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ign-Temperature, Bond, and Environmental Impact Assess-	2
ent of Alkali-Activated Concrete (AAC)	3
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Alkali-activated binder (AAB) has been extensively researched in recent years due 14 to its potential to replace Portland cement (PC) and lower carbon footprint. However, ma-15 jor barriers to its commercialization are related to the inadequate characterization of me-16 chanical properties and long-term durability. The mechanical and durability performance 17 of AAB is highly influenced by its microstructure. There is minimal research on correlat-18 ing the microstructural changes to the specimen-level performance of AAB [1]. Among 19 AAB's primary advantages as a building material is its superior performance at high tem-20 peratures and lower environmental impact [2]. The performance of reinforced concrete to 21 function as a composite at high temperatures is evaluated through its bond strength. Sev-22 eral studies reported the effect of mix proportions, curing conditions, and rebar specifica-23 tions on the bond strength of thermal-cured alkali-activated concrete (AAC) [3-6]. How-24 ever, there is no reported study on the bond strength of ambient cured (fly ash + slag)-25 based AAC. To validate the practical sustainability of AAC, life cycle assessment (LCA) 26 can be used to evaluate the environmental impact. 27

Therefore, the present study evaluates the effect of varying precursor proportion (fly 28 ash: slag varied as 100:0, 70:30, 60:40, and 50:50), activator modulus (Ms, varied as 1.0 and 29 1.4), and high-temperatures (538 °C, 760 °C, and 892 °C) on the mechanical properties and 30 microstructure of AAC. The microstructural characteristics are evaluated using X-ray dif-31 fraction (XRD), Fourier transform infrared spectroscopy (FTIR), and scanning electron mi-32 croscopy coupled with energy-dispersive X-ray spectroscopy (SEM-EDS). The effect of 33 varying precursor proportions and Ms on the mechanical performance of AAC is evalu-34 ated through compressive strength, bond strength, flexural strength, and split tensile 35 strength testing. The performance of AAB at extremely high temperatures is assessed in 36 terms of residual compressive and bond strength. LCA of AAC is conducted using the 37 ReCiPe 2016 methodology. Furthermore, since the commercialization of any novel alter-38 native material depends on cost-effectiveness, a simplified cost analysis is performed. 39

The results from microstructural experiments show the formation of new crystalline 40 phases and decomposition of reaction products when exposed to high temperatures, and 41 they correlate well with the observed mechanical performance. The 28-day compressive 42 strength with slag content is enhanced by 151.8 - 339.7 %, depending on the mix. In ambient conditions, lower Ms improves mechanical performance. When exposed to high temperatures, specimens with a high slag content and a low Ms suffered significant deterioration. AAC with fly ash: slag ratio of 70:30 and Ms of 1.4 is proposed as optimal from the 46

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results obtained in the present study [7]. The results reveal that the biggest impact on 47 climate change comes from transport (45.5 - 48.2 %) and sodium silicate (26.7% - 35.6 %). 48Environmental impact is determined to be primarily influenced by sodium hydroxide. 49 The proposed optimal AAC mix has a global warming potential 42.6 % lower than PC 50 concrete [8]. A comparison with the default procedures in the International Reference Life 51 Cycle Data System (ILCD) handbook reveals that the ReCiPe midpoint approach is more 52 efficient in analyzing all impact categories except freshwater ecotoxicity (FETP) and hu-53 man toxicity potentials (HTP). Evaluation of FETP and HTP is recommended with USEtox 54 [9]. The proposed AAC mix has a higher cost than PC concrete in the present scenario. In 55 contrast, if a carbon tax is enacted, the cost of the proposed AAC mix will rise by only 18.4 56 %, whereas PC concrete prices will rise by 81.7 %. This proposed AAC mix is an environ-57 mentally sustainable replacement for PC concrete specifically intended for applications 58 requiring the superior high-temperature performance of reinforced concrete. 59

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