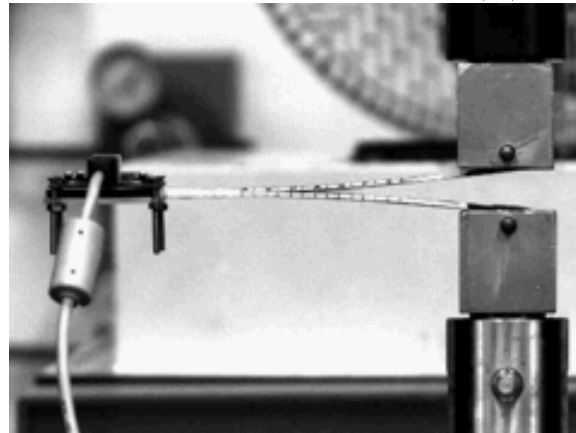
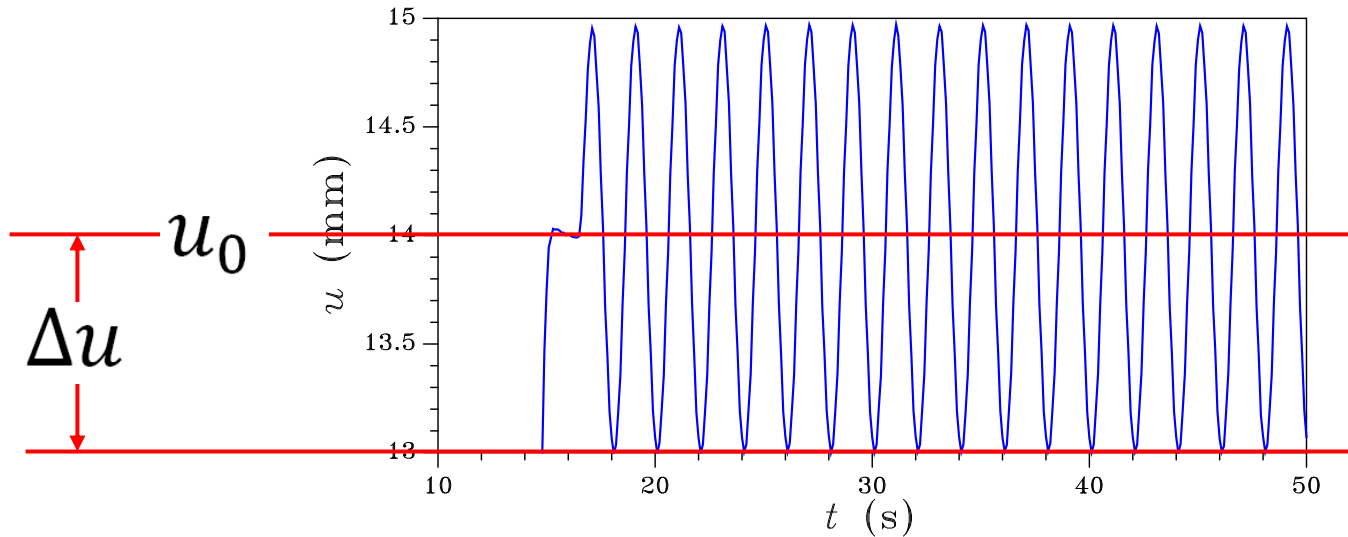
Test #1: DCB test under continuously increasing displacement



Fair correlation between load drops and acceleration peaks

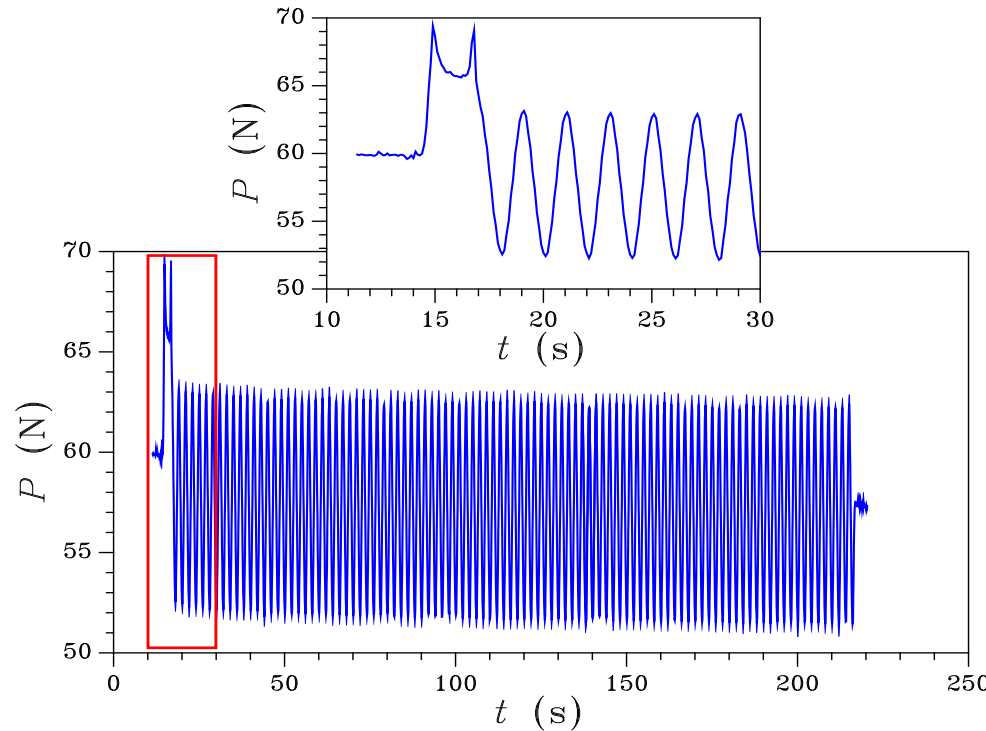
Input: Sinusoidal displacement u

(at increasing u_0 , $\Delta u = 2.5$ mm, frequency = 0.5 Hz, 200 cycles)

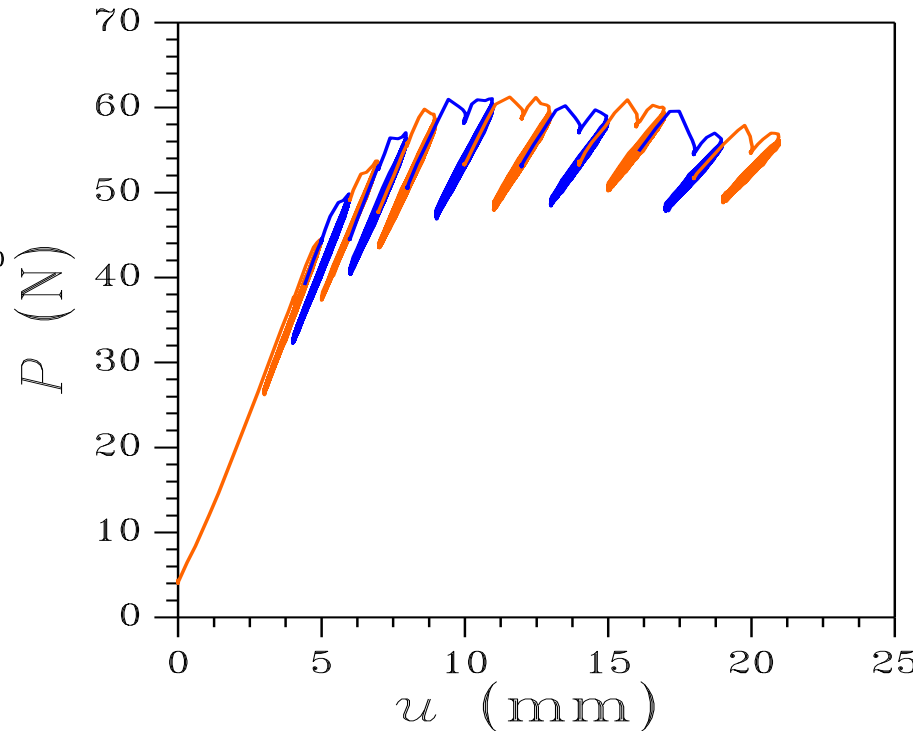


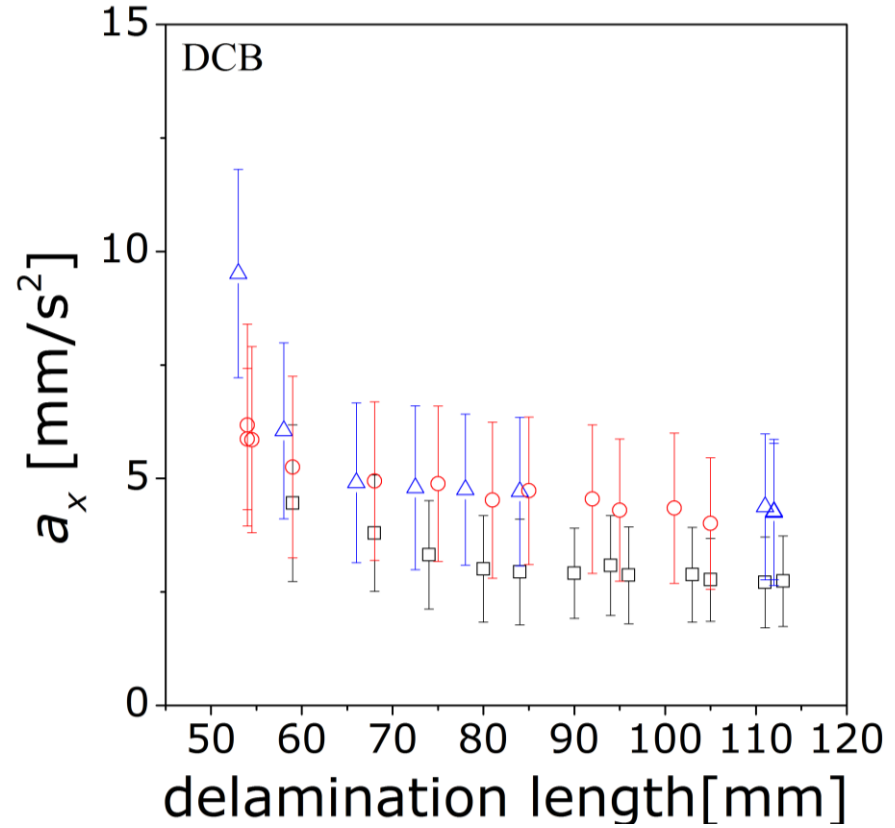
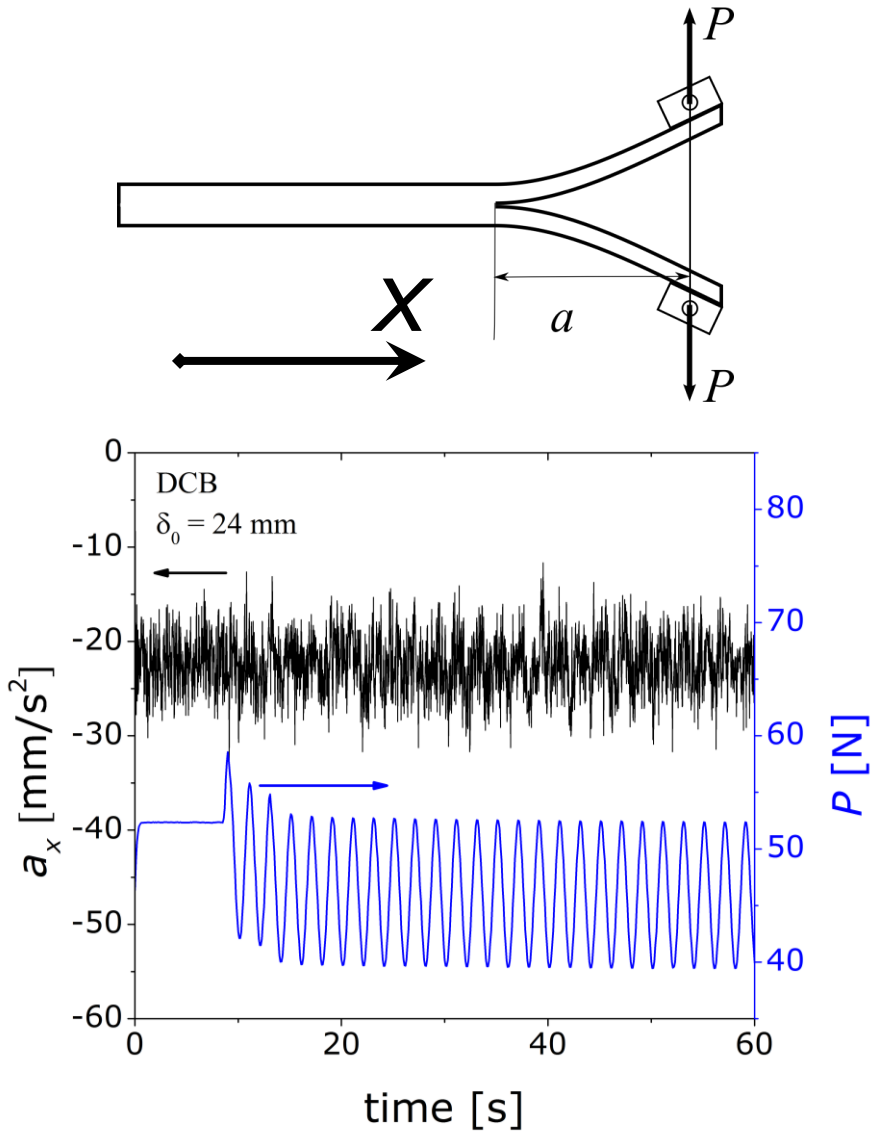


test #2: load output



Load P suffers drops because of delamination growth at the beginning of load steps

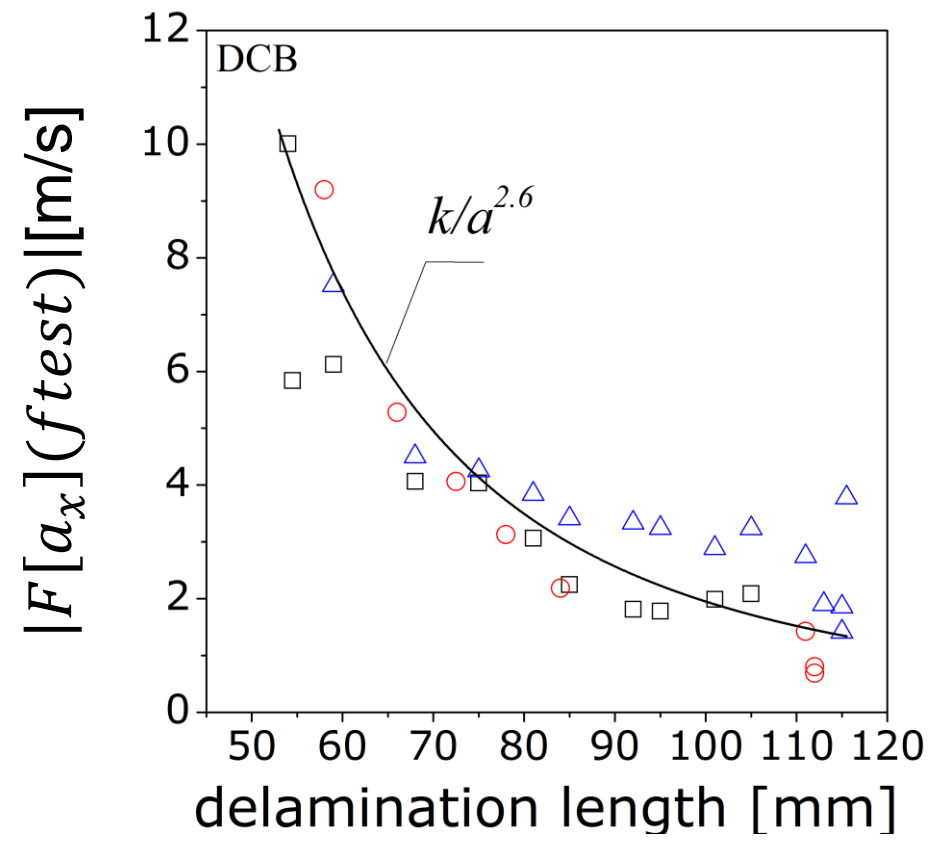
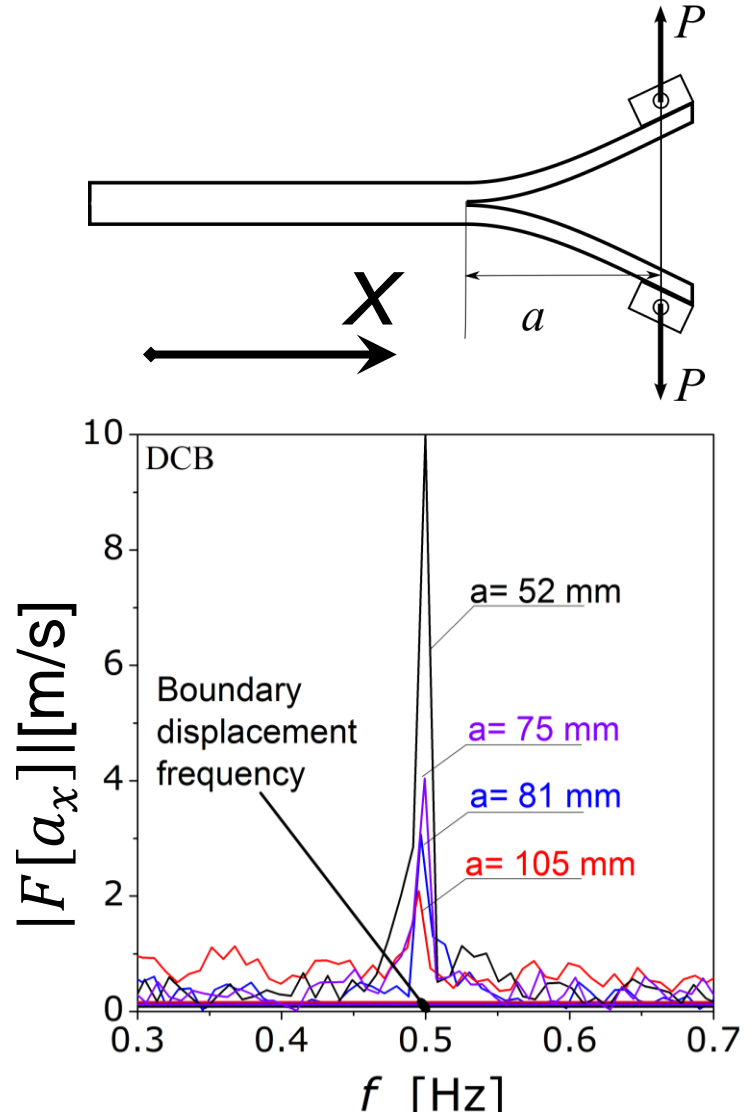




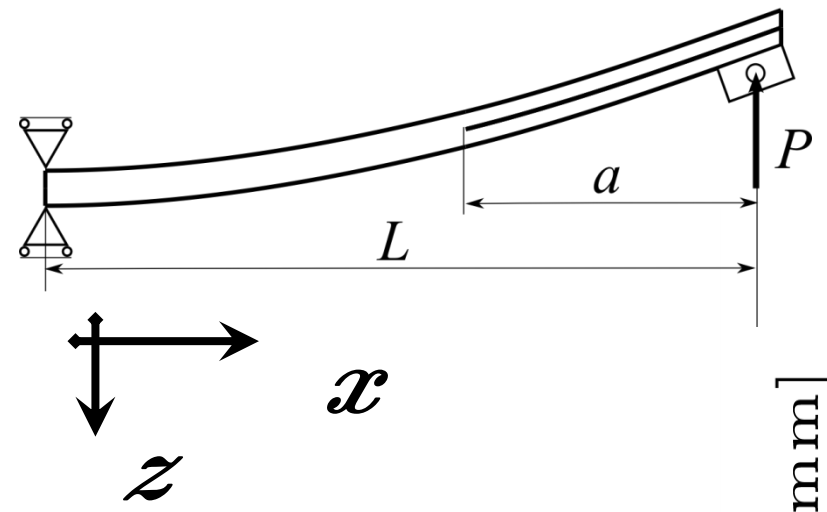
the acceleration, a_x , is too noisy to reliably determine the crack length

test 2#: simple sensing system for DCB specimens

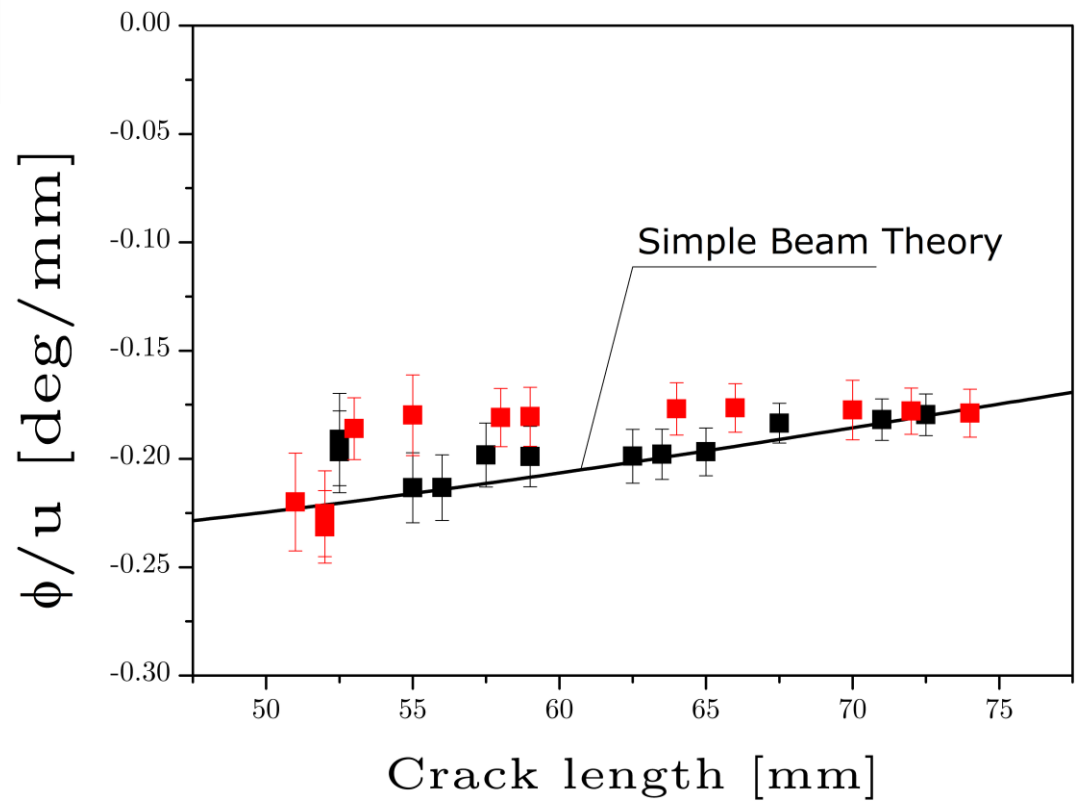
but taking the Fourier transform $F[a_x]$ of the signal



ELS: mean rotation

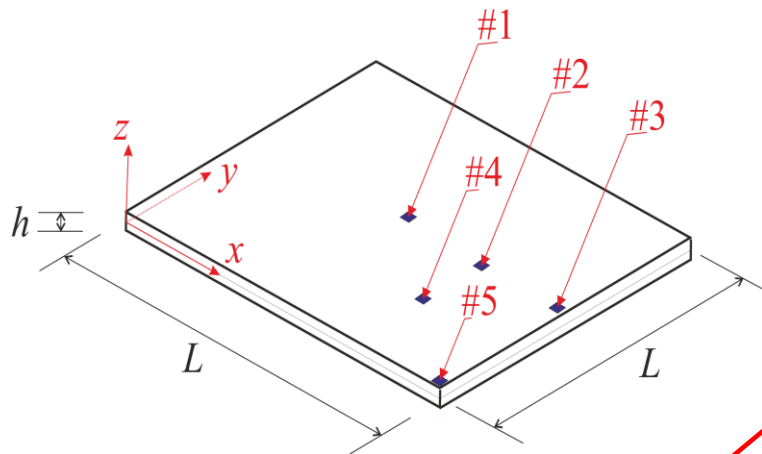


$$\phi = \frac{du}{dx} \simeq \text{atan} \frac{a_x}{a_z}$$





- **Topology approach:** define a density distribution \mathbf{x} representing sensor position and optimize it in order to make damage detection easier
- **Finite elements (FE)** for structural analysis (plates)
- **Method of moving asymptotes (MMA)** for optimization



penalization term to approach pure 0-1 distributions

undamaged plate solution damaged plate solution

$$\left\{ \begin{array}{l} \max_{\mathbf{x}} \sum_{i=1}^n x_i^p (u_i - \hat{u}_i)^2 \\ \text{s. t.} \\ \sum_{i=1}^n x_i \leq \bar{N} \\ 0 \leq x_i \leq 1 \quad i = 1, \dots, n \end{array} \right.$$

max allowed number of sensors

number of possible sensor locations (FE)



Objective functions for an arbitrary number of damaged regions

number of damaged areas

In case of a **multiple damaged regions** (and/or unknown position), to maximize the **sensitivity to the magnitude** of the effects of damage [FORM-1]:

$$\left\{ \begin{array}{l} \max_x \sum_{k=1}^s \left[\sum_{i=1}^n x_i^p (u_{ki} - \hat{u}_i)^2 \right] \\ \text{s. t.} \\ \sum_{i=1}^n x_i \leq \bar{N} \\ 0 \leq x_i \leq 1 \quad i = 1, \dots, n \end{array} \right.$$

or, to maximize the **sensitivity to damage** [FORM-2]:

$$\left\{ \begin{array}{l} \max_x \sum_{k=1}^s \left[\frac{\sum_{i=1}^n x_i^p (u_{ki} - \hat{u}_i)^2}{\max_i x_i^p (u_{ki} - \hat{u}_i)^2} \right] \\ \text{s. t.} \\ \sum_{i=1}^n x_i \leq \bar{N} \\ 0 \leq x_i \leq 1 \quad i = 1, \dots, n \end{array} \right.$$

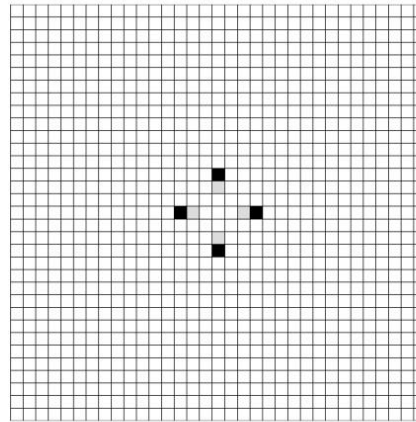
displacement variable:

$$u_{ki} = \sqrt{\phi_{x,ki}^2 + \phi_{y,ki}^2}$$

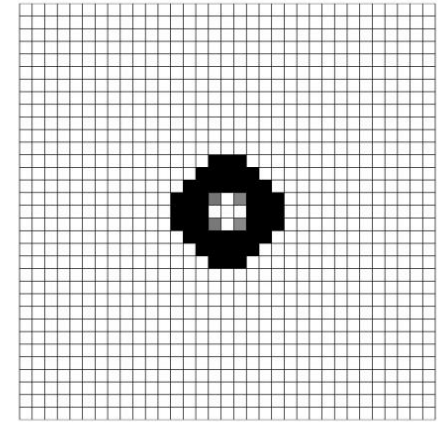
damage can be anywhere,
known size (1 FE)

[FORM-1]

$$\bar{N} = 5$$

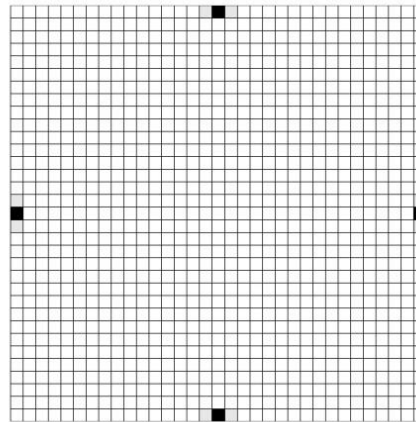


$$\bar{N} = 50$$

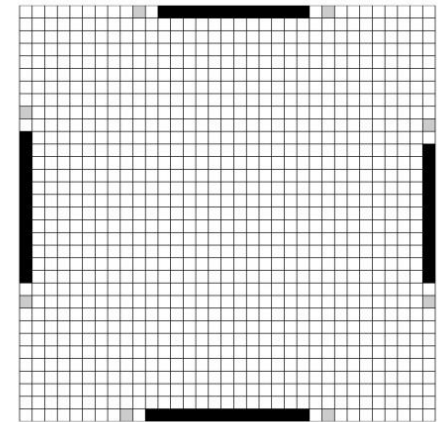


[FORM-2]

$$\bar{N} = 5$$



$$\bar{N} = 50$$



(Mariani et al., JIMSS 2013;24:1105)



simply supported plate, distributed load

damaged area

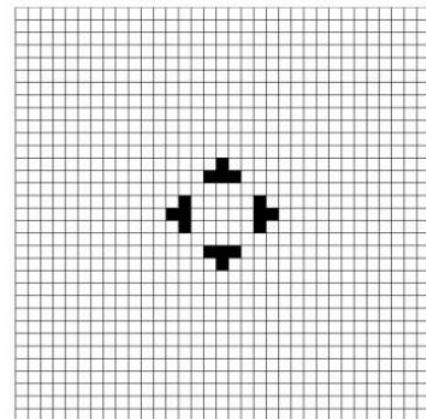
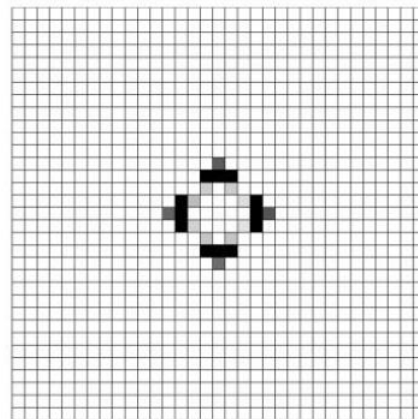
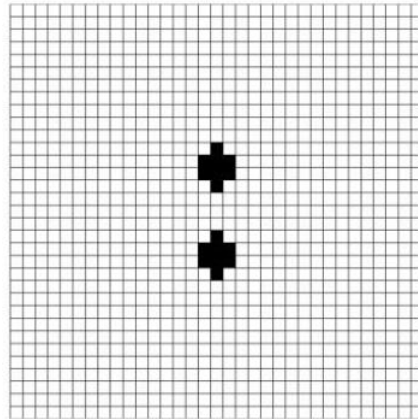
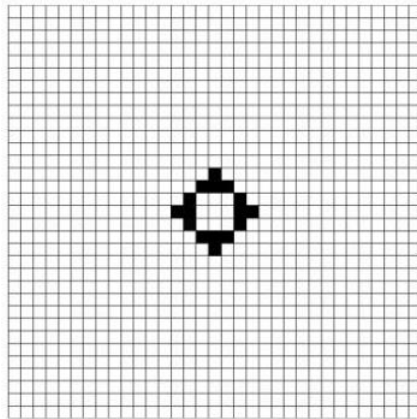
1×1 ■

1×2 ■

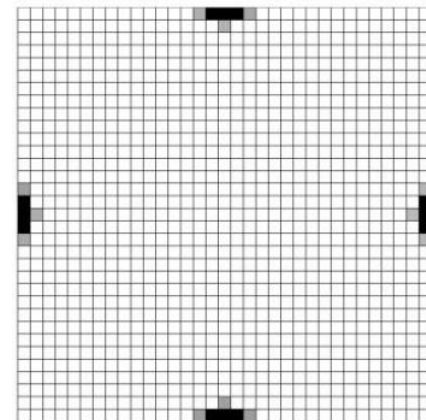
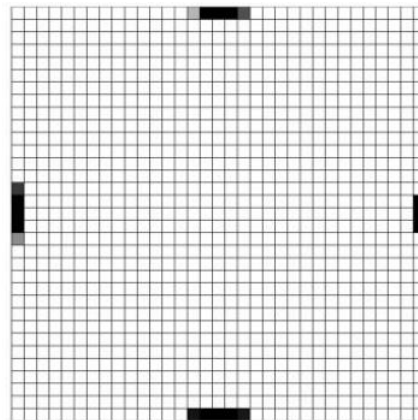
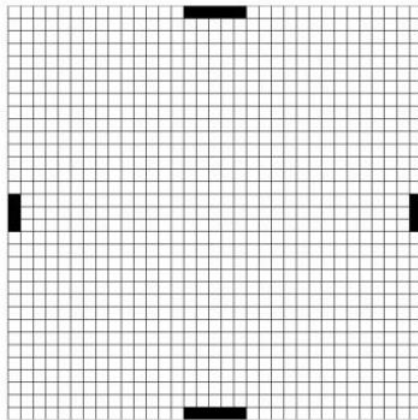
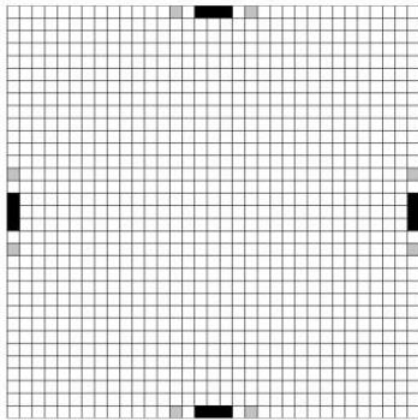
2×2 ■

4×4 ■

[FORM-1]



[FORM-2]





clamped plate, concentrated load, [FORM-2],

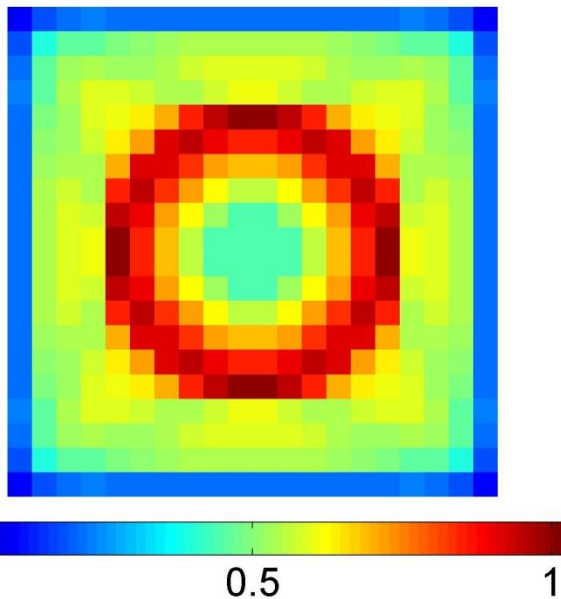
Multi-scale analysis:

$L=1$ m (side length, or structural size)

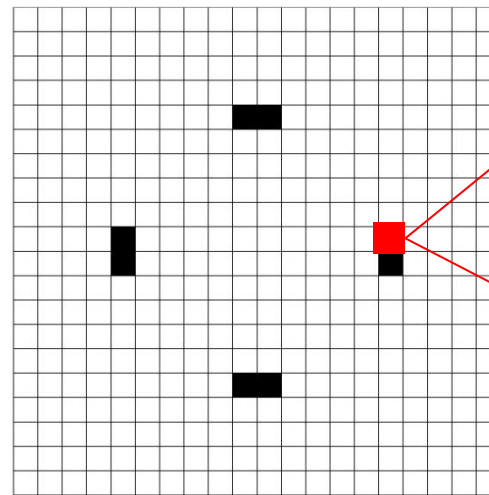
$s=5$ cm (element, or damaged area size)

$l=2.5$ mm (sensor size)

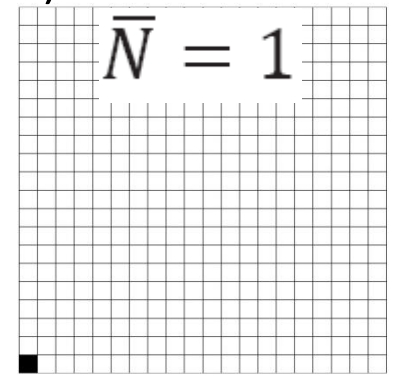
objective function



sensor macro-placement

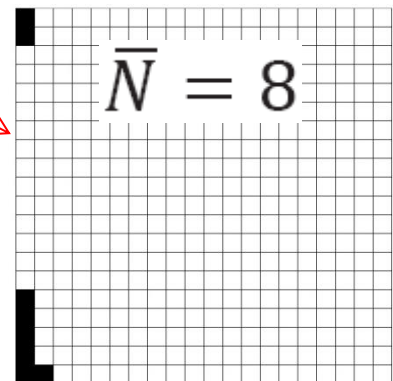


$$\bar{N} = 1$$



sensor micro-placement

$$\bar{N} = 8$$





- We proposed a MEMS-based SHM system, sensitive to damage (delamination) extent in composite
- We proposed a (possibly multi-scale) topology optimization-like procedure to deploy MEMS, so as to maximize sensitivity to damage

Ongoing activities and future work

- real-time damage detection and identification for flexible (composite) plates
- minimization of \bar{N}
- Application: engineered bike and ski helmets (to understand links between impacts and brain injuries)

Acknowledgments

- Italian MIUR-PRIN, project *Mechanics of microstructured materials: multi-scale identification, optimization and active control*
- Italian Consorzio Interuniversitario Nazionale per la Scienza e la Tecnologia dei Materiali (INSTM)
- Regione Lombardia and CILEA Consortium, grant *M²-MEMS*
- Fondazione Cariplo, project *Safer Helmets*