

1 *Conference Proceeding*

# 2 **Rule operation model for dams with gate-controlled** 3 **spillways**

4 **Sordo-Ward Alvaro<sup>1,\*</sup>, Gabriel-Martin Iván<sup>1</sup>, Bianucci Paola<sup>2</sup>, Morello Andrea<sup>3</sup> and Garrote Luis<sup>1</sup>**

5 <sup>1</sup> Department of Civil Engineering: Hydraulic, Energy and Environment, Technical University of Madrid,  
6 Madrid 28040, Spain

7 <sup>2</sup> AQUATEC: Proyectos para el Sector del Agua, S.A.U., Madrid 28037, Spain

8 <sup>3</sup> Department of Environment, Land and Infrastructures Engineering, Politecnico di Torino, Turin 10129,  
9 Italy.

10 \* Correspondence: alvaro.sordo.ward@upm.es; Tel.: +34-913366703

11 **Abstract:** The study developed a rule operation model for gated spillways (named K-Method)  
12 which improved the performance of the volumetric evaluation method (VEM). VEM was  
13 proposed by Girón (1988) and is largely used in common practice in Spain. The K-Method was  
14 developed by modifying the VEM and by including a K factor which affects the released flows. A  
15 Monte Carlo simulation environment was designed to evaluate the method under a wide range of  
16 inflow conditions (100,000 hydrographs) and with return periods ranging from 1 to 10,000 years.  
17 The methodology was applied to the Talave reservoir, located in the south-east of Spain. Results  
18 showed that K-Values higher than one always reduced the maximum reservoir levels reached in  
19 the dam. For K-Values ranging from one to ten and for inflow hydrographs with return periods  
20 higher than 50 years, we found a decrease of the maximum levels and outflows compared with the  
21 VEM. Finally, by carrying out a dam risk analysis, a K-Value of 5.25 was the best reducing 8.4%  
22 VEM expected annual damage.

23 **Keywords:** Flood control operation, Gated spillway, Volumetric evaluation method; Rule  
24 operation.

25 **PACS:** J0101

---

## 27 **1. Introduction**

28 Dam operations to manage the floods should guarantee the dam safety, minimize the risk of  
29 floods downstream the dam and maintain the reservoir at full operational capacity once the flood is  
30 over [1-5]. Dams with gated spillway represent around 30% of large dams around the world [6] and  
31 give more possibilities for water conservation and flood abatement than those with fixed-crest  
32 spillways [7]. They provide more flexibility of operation by incorporating different strategies for  
33 managing the floods [8]. On the other side, gate management during a flood event represents a  
34 challenge for the dam operator, who has to make decisions under pressure and in uncertain  
35 conditions. In addition, the time frame for decision making is usually extremely short, the  
36 information available is generally sparse, and the predictability of the meteorological situation is  
37 limited [9]. Real-time flood control operations in dams have historically been approached using  
38 predefined graphs obtained by simulation techniques [10]; or using simulation methods such as the  
39 volumetric method (VEM) [11], commonly used in Spain.

40 Simulation methods generally establish the total flow discharge at a time instant considering  
41 information about inflow, reservoir stage, stored volume and outflow discharged downstream  
42 available at the previous time [12]. Dams Master Plans include these methods, helping operators to  
43 manage floods in an efficient way [1]. These models are usually more flexible and easier to interpret  
44 for the dam operators comparing with others models like optimization models [13-18] or data-based  
45 learning models [19-24], among others.

46 The main objective is to develop a rule operation model for gated reservoirs with the aim of  
 47 improving the VEM proposed by Girón [11] and by using a Monte Carlo approach. The proposed  
 48 methodology allows to improve flood control operations, giving dam managers a tool to decide  
 49 which is the best way of reducing flood risk associated to the dam and downstream safety.

## 50 2. Materials and Methods

51 A probabilistic approach was implemented combining a Monte Carlo framework and  
 52 deterministic reservoir flood control rules. We proposed an operation rule named as K-Method, as  
 53 an improvement of the wide used VEM [11]. A Monte Carlo environment was carried out to  
 54 generate a set of storms and the corresponding hydrographs that were used as input to the reservoir.  
 55 The abatement of the floods was implemented considering the proposed method. Additionally, its  
 56 behavior was compared with the VEM and the Inflow-Outflow Method (I-O). I-O for gate operation  
 57 exchange similar values of inflow to the reservoir by discharges, so no attenuation effect of the  
 58 reservoir is considered while the gates are partially opened.

59 The methodology can be outlined with three main components:

- 60 1. Rainfall generation and hydrometeorological model.
- 61 2. Flood routing in the reservoir and dam operation applying the different operation simulation  
 62 models: VEM, K-Method and I-O Method.
- 63 3. Result analysis.

64 In order to compare the behavior of the different operation rules through a large range of  
 65 floods, the study considered return periods from one to 10,000 years. As recommended by other  
 66 authors, for obtaining representative and robust results [25-28], we generated and analyzed 100,000  
 67 maximum annual reservoir inflow hydrographs. In order to generate the set of inflow hydrographs,  
 68 the rainfall generation and the hydrometeorological model was based on the Monte Carlo simulation  
 69 framework proposed by [28]. The reader may refer to [28] for a more detailed description of the  
 70 processes involved.

71 Regarding to the reservoir routing and gated-controlled rule operation we applied three  
 72 methods: The volumetric evaluation method (VEM), the I-O and the K-Method. VEM was proposed  
 73 by Girón [11] and it is a simulation model that allows to calculate in real time the outflow during a  
 74 flood event in reservoirs with controlled outflows. VEM is based on three principles:

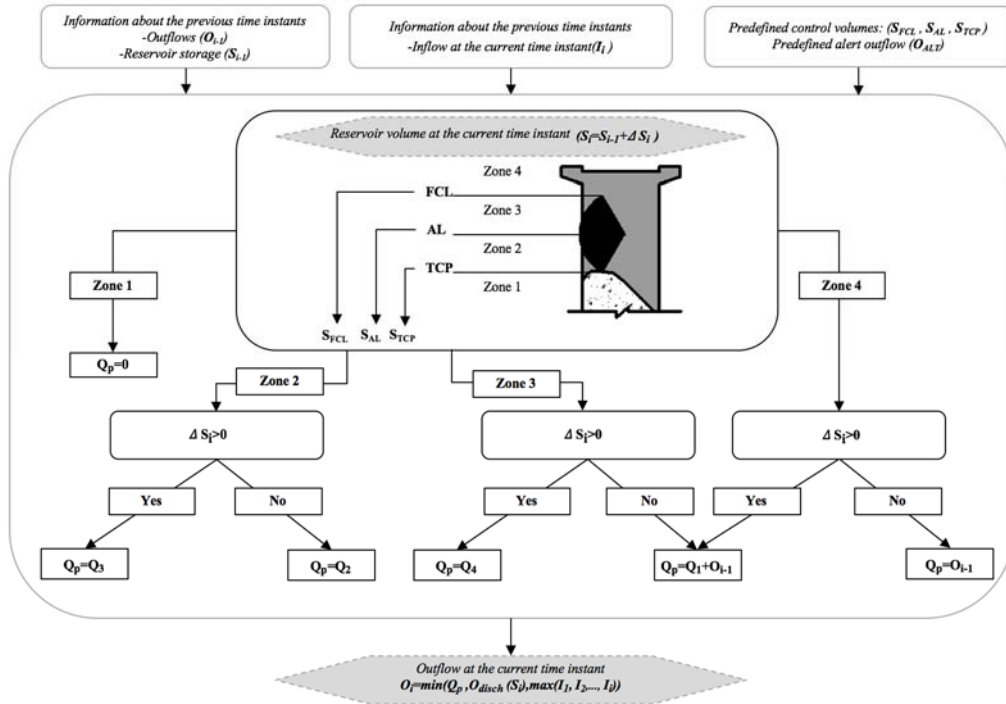
- 75 1. Outflows are lower or equal than inflows while the inflow hydrograph is increasing.
- 76 2. Outflows increase when inflows increase.
- 77 3. The higher the reservoir level, the higher the percentage of outflow increases.

78 VEM manages the available flood control storage progressively, increasing the outflows as the  
 79 flood control storage decreases.

80 Figure 2 shows the general scheme of the method implementation. First, the reservoir volume  
 81 was obtained ( $S_i$ ). The proposed outflow ( $Q_p$ ) was chosen in function of the reference zone (1,2,3 or 4)  
 82 and whether the reservoir volume increase or decrease ( $\Delta S_i > 0$  or  $\Delta S_i < 0$ ). Once  $Q_p$  is obtained, it is  
 83 compared to the discharge at the current reservoir level ( $O_{\text{disch}}(S_i)$ ) and the maximum of the previous  
 84 inflows ( $I_1, I_2, \dots, I_i$ ), being the minimum of the three values the selected flow for being released  
 85 through the gates ( $O_i$ ).

86 The K-method is a modification of the VEM. A factor (K) is applied to the expression of  $Q_1$   
 87 proposed by the Girón method:

$$\text{If } S_i^F \leq \Delta S_i : Q_1 = \frac{\Delta S_i}{\Delta t}; \text{ else } Q_1 = \mathbf{K} \cdot \frac{\Delta S_i^2}{S_i^F \cdot \Delta t} \quad (1)$$



88

89 **Figure 2.** Volumetric evaluation method scheme (developed from [11]). Four different zones with  
 90 their corresponding proposed discharge formulas were defined ( $Q_1$ ,  $Q_2$ ,  $Q_3$  and  $Q_4$ , not shown).  $S_{TCP}$   
 91 represents the volume at the top control pool,  $S_{AL}$  is the volume at activation level,  $S_{FCL}$  is the volume  
 92 at the flood control level,  $S_i$  is the volume in the reservoir at the time  $i$ ,  $S_{i-1}$  represents the volume in  
 93 the reservoir at the previous time  $i-1$ ,  $O_{i-1}$  is the discharged at the previous time instant and the alert  
 94 outflow is  $O_{ATL}$  (which represents the threshold of outflow from which it is expected to have damage  
 95 downstream).

96 As can be seen in Figure 2 the K factor affects the calculation of discharges in zones 2, 3 and 4. A  
 97 wide range of K-Values were analyzed (varying from  $K = 0.1$  to  $K = 500$  with intervals of 0.05)  
 98 in order to improve the reservoir management rules. Finally, we implemented the I-O method. This  
 99 method consists on applying, for all zones, the expressions corresponding to zone 4, this is, the  
 100 outflows equal the inflows when the hydrograph is increasing (until the maximum discharge  
 101 capacity in which it begins to work as a fixed-crest spillway).

102 *2.1. Case study*

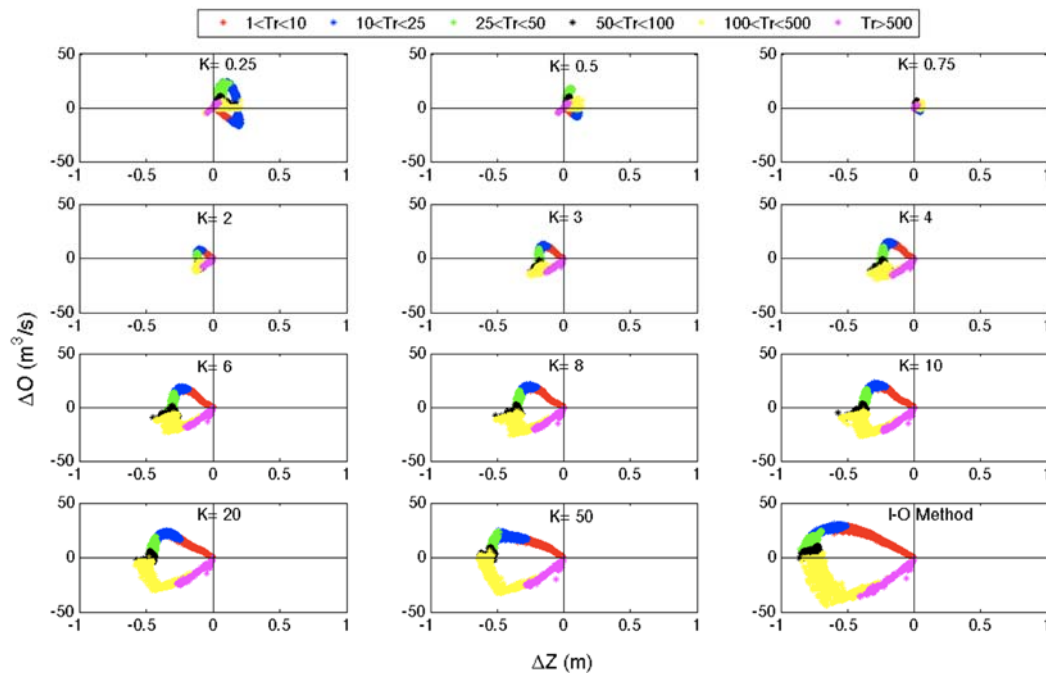
103 The proposed methodology was applied to Talave reservoir. It is located in the province of  
 104 Albacete, in the south-east of Spain. It belongs to the Mundo river basin, being Talave watershed  
 105 area 766.5 km<sup>2</sup>. The climate of the region is mediterranean (mean annual precipitation of 557 mm).  
 106 The main characteristics of the dam-reservoir system configuration are shown in Table 1. The  
 107 principal uses of the reservoir are flood regulation, hydropower generation and water supply for the  
 108 Region of Murcia.

109 **Table 1.** Characteristic reservoir levels and outflows of the dam configuration.

Reservoir levels (m.a.s.l)	Maximum outflow capacity at design flood level (DFL) (m <sup>3</sup> /s)	Characteristic outflows (m <sup>3</sup> /s)
Top of control pool (TCP)	508.9	Gated-spillway 284.9
Activation level (AL)	509.3	Alert outflow ( $O_{ALT}$ ) 100
Flood control level (FCL)	509.9	Fixed-crest spillway 41
Design flood level (DFL)	511.3	Warning outflow ( $O_{WARN}$ ) 150
Crest of dam (COD)	512.4	Bottom outlet 99.5
		Emergency outflow ( $O_{EMER}$ ) 300
		Lower water intakes 18
		Medium water intakes 123

### 110 3. Results and discussion

111 First, we compared the K-Method and I-O to the VEM applying a comparative scheme based on  
 112 quadrants analysis (Figure 2). The points located in the upper right quadrant ( $Q_I$ ) represent events  
 113 where the maximum level reached in the reservoir and the maximum outflow were higher than by  
 114 applying VEM. The points located in the upper left quadrant ( $Q_{II}$ ) show an intermediate situation  
 115 with lower maximum levels but higher outflows. Lower left quadrant ( $Q_{III}$ ) represent cases for which  
 116 both maximum level and maximum outflow are lower than by applying VEM (the best situation).  
 117 Lower right quadrant ( $Q_{IV}$ ) represent intermediate situations with higher maximum levels and lower  
 118 maximum outflows. We also associated the return periods of the inflow hydrographs. Results for  
 119 some analyzed K-Values and I-O are reported in Figure 2.



120

121 **Figure 2.** Comparison of K-Method (for different K-Values) and I-O respect to MEV. Horizontal axis  
 122 shows the increments of maximum reservoir level in meters ( $\Delta Z$ ) by applying the K-Method and I-O  
 123 compared to MEV. Vertical axis shows the increments of maximum outflow in cubic meters per  
 124 second ( $\Delta O$ ) of each method compared with MEV. Red points correspond to events with Tr ranging  
 125 from 1 to 10 years, blue points ranging from 10 to 25, green points from 25 to 50, black points from 50  
 126 to 100, yellow points from 100 to 500 and magenta points from 500 to 10,000 years.

127 It can be seen that if K-Values were lower than one, there was no improvement respect to the  
 128 VEM: most of the points were in  $Q_I$  or  $Q_{IV}$ . Therefore, we focused the following analysis in K-Values  
 129 higher than one, in which the entire set of events were placed in the  $Q_{II}$  or  $Q_{III}$ . Moreover, when  
 130 analyzing the percentage of cases in  $Q_{III}$  and their corresponding Trs (Table 2), all the events with Tr  
 131 lower than 25 years were located in  $Q_{II}$  (regardless the analyzed K-Value), improving the maximum  
 132 levels but worsening the outflows by comparing with VEM. Nevertheless, the maximum outflows  
 133 for K-Values higher than one and lower than ten, for inflows with Tr lower than 25 years, did not  
 134 jeopardize downstream safety as  $O_{ALT}$  was not exceeded. For Tr ranging from 25 to 500 years, the  
 135 percentage of cases included in  $Q_{III}$  (quadrant with the best situation) decreased as K-Value  
 136 increased. For incoming inflows with Tr higher than 500 years, all points were located in  $Q_{III}$ ,  
 137 regardless of K-Value.

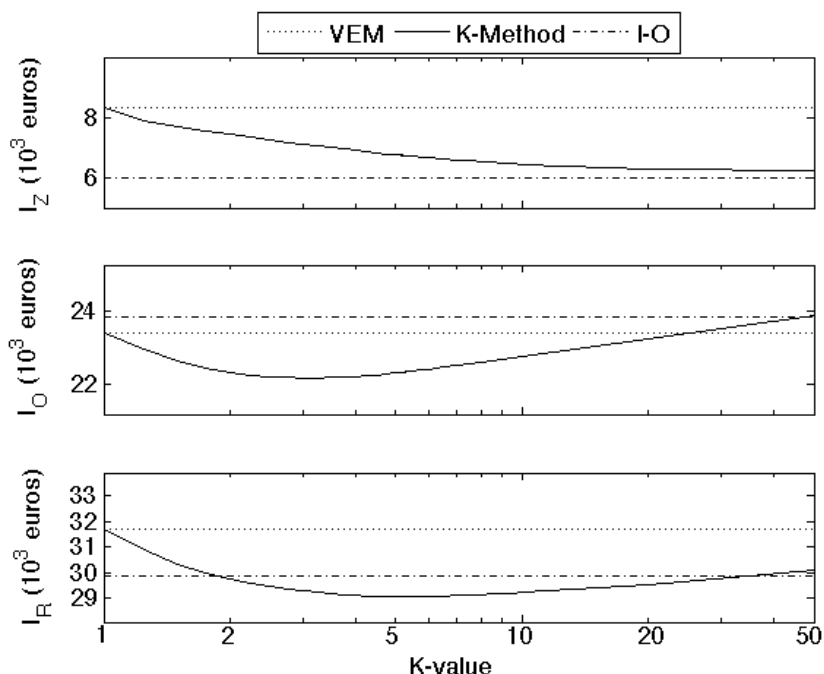
138 We also analyzed the improvement in absolute terms of  $\Delta Z$  and  $\Delta O$ . When analyzing  $\Delta Z$ , the  
 139 higher K-Value was, the higher improvement regardless the range of Trs studied. However, when  
 140 analyzing  $\Delta O$  there were different behaviors depending on the Trs studied. The improvement of  $\Delta O$   
 141 decreased as K-Value increased for Trs lower than 50 years. Within the range from 50 to 100 years,

142  $\Delta O$  decreased or increased depending on the K-Values studied, being the improvement close to  
 143 zero. For  $T_r$ s higher than 100 years, the improvement of  $\Delta O$  increased as K-Value increased.  
 144 Therefore, the choice of a K-Value will depend on whether the dam manager decide to prioritize the  
 145 number of events improved or the entity of improvement. Since the maximum reservoir levels  
 146 decreased for all cases, the hydrologic dam safety is improved but may imply a decrease in  
 147 downstream safety (increase of maximum outflows). However, as it was stated, for K-Values from  
 148 one to ten, the outflows obtained did not exceed  $O_{ALT}$ , causing no damages downstream the dam for  
 149 inflows of return periods lower than 25 years.

150 **Table 2.** Percentage of cases located in the third quadrant ( $Q_{III}$ ) for the different range of return  
 151 periods ( $T_r$ ) studied depending on the K-Value (K) adopted. First value is associated to the lowest  
 152 limit of the interval of K-Value studied

K-Value	Range of % of Cases in $Q_{III}$					
	$T_r < 10$	$10 < T_r < 25$	$25 < T_r < 50$	$50 < T_r < 100$	$100 < T_r < 500$	$T_r > 500$
$1 < K < 5$	0-0	0-0	72-23	100	100-100	100-100
$5 < K < 10$	0-0	0-0	23-4	100-92	100-100	100-100
$K > 10$	0-0	0-0	4-0	92-0	100-93	100-100

153 In order to quantify the influence of K-Value, we approached the problem applying a risk-based  
 154 methodology based on [18]. We implemented the overall risk index ( $I_R$ ) analysis applying the  
 155 concept of expected annual damage [29], being  $I_R$  expressed in euros. We obtained the partial risk  
 156 indexes associated to the maximum reservoir level ( $I_z$ ) and the maximum released outflows ( $I_o$ ). By  
 157 adding  $I_o$  and  $I_z$  we estimated the overall risk index ( $I_R$ ). For Talave, the value of K that optimized  $I_R$   
 158 is 5.25, with a reduction of 8.4% compared with the  $I_R$  associated to VEM (Figure 5). Even though it  
 159 may seem a small reduction, there should be taking into account that applying K-Method has no  
 160 costs associated and the improvement would be applied during the whole dam life.



161 **Figure 3.** Risk indexes for MEV, I-O method and different values of K-Method. Upper subplot  
 162 vertical axis shows  $I_z$ , which is the storage risk index. Middle subplot vertical axis shows  $I_o$ , which is  
 163 the released flow risk index. Lower subplot vertical axis shows  $I_R$ , which is the global risk index.  
 164 Horizontal axis shows the different values of K. The optimum K for  $I_R$  is 5.25.  
 165

## 166 5. Conclusions

167 The proposed K-Method developed in this work improved the Volumetric Evaluation Method  
168 (VEM), which is largely used for operation of gated spillways in Spain. It was shown that the best  
169 K-Value depends on the dam manager interests:

- 170 • Any K-Value adopted (higher than one) reduces the maximum reservoir levels reached in the  
171 dam. Therefore, the adoption of K-Method allows the dam manager to reduce the flood control  
172 volume increasing the useful water volume in the reservoir.
- 173 • For K-Values ranging from one to ten, for the study case, there was an improvement of the VEM  
174 for inflows of return periods higher than 50 years.
- 175 • For return periods of inflows lower than 25 years, K-Method reduces maximum reservoir levels  
176 but increases maximum outflows respect to VEM. Although, the increase of outflows did not  
177 endanger downstream safety.
- 178 • By carrying out a dam risk analysis, a K-Value of 5.25 was the best reducing 8.4% VEM  
179 expected annual damage.


180 The proposed procedure should be applied to other reservoirs and dams in order to recognize  
181 common trends and behaviors.


182 **Acknowledgments:** The authors would like to thank the funds from Fundación José Entrecanales Ibarra in the  
183 framework of the Program “Support program for young professors for doing international stays” and the funds  
184 from the same institution from the Program “Support program for research purposes”.

185 **Author Contributions:** Alvaro Sordo-Ward, Iván Gabriel-Martín, Paola Bianucci, Andrea Morello and Luis  
186 Garrote designed and carried out the experiments, analyzed, discussed and wrote the manuscript.

187 **Conflicts of Interest:** The authors declare no conflict of interest.

## 188 References

- 189 1. Wurbs, R.; *Comparative Evaluation of Generalized River/Reservoir System Models*; Texas Water Resources  
190 Institute: College Station, TX, USA, 2005.
- 191 2. Wang, L.; Nyunt, C.T.; Koike, T.; Saavedra, O.; Nguyen, L.C.; Van Sapt, T.; Development of an integrated  
192 modeling system for improved multi-objective reservoir operation. *Front. Archit. Civ. Eng. China* **2010**, *4*,  
193 47-55, DOI:10.1007/s11709-010-0001-x.
- 194 3. Hossain, M.S.; El-shafie, A. Intelligent systems in optimizing reservoir operation policy: A review. *Water*  
195 *Resour. Manag.* **2013**, *27*, 3387-3407. 
- 196 4. Feng, M.; Liu, P. Spillways scheduling for flood control of Three Gorges Reservoir using mixed integer  
197 linear programming model. *Math. Probl. Eng.* **2014**, *2014*, 1-9.
- 198 5. Pan, L.; Housh, M.; Liu, P.; Cai, X.; Chen, X. Robust stochastic optimization for reservoir operation. *Water*  
199 *Resour. Res.* **2015**, *51*, 409-429.
- 200 6. International Commission on Large Dams (ICOLD); *World Register of Dams*; International Commission on  
201 Large Dams, Paris, France, 2003.
- 202 7. Sordo-Ward, A.; Garrote, L.; Bejarano, M.D.; Castillo, L.G. Extreme flood abatement in large dams with  
203 gate-controlled spillways. *J. Hydrol.* **2013**, *498*, 113-123.
- 204 8. Afshar, A.; Salehi, A. Gated spillways operation rules considering water surface elevation and flood peak:  
205 Application to Karkheh Dam. In *World environmental and water resources congress 2011*, pp 3007-3015.
- 206 9. Molina, M.; Fuentetaja, R.; Garrote, L. Hydrologic models for emergency decision support using bayesian  
207 networks. In *Symbolic and quantitative approaches to reasoning with uncertainty: 8th european conference,*  
208 *ecsqaru 2005, barcelona, spain, july 6-8, 2005. Proceedings*, Godo, L., Ed. Springer Berlin Heidelberg: Berlin,  
209 Heidelberg, 2005; pp 88-99.
- 210 10. Li, Y.; Guo, S.; Quo, J.; Wang, Y.; Li, T.; Chen, J. Deriving the optimal refill rule for multi-purpose  
211 reservoir considering flood control risk. *J. Hydro-Environ. Res.* **2014**, *8*, 248-259.
- 212 11. Girón, F.; Yagüe, J.; Martínez, R. Flood routing in reservoirs base on hydrological forecasting. In  
213 *Proceedings of the Trans Twentieth International Congress on Large Dams, Beijing, China, 2000;*  
214 *Rapports on Question 79, Response 25 (Q79-R25)*; International Commission on Large Dams: Paris,  
215 France, 2000; Volume 4, pp. 403-417.

- 216 12. Loucks, D.; Sigvaldason, O. Multiple-reservoir operation in North America. In: The operation of multiple  
217 reservoir system; edited by Kaczmarek and Kindler; International Institute for Applied System Analysis;  
218 Laxenburg, Austria, 1982.
- 219 13. Needham, J.T.; Watkins, D.W.; Lund, J.R.; Nanda, S.K. Linear programming for flood control in the Iowa  
220 and Des Moines rivers. *J. Water Resour. Plan. Manag.* **2000**, *126*, 118-127.
- 221 14. Raman, H.; Chandramouli, V. Deriving a general operating policy for reservoirs using neural network. *J.*  
222 *Water Resour. Plan. Manag.* **1996**, *122*, 342-347. 
- 223 15. Chang, L.C. Guiding rational reservoir flood operation using penalty-type genetic algorithm. *J. Hydrol.*  
224 **2008**, *354*, 65-74.
- 225 16. Le Ngo, L.; Madsen, H.; Rosbjerg, D. Simulation and optimisation modelling approach for operation of  
226 the Hoa Binh Reservoir, vietnam. *J. Hydrol.* **2007**, *336*, 269-281.
- 227 17. Oliveira, R.; Loucks, D. Operating rules for multireservoir systems. *Water Resour. Res.* **1997**, *33*(4), 839-852.
- 228 18. Bianucci, P.; Sordo-Ward, A.; Perez, J.I.; Garcia-Palacios, J.; Mediero, L.; Garrote, L. Risk-based  
229 methodology for parameter calibration of a reservoir flood control model. *Nat. Hazards Earth Syst. Sci.*  
230 **2013**, *13*, 965-981.
- 231 19. Chang, F.-J.; Chang, Y.-T. Adaptive neuro-fuzzy inference system for prediction of water level in  
232 reservoir. *Adv. Wat. Res.* **2006**, *29*, 1-10.
- 233 20. Chang, L.C.; Chang, F.J.; Hsu, H.C. Real-time reservoir operation for flood control using artificial  
234 intelligent techniques. *Int. J. Nonlin. Sci. Num.* **2010**, *11*, 887-902.
- 235 21. Ishak, W.W.; Ku-Mahamud, K.-R.; Norwawi, N.M. Mining temporal reservoir data using sliding window  
236 technique. *CiiT International Journal of Data Mining Knowledge Engineering* **2011**, *3*, 473-478.
- 237 22. Khalil, A.; McKee, M.; Kemblowski, M.; Asefa, T. Sparse bayesian learning machine for real-time  
238 management of reservoir releases. *Water Resour. Res.* **2005**, *41*.
- 239 23. Mediero, L.; Garrote, L.; Martin-Carrasco, F. A probabilistic model to support reservoir operation  
240 decisions during flash floods. *Hydrolog. Sci. J.* **2007**, *52*, 523-537.
- 241 24. Cuevas Velasquez, V. Modelo de gestión de un embalse en tiempo real durante avenidas basado en redes  
242 bayesianas entrenadas con el método de optimización PLEM. Ph.D. Dissertation, Technical University of  
243 Madrid, **2015**.
- 244 25. Loukas, A.; Quick, M.C.; Russell, S.O. A physically based stochastic-deterministic procedure for the  
245 estimation of flood frequency. *Water Resour. Manag.* **1996**, *10*, 415-437.
- 246 26. Loukas, A. Flood frequency estimation by a derived distribution procedure. *J. Hydrol.* **2002**, *255*, 69-89.
- 247 27. Blazkova, S.; Beven, K. Flood frequency estimation by continuous simulation of subcatchment rainfalls  
248 and discharges with the aim of improving dam safety assessment in a large basin in the czech republic. *J.*  
249 *Hydrol.* **2004**, *292*, 153-172.
- 250 28. Sordo-Ward, A.; Garrote, L.; Martin-Carrasco, F.; Bejarano, M.D. Extreme flood abatement in large dams  
251 with fixed-crest spillways. *J. Hydrol.* **2012**, *466*, 60-72.
- 252 29. Arnell, N.W. Expected annual damages and uncertainties in flood frequency estimation. *J. Water Resour.*  
253 *Plan. Manag.* **1989**, *115*, 94-107.

