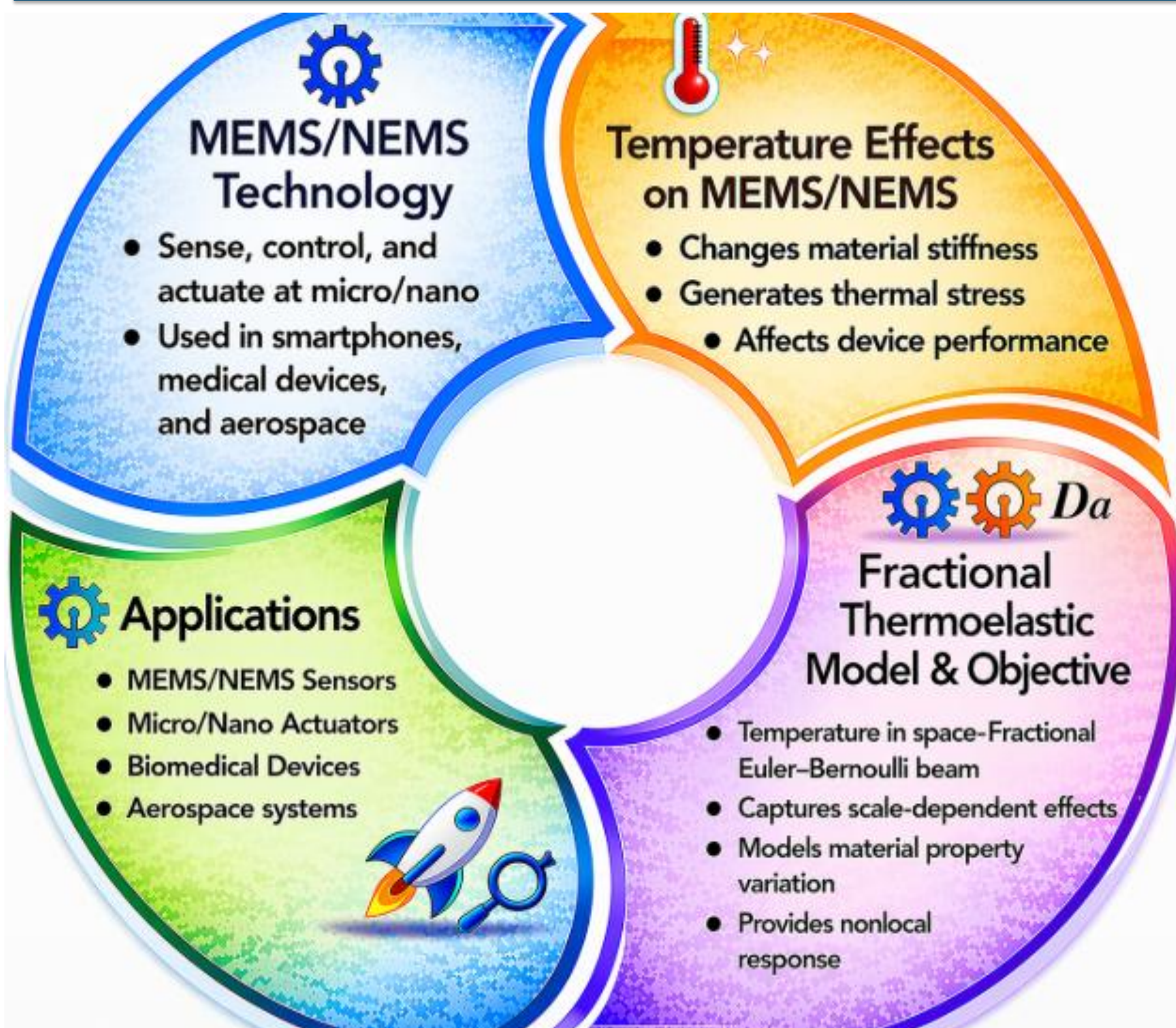


## Fractional Calculus for Space-Fractional Thermoelasticity

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### INTRODUCTION & AIM



### Method

Space-fractional Euler–Bernoulli beam [1] is extended by including temperature-dependent parameters  $E(T)$ ,  $\alpha(T)$  and  $l_f(T)$ :

$$D_x^\alpha \{ l_f^{\alpha-1} D_x^\alpha [ l_f^{2\alpha-2} D_x^\alpha ( l_f^{\alpha-1} D_x^\alpha u ) ] \} EI = p(x)$$

### Special Case:

For  $\alpha = 1$ , the model reduces to the classical Euler–Bernoulli beam:

$$\frac{d^4 u}{dx^4} EI = p(x)$$

### Boundary Conditions:

Propped cantilever beam:

$$\begin{cases} u_0(x_0)=0, \varphi_0(x_0)=0, \\ u_n(x_n)=0, M_n(x_n)=0 \end{cases}$$

### Solution Approach:

1. Finite Difference Method.
2. Trapezoidal rule [1] (for approximating Caputo derivative).



### RESULTS & DISCUSSION

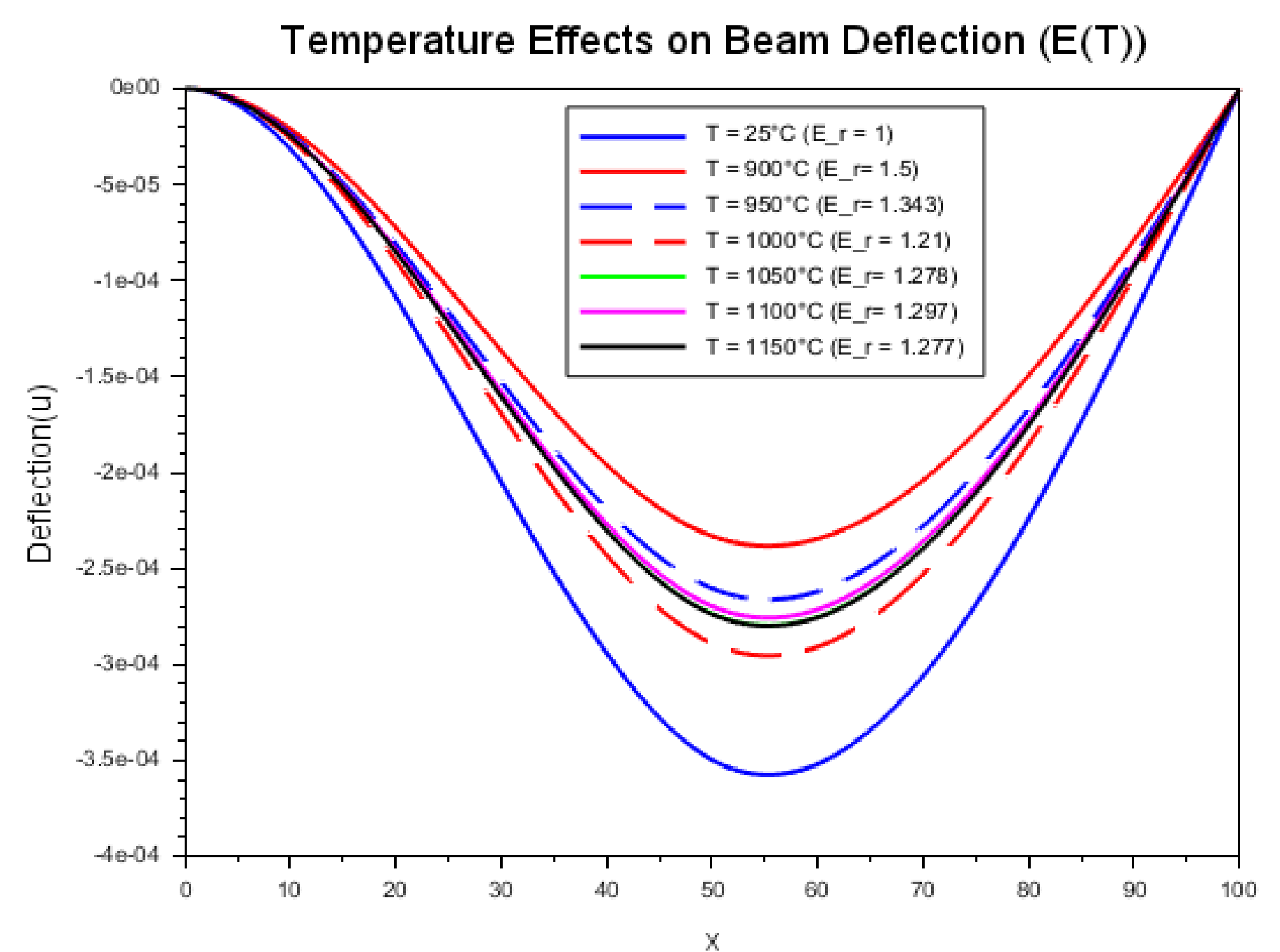


Figure 1: The effect of increasing temperature on deflection, with varying Young's modulus  $E(T)$  while the grain size remains constant.

### Temperature Effects on Beam Deflection (E(T) & Grain Size)

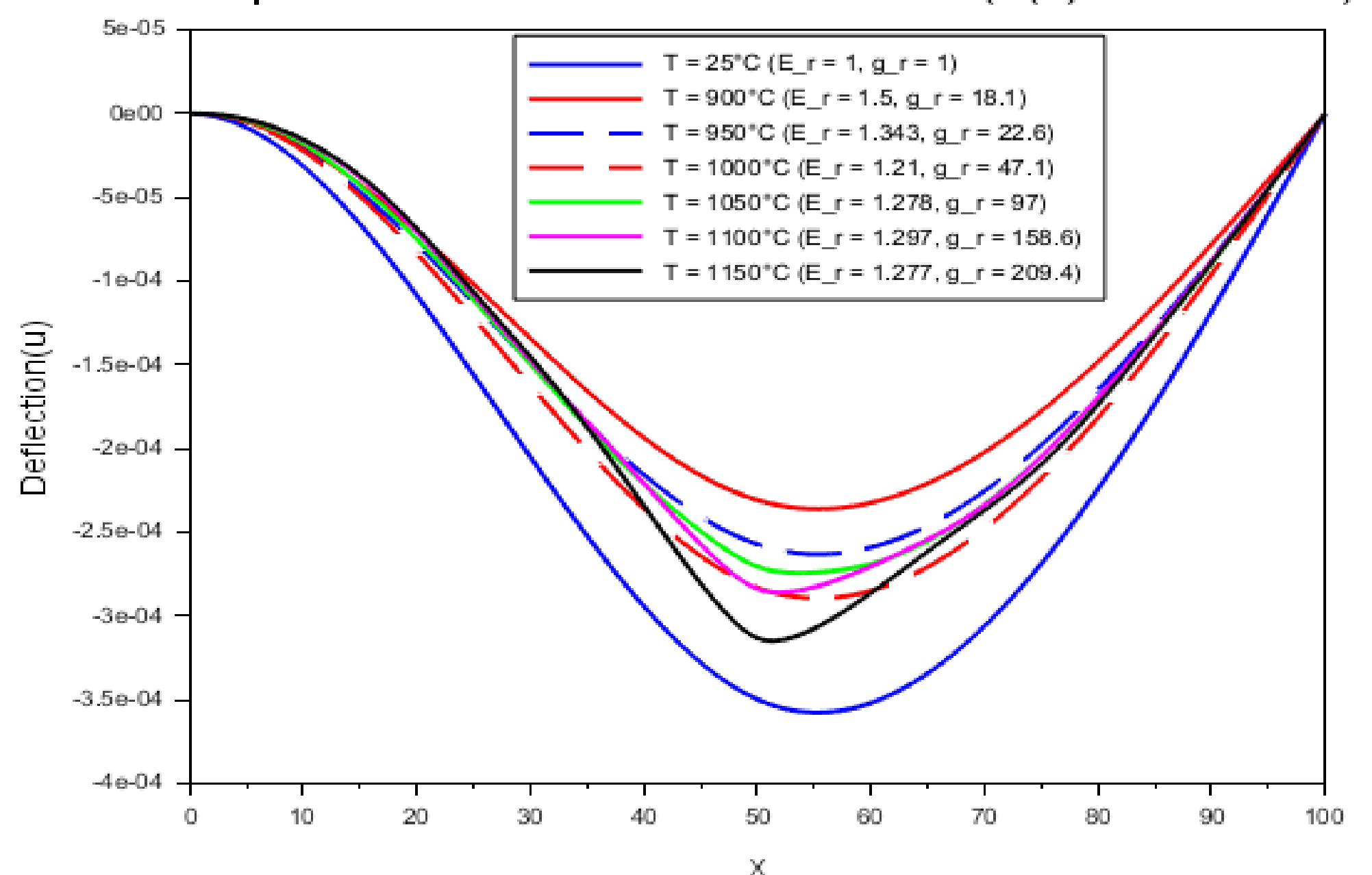


Figure 2: The effect of increasing temperature on deflection, with varying Young's modulus  $E(T)$  and grain size.

### CONCLUSION

- For a constant grain size, an increase in temperature leads to a reduction in Young's modulus, which results in enhanced beam deflection.
- Moreover, deflection increases further due to the combined influence of decreasing Young's modulus and increasing grain size with rising temperature.

### REFERENCES

- 1: Stempin P, Sumelka W. Space-fractional Euler–Bernoulli beam model – Theory and identification for silver nanobeam bending. Int J Mech Sci 2020;186:105902.