

# CFD Design of a NETmix Crystalliser for Struvite Precipitation from Sidestream Digestate

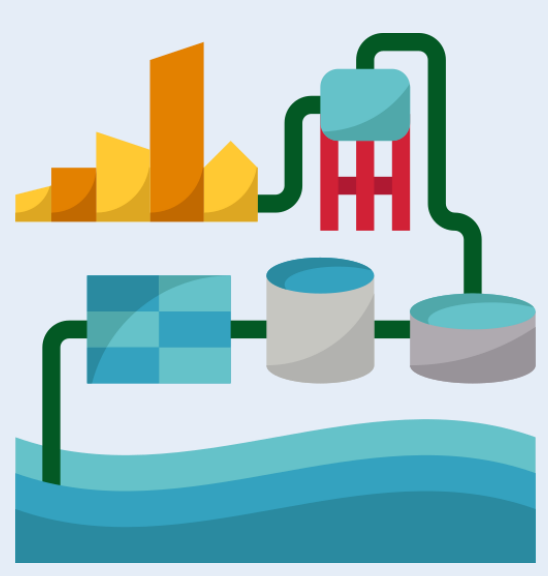
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## INTRODUCTION & AIM

### Wastewater treatment plants



Dewatering process of digested sludge generates a liquid stream called the **centrate**<sup>1,2</sup>

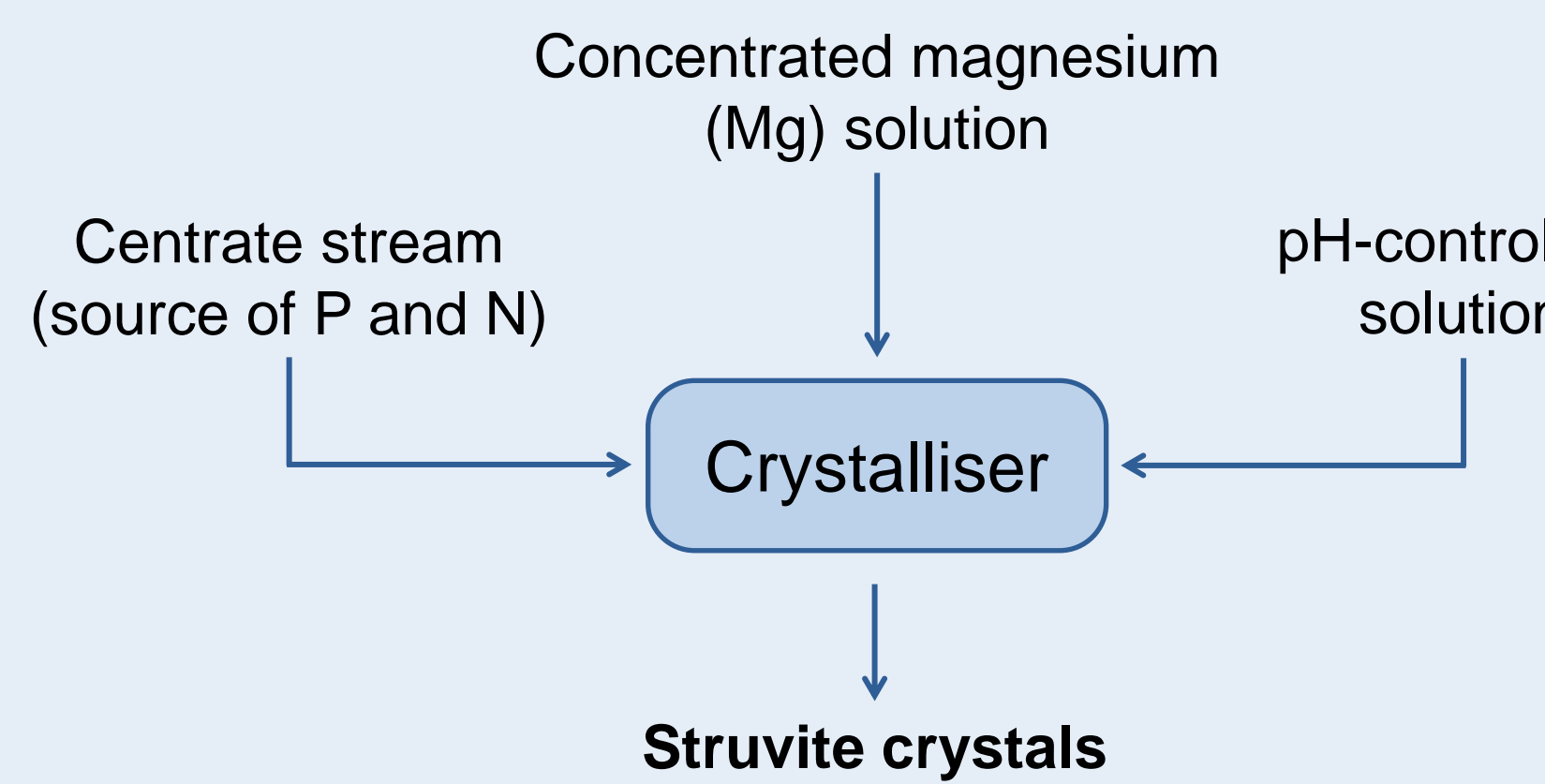
Source of phosphorus (P) and nitrogen (N)<sup>1,2</sup>

Recovery of P and N in solid form through the **struvite precipitation** process<sup>1,2</sup>

Struvite crystals are subsequently used as slow-release environmentally-friendly fertilisers<sup>1,2</sup>



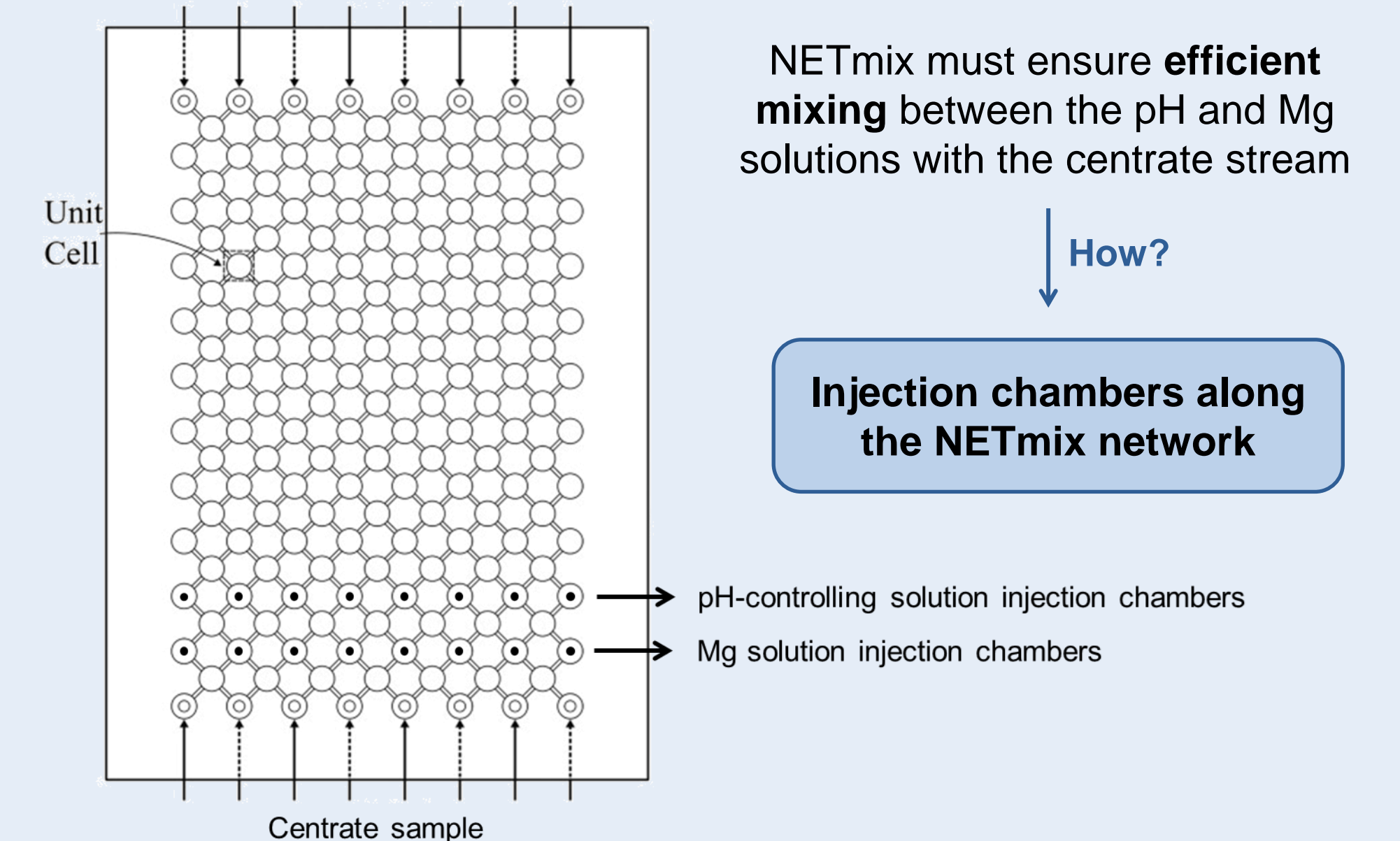
### Struvite precipitation process<sup>3</sup>



#### Main objective

Assess the effect of injection chamber position on the micromixing performance of the NETmix reactor through the Computational Fluid Dynamics (CFD) simulation of passive tracer mixing

### Struvite precipitation in NETmix



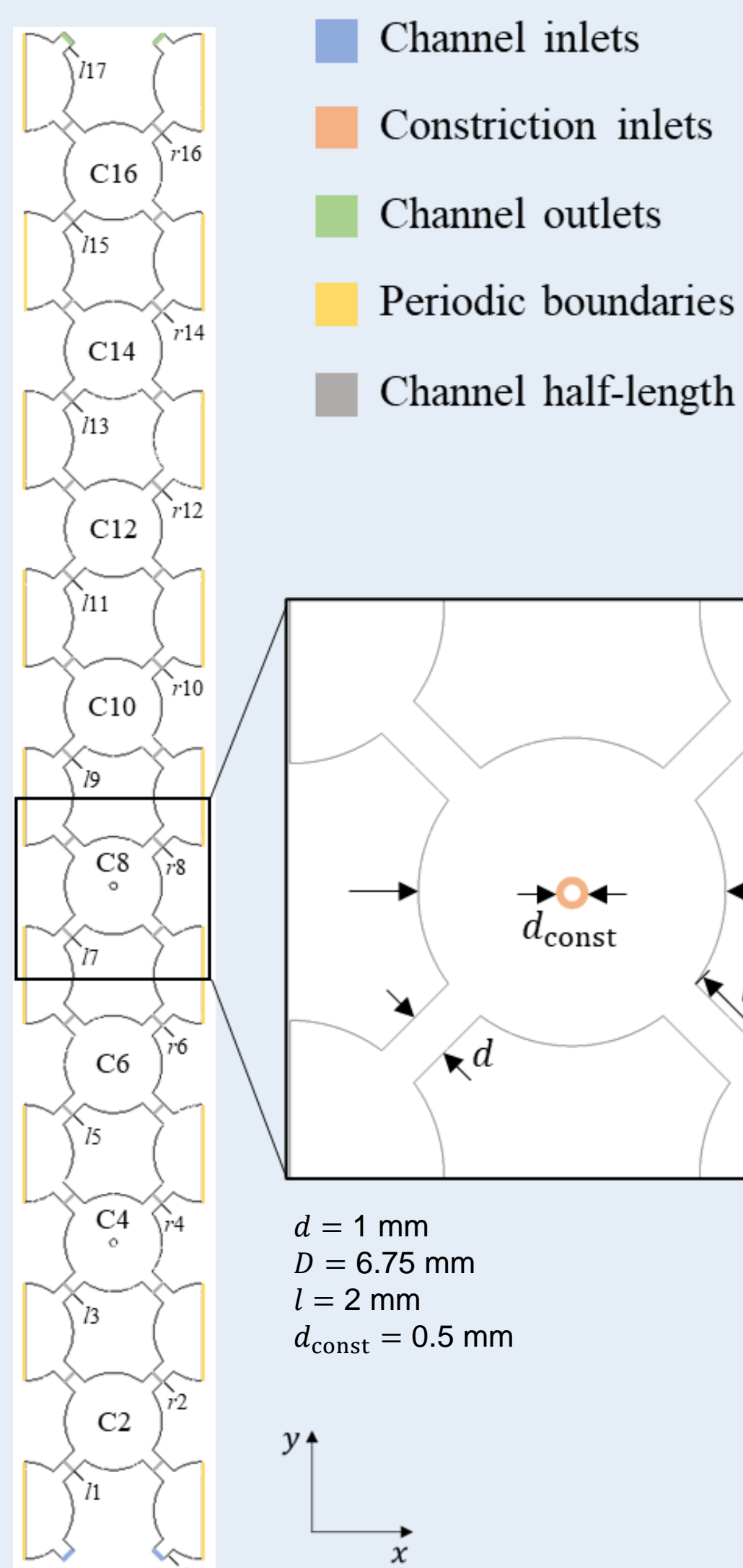
NETmix must ensure **efficient mixing** between the pH and Mg solutions with the centrate stream

How?

Injection chambers along the NETmix network

The Mg and pH-controlling solutions are separately injected at low flowrate ratios relative to the main feed flowrate (effluent) directly into selected chambers along the NETmix reactor

## CFD MODEL



- Simulation of **passive tracer mixing** experiments
- No sub-grid scale modelling
- Working fluids:** water (centrate stream), tracer 1 (Mg solution) and tracer 2 (pH solution) ( $\rho = 998.2 \text{ kg m}^{-3}$  and  $\mu = 1.003 \text{ mPa s}$ )
- Inlet conditions:**
  - Channel inlets:  $Re_{ch} = 300$  (water)
  - Constriction inlets:  $Re_{const} = 45$  (bottom: tracer 1 | top: tracer 2)
- Topologies of injection studied:**
  - C2 and C4
  - C2 and C6
  - C2 and C8
  - C2 and C10
  - C4 and C6
  - C4 and C8
  - C4 and C10

$Re_{ch}$  - Channel inlet Reynolds number  
 $Re_{inj}$  - Constriction inlet Reynolds number  
 $\rho$  - fluid density  
 $\mu$  - fluid viscosity

Figure 1. 2D NUB17 CFD model

## RESULTS & DISCUSSION

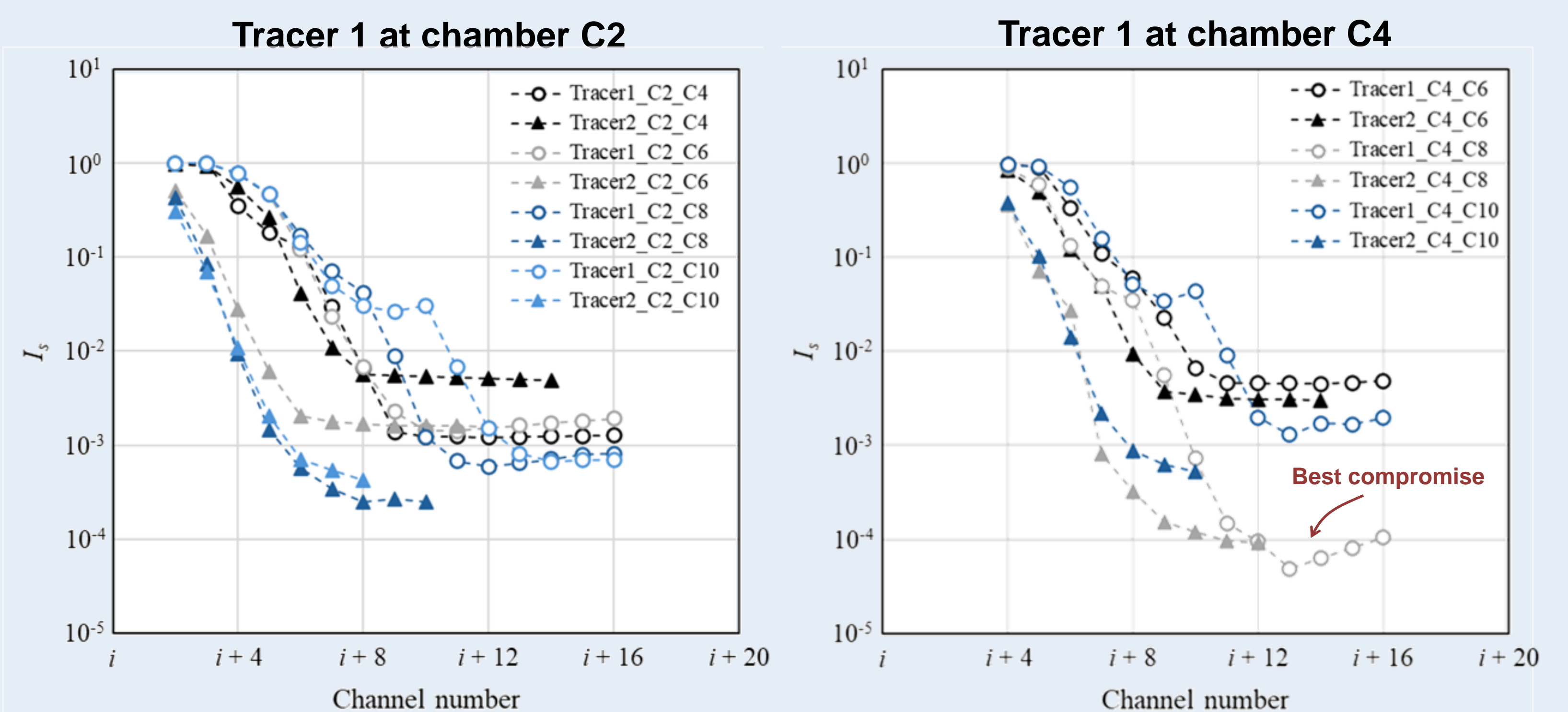


Figure 2. Intensity of segregation,  $I_s = \frac{\sum_{i=1}^N (x_i - \bar{x}_t)^2}{\bar{x}_t(1 - \bar{x}_t)N}$ , along the NETmix channels when tracer 1 is injected in chamber C2 (on the left) and in chamber C4 (on the right) ( $\bar{x}_t$  - average tracer mass fraction)

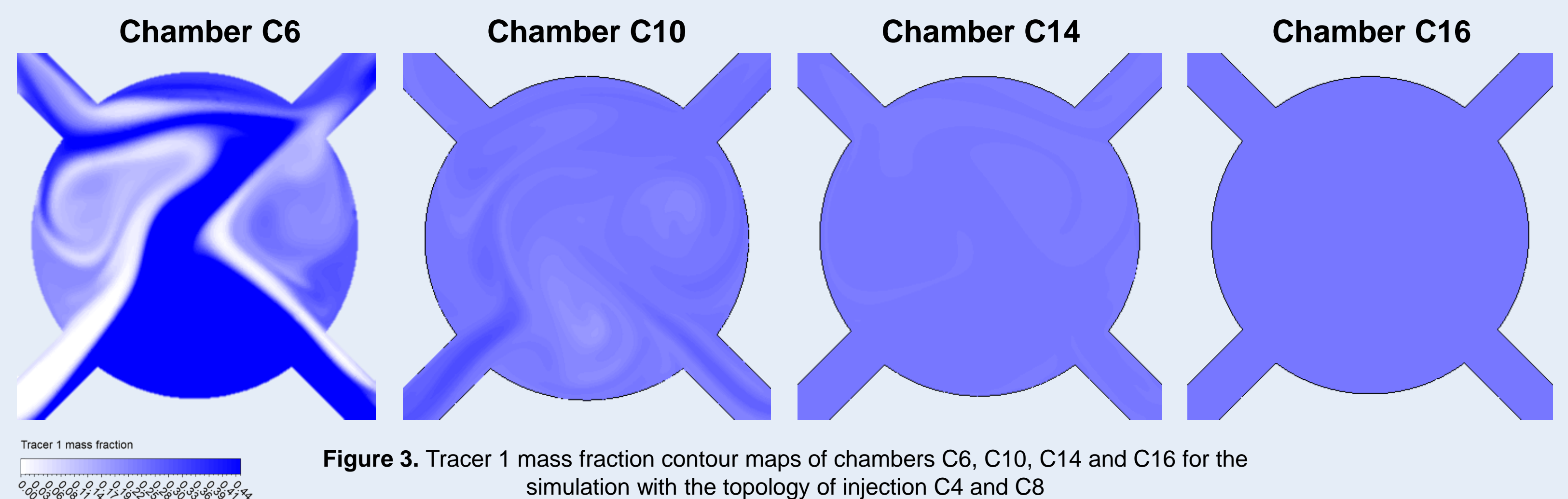


Figure 3. Tracer 1 mass fraction contour maps of chambers C6, C10, C14 and C16 for the simulation with the topology of injection C4 and C8

## CONCLUSIONS

- Results showed that the topology of injection has a great impact on mixing;
- For all configurations studied, the intensity of segregation decreased along the NETmix network, indicating **progressive homogenisation of the streams**;
- The topology of injection that ensured **better mixing performance** (lower  $I_s$  values) was the one with the injection points at **chambers C4 and C8**;
- The optimised injection scheme reduced the intensity of segregation by 99.9 %;
- It also ensured **comparable mixing degrees for both tracers** (Mg and pH-controlling solutions) at the outlets;
- These results are highly relevant for crystalliser design, since mixing directly influences supersaturation, chemical reaction, nucleation and crystal growth during precipitation processes;
- A NETmix crystalliser prototype was constructed based on the CFD results of the present work and will be used for the production of struvite crystals from centrate streams.

## REFERENCES

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- [2] Desmidt, E., et al., Global Phosphorus Scarcity and Full-Scale P-Recovery Techniques: A Review. Critical Reviews in Environmental Science and Technology, 2015. 45(4): p. 336-384.
- [3] Lu, H., et al., Crystallization techniques in wastewater treatment: An overview of applications. Chemosphere, 2017. 173: p. 474-484.

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