The 4th International Online Conference on Materials



3-6 November 2025 | Online



Load Effects on the Tribological Response of Zr-Based Bulk Metallic Glasses

Patricia Catalán Wic, Paschal Ateb Ubi, Zheming Ding, Martin Stiehler, Mohamed Kalifa, Muhammad Khan, Konstantinos Salonitis and Konstantinos Georgarakis

Faculty of Engineering and Applied Sciences, Cranfield University, United Kingdom

INTRODUCTION & AIM

Challenges of the space environment [1]



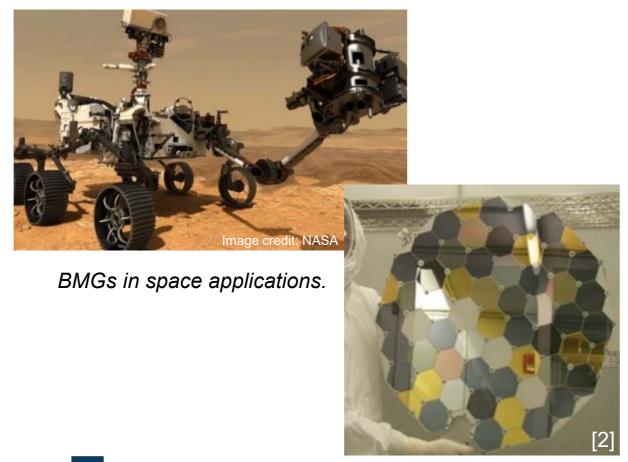
Ultra-high vacuum. Cosmic radiation.



Extreme temperature gradients



ntense mechanical vibrations



Use of BMGs

Exceptional mechanical strength and superior resistance to wear, corrosion, and scratching [3].



AIM AND OBJECTIVES **Examination of friction characteristics of Zr-based BMG**

Comparing results with the existing literature

METHODOLOGY

Sample preparation

Precharacterisation of the samples

XRD testing

Confirming

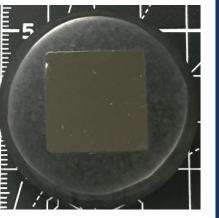
amorphous

structure and

composition

Post-Wear tests characterisation of the samples

- Ball-on-disc
 - Use of XRD techniques
 - SEM-EDS techniques



Resin

embedding

Polishing

BMG and countersurface materials

BMG material (at. %): $Zr_{55}Cu_{30}AI_{10}Ni_5$

Counterpart material: Steel 100Cr6



Counterpart balls

BMG sample

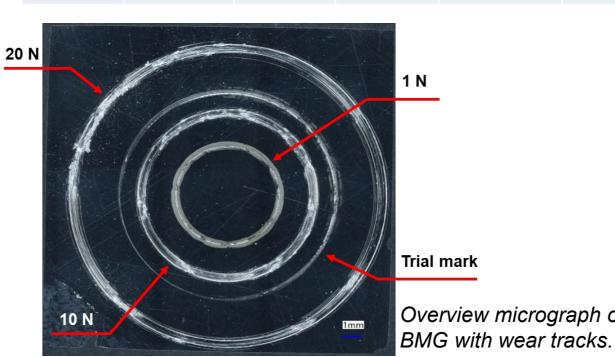
mounted in resin



Tribological setup (TR3 tribometer, Anton Paar, Austria).

Table 1. Friction tests key parameters for Zr-based sample.

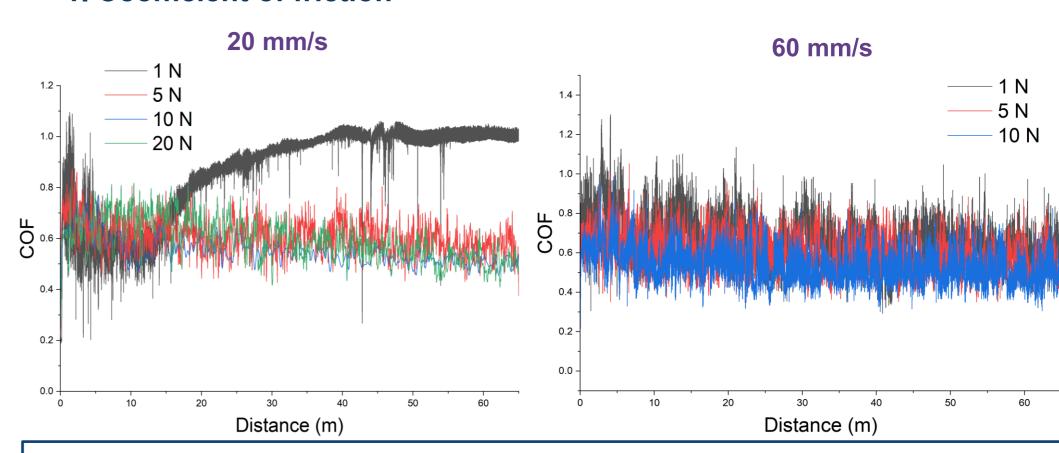
| | | , , | | | • |
|-------------|-----------------|-------------|-------|-----------------|--------|
| Load (N) | Speed (mm/s) | Radius (mm) | RPM | Distance (m) | Cycles |
| 1 | 20 | 3 | 63.7 | 65 | 3448.4 |
| 5 | 20 | 5 | 38.2 | 65 | 2069.0 |
| 10 | 20 | 5 | 38.2 | 65 | 2069.0 |
| 20 | 20 | 9 | 21.2 | 65 | 1149.5 |
| 1 | 60 | 3 | 190.0 | 65 | 3448.4 |
| 5 | 60 | 5 | 114.6 | 65 | 2069.0 |
| 10 | 60 | 7 | 81.8 | 65 | 1477.9 |



Overview micrograph of Zr-based

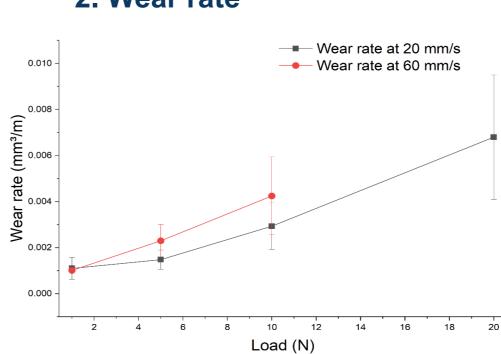
RESULTS & DISCUSSION

1. Coefficient of friction



- Elevate contact pressures → Uniform plastic deformation → More stable wear process [4].
- Low loads and low speed -> Characteristic behaviour due to abrasive and oxidative wear mechanisms [5].

2. Wear rate

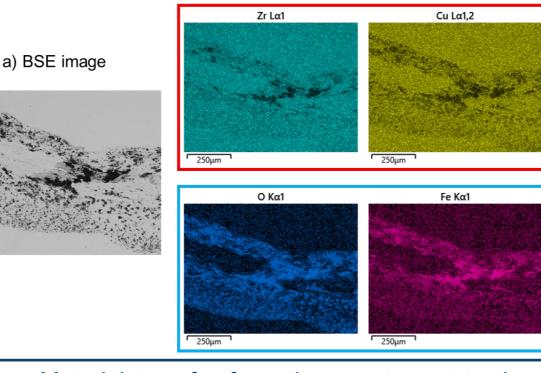


- between Correlation increased contact pressure and the enlargement of width and depth of wear tracks [4].
- Xie et al. present wear rates consistently below 3.0 · 10⁻⁴ mm³/N·m [5].

3. Wear mechanisms

Results for 1 N

b) Elemental maps



- Material transfer from the counterpart to the surface of the base material.
- Zhou et al. found that oxidation can lead to the formation of hard particles.
- Principle wear mechanism: mixture of abrasive and oxidative wear [4].

Results for 5 N, 10 N and 20 N

b) Elemental maps a) BSE image Legend: Elements for steel 100Cr6

- No detectable presence of elements from the counterpart material into the sample.
- Material transfer to the counterpart balls.
- Evolution from abrasive to adhesive wear mechanism [6, 7].

CONCLUSION

Coefficient of friction

- · Inverse relationship between COF and applied load.
- At low loads (1 N) → Bigger initial adaptation phase.
- At high loads (5N, 10 N, 20 N) → More stable COF values and behaviour.

Wear rate evaluation

- BMGs maintain low rates even wear under high contact pressures.
- More influence of sliding speed.

Wear mechanisms

- At low loads (1 N) \rightarrow Abrasive and oxidative wear mechanisms.
- At high loads (5N, 10 N, 20 N) → Adhesive wear mechanism.

FUTURE WORK / REFERENCES

- [1] E. W. Roberts, J. Phys. D: Appl. Phys., <u>45</u> (2012) 503001.
- [2] D. S. Burnett, et al., PNAS <u>108</u> (2011) 19147. [3] C. Suryanarayana, et al, CRC Press, <u>2</u> (2017) 542.
- [4] Z. Zhou, et al, Tribology International, <u>197</u> (2024) 109763.
- [5] C. Xie, et al, Journal of Non-Crystalline Solids, 646 (2024) 123266. [6] T. Rose, Cranfield University, 2005.
- [7] Y. Wang, et al, Materials & Design, <u>111</u> (2016) 213-221.