

Mathematical Modeling and Free Vibration Analysis of Nonhomogeneous Nanobeams with Axially Varying Nonlocal Parameter

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INTRODUCTION & AIM

Introduction:

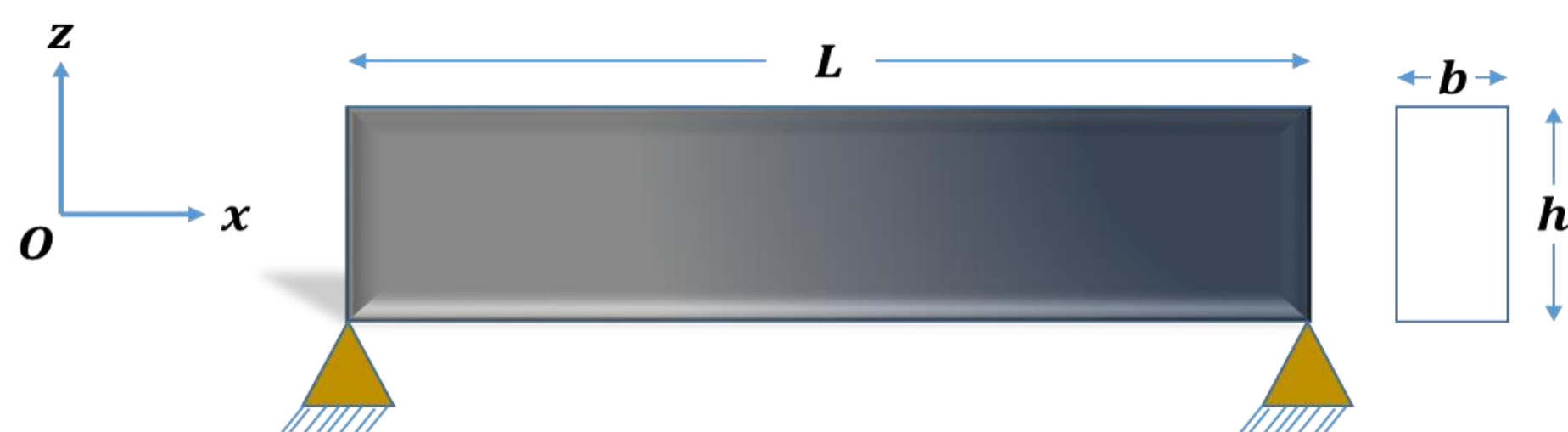
- Nonhomogeneous nanobeams, particularly axially functionally graded (AFG) nanobeams, possess continuously varying material properties, making them suitable for advanced nano-engineering applications.

Research Gap:

- Most existing studies assume a constant nonlocal parameter throughout the nanobeam.
- In practical AFG nanobeams, the nonlocal parameter may also vary along the grading direction.

Objective:

- Develop a vibration model for axially FG nanobeams with a linearly varying nonlocal parameter.
- Investigate the effects of power-law exponent (k), variable nonlocal parameters (a , b), and material gradation on the natural frequencies.



METHOD

Material Properties [1, 2]:

Young's modulus: $E(x) = E_l V(x) + E_r (1 - V(x))$,

Mass density: $\rho(x) = \rho_l V(x) + \rho_r (1 - V(x))$,

where the volume fraction $V(x) = \left(1 - \frac{x}{L}\right)^k$, subscripts l and r denote the left and right sides of the nanobeam, and k is the power-law exponent (non-negative).

Variable Nonlocal Parameter [2]:

$$\mu(x) = a + bx,$$

where a and b are constants.

The maximum strain (S) and kinetic (T) energies of the Euler-Bernoulli AFG nanobeam incorporating Eringen's nonlocal theory are expressed as [2]:

$$S_{max} = \frac{1}{2} \int_0^L \left(J_0 \left(\frac{dU_0}{dx} \right)^2 - J_1 \frac{d^2 W_0}{dx^2} \frac{dU_0}{dx} - \omega^2 (\mu(x))^2 \left(I_0 \left(\frac{dU_0}{dx} \right)^2 - I_1 \frac{d^2 W_0}{dx^2} \frac{dU_0}{dx} \right) - J_1 \frac{dU_0}{dx} \frac{d^2 W_0}{dx^2} + J_2 \left(\frac{d^2 W_0}{dx^2} \right)^2 + \omega^2 (\mu(x))^2 \left(I_0 W_0 \frac{d^2 W_0}{dx^2} + I_1 \frac{dU_0}{dx} \frac{d^2 W_0}{dx^2} - I_2 \left(\frac{d^2 W_0}{dx^2} \right)^2 \right) \right) dx,$$

$$T_{max} = \frac{\omega^2}{2} \int_0^L \left(I_0 (U_0^2 + W_0^2) - 2I_1 U_0 \frac{dW_0}{dx} + I_2 \left(\frac{dW_0}{dx} \right)^2 \right) dx.$$

where

$$(J_0, J_1, J_2) = \int_{-\frac{h}{2}}^{\frac{h}{2}} E(x)(1, z, z^2) dz, (I_0, I_1, I_2) = \int_{-\frac{h}{2}}^{\frac{h}{2}} \rho(x)(1, z, z^2) dz$$

Implementation of Rayleigh-Ritz Method:

Here, the values of natural frequency ω are found using the Rayleigh-Ritz method. In this approach, the displacement functions $U_0(x)$ and $W_0(x)$ are expressed as (for simply-supported boundary conditions) [2]:

$$U_0(x) = x(L-x) \sum_{i=1}^N c_i x^{i-1}, \quad W_0(x) = x(L-x) \sum_{j=1}^N d_j x^{j-1},$$

The Rayleigh Quotient is obtained by equating the expressions for the maximum strain energy with the maximum kinetic energy. Then by partially differentiating it by c_i and d_j , a system of $2N$ linear equations is generated, which is represented as:

$$([K] - \lambda^2 [M])\{\Delta\} = 0,$$

where $[K]$ and $[M]$ are stiffness and inertia matrices, respectively, $\{\Delta\}$ denotes the column vector containing c_i 's and d_j 's, and the frequency parameter λ is defined by $\lambda = \omega L^2 \sqrt{(\rho_l A)/(E_l I)}$, where I is the moment of inertia.

RESULTS & DISCUSSION

| k | a | b | λ_1 | λ_2 | λ_3 | λ_4 |
|-----|-----|-----|-------------|-------------|-------------|-------------|
| 0 | 0 | 0 | 9.8692 | 39.4719 | 88.7936 | 157.8099 |
| | 0 | 0.2 | 9.3522 | 31.9999 | 60.0851 | 90.0130 |
| | 0.1 | 0.2 | 8.2992 | 24.0160 | 40.6329 | 57.1498 |
| | 0.1 | 0.3 | 7.6467 | 20.5155 | 33.6940 | 46.7374 |
| 1 | 0 | 0 | 7.0305 | 28.1832 | 63.4332 | 112.7592 |
| | 0 | 0.2 | 6.5858 | 21.8572 | 40.1720 | 59.4307 |
| | 0.1 | 0.2 | 5.7952 | 16.3291 | 27.3910 | 38.3995 |
| | 0.1 | 0.3 | 5.2750 | 13.7990 | 22.4935 | 31.1140 |
| 3 | 0 | 0 | 5.7321 | 23.7285 | 53.7589 | 95.8016 |
| | 0 | 0.2 | 5.3893 | 18.6316 | 34.6167 | 51.4234 |
| | 0.1 | 0.2 | 4.7542 | 13.9012 | 23.4582 | 32.9544 |
| | 0.1 | 0.3 | 4.3458 | 11.7645 | 19.2830 | 26.7355 |
| 5 | 0 | 0 | 5.4117 | 22.4032 | 50.8812 | 90.7772 |
| | 0 | 0.2 | 5.1055 | 17.7720 | 33.2388 | 49.5475 |
| | 0.1 | 0.2 | 4.5150 | 13.2701 | 22.4730 | 31.6111 |
| | 0.1 | 0.3 | 4.1416 | 11.2556 | 18.5074 | 25.6866 |

It is observed that higher values of the power-law exponent result in lower frequency parameter values. Similarly, increasing the nonlocal parameter (by increasing a , b , or both) also reduces the frequency parameters.

CONCLUSION

- A vibration model for axially FG nanobeams with variable nonlocal parameter is developed.
- Rayleigh-Ritz method is implemented to obtain the values of frequency parameters.
- Future research could explore more complex boundary conditions, multi-scale modeling, and the impact of environmental factors.

FUTURE WORK / REFERENCES

- Alshorbagy, A. E., Eltahir, M. A., & Mahmoud, F. (2011). Free vibration characteristics of a functionally graded beam by finite element method. *Applied mathematical modelling*, 35(1), 412-425.
- Gartia, A. K., & Chakraverty, S. (2025, January). Effect of Variable Nonlocal Parameter on the Free Vibration of Axially Functionally Graded Nanobeams. In *International Conference on Computational Mathematics and Applications* (pp. 293-303). Singapore: Springer Nature Singapore.