



Proceedings

Application of Torque Transducer and Rotary Encoder in a Hardware-in-the-Loop Wind Turbine Emulation [†]

Felipe Ozawa *, Marco Rocha, Guilherme Lucas, Wallace Souza and Andre Andreoli

Department of Electrical Engineering, São Paulo State University (UNESP), Bauru, Brazil; <u>marco.rocha@unesp.br</u> (M.R.) guilherme.beraldi@unesp.br (G.L.) Wallace.g.souza@unesp.br (W.S.) andre.andreoli@unesp.br (A.A.)

- * Correspondence: lipeozawa@outlook.com; Tel.: +55 11 98320-4827
- † Presented at the 6th International Electronic Conference on Sensors and Applications, 15–30 November 2019; Available online: https://ecsa-6.sciforum.net/

Published: 14 November 2019

Abstract: Wind energy is one of the most promising forms of renewable energy. For the constant evolution of power generation technology, the use of sensors is fundamental to the development of wind turbine emulators. A wind turbine emulator allows tests and evaluations of a wind power system, regardless of weather conditions. Therefore, to further improve this technology, this work focuses on the application of a torque transducer and a rotary encoder for the implementation of a closed-loop wind turbine emulator. The sensors provide the torque and speed feedback signals to the computational model so that the model could plot the power curves and produce the set point voltage used by a variable-frequency drive (VFD) to control a three-phase induction motor (TIM). The emulator was implemented using a control algorithm designed on LabVIEW with a NI 6211 for data acquisition. Finally, the system emulates the behaviour of a wind turbine, considering the variations in wind speed, aerodynamic phenomena, load effects, and pitch angle. Experimental results demonstrated the effectiveness of using the TIM-VFD assembly for emulating a wind turbine since the wind turbine emulator behaved like a wind turbine in real-time.

Keywords: Wind turbine emulator; LabVIEW; Wind Energy; Torque transducer; Rotary encoder

1. Introduction

Increasing demand for electrical energy, driven by the development of the world economy, requires new energy strategies for competitiveness in modern market. Conventional energy sources such as oil, coal and natural gas present significant financial risks as they have constant price fluctuations. In addition, there is a steady increase in worldwide concern about global warming and climate change, caused by the increase in carbon dioxide emissions. In the other hand, the development of renewable energy sources stand out as an alternative to mitigate the setbacks of conventional power generation [1–4]

The expansion of wind power generation has led to a significant increase in wind energy conversion systems (WECS) research. As the wind is a stochastic variable, the experimental studies regarding WECS are not always feasible. Thus, wind turbine emulators (WTE) becomes essential for the technological development of the area, once they are independent of the intermittent nature of the wind. In addition, WTEs are capable of reproducing the same aerodynamic behaviour of real wind turbines [5–7].

Proceedings **2019**, 2019 2 of 6

However, to implement a closed-loop emulator, it is necessary to have feedback on some operational values. To accomplish that, it is essential the application of transducers to provide data from the test bench to the computational model. Therefore, the focus of this paper is to apply a torque transducer and a rotary encoder for signal acquisition aiming to develop a hardware-in-the-loop WTE.

In order to achieve the proposed scope, the test bench was assembled using a three-phase induction motor TIM driven by a variable-frequency drive (VFD). A DC generator was coupled to the TIM and connected to a resistive load, aiming to apply different torque levels. To measure the angular speed and torque levels it was used a rotary encoder and a torque meter. All the aerodynamic characteristics of a real wind turbine were considered in the LabVIEW model. Finally, it was used a DAQ NI 6211 for acquire the signal provided by the two sensors and to set the control signal for the VFD.

The results showed that the proposed WTE was able to provide precise and exact values for torque and power curves, matching a real wind turbine. There are seven sections in this works. Section 2 presents the aerodynamic model of the wind turbine. Section 3 outlines the use of the torque transducer. In Section 4, the rotary encoder is detailed. The Section 5 is dedicated to materials and methods. The results are discussed in Section 6. At last, the conclusions about this work are presented in Section 7.

2. Aerodynamic Model

The principle of working of wind turbine is based on aerodynamics. The turbine's aerodynamic output power is given as [8,9]:

$$P = \frac{1}{2}\rho.A.C_p(\lambda,\beta)v^3$$
 (1)

Where v is the velocity of air, C_p is the power coefficient, ϱ is the air density, and A is the area swept by rotor blades. The conversion efficiency or C_p is the ratio of available wind energy to the turbine shaft mechanical energy. It is a function of tip speed ratio (λ) and pitch angle (β) which is given as.

$$\lambda = \frac{V_{tg}}{v} = \frac{\omega_T R}{v} \tag{2}$$

where V_{tg} is the tangential velocity, v is the velocity of air, ωT in (rad/s) is the rotor angular velocity. The conversion efficiency or C_p (λ,β) is given as:

$$C_{p}(\lambda, \beta) = c_{1} \left(\frac{c_{2}}{\lambda_{i}} - c_{3}\beta - c_{4}\beta^{c_{5}} - c_{6}\right) e^{-\frac{c_{7}}{\lambda_{i}}} + c_{8}\lambda$$
(3)

with λ_i given as:

$$\frac{1}{\lambda_{i}} = \frac{1}{\lambda + c_{9}\beta} - \frac{c_{10}}{\beta^{3} + 1} \tag{4}$$

The coefficients are given as [10]:

Table 1. Empiric coefficients for aerodynamic model.

Coefficient	c_1	c_2	c_3	c_4	c_5	<i>c</i> ₆	c ₇	<i>c</i> ₈	C 9	c ₁₀
Heier	0.5	116	0.4	0	0	5	21	0.0068	0.08	0.035

The mechanical torque of a wind turbine is given by the ratio between the mechanical power and the angular speed of wind turbine:

$$T = \frac{1}{2} QAC_p(\lambda, \beta) \frac{V_w^2}{\omega_T}$$
 (5)

The angular speed of the wind turbine can be obtained from the one mass model, which considerate the inertia J, the mechanical torque T and the electromagnetic torque Te:

Proceedings **2019**, 2019 3 of 6

$$\frac{d\omega_{\rm T}}{dt} = \frac{1}{I} (T - T_{\rm e} - B\omega_{\rm T}) \tag{6}$$

3. Torque Transducer.

The device used in this work is the MT-103 from SODMEX (Figure 1). The parameters provided by the manufacturer were presented in Table 2. Once the maximum output voltage generated by the torque transducer is 20.9 mV, it was used a load cell to amplify the measured signal. This type of sensor assess the torque values using four strain gauges attached to the meter shaft. The gauges are connected in order to form a Wheatstone bridge circuit. The deformation of the strain gauges causes a resistance alteration, which leads to different voltage levels in the bridge output. These voltage levels have a direct relation to the torque applied to the shaft [11].

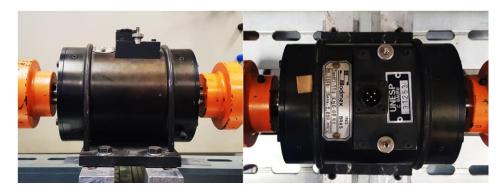


Figure 1. Torque transducer.

Table 2. Transducer parameters.

Parameter	Value			
Maximum torque	50 N.m			
Sensitivity	$\pm~2.09~mV/V$			
Input voltage (DC)	10 V			

4. Rotary Encoder

The rotary encoder used in the WTE was the H38S400B model (Figure 2). This equipment generates 1600 pulses per minute for quadrature outputs, which allows the direction of TIM rotation to be determined. Additionally, the angular speed can be obtained by processing the pulse signal [12].



Figure 2. Rotary encoder.

Proceedings **2019**, 2019 4 of 6

4. Materials and Methods

In this section, the steps taken to accomplish the WTE are presented. The Figure 3 shows a diagram of the experimental bench and signal acquisition.

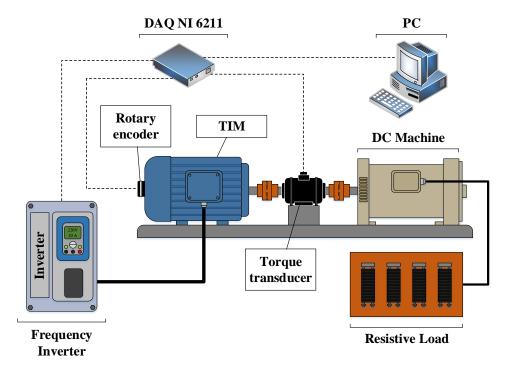


Figure 1. Setup Diagram

4.1. Test Bench Setup

Initially, the 4 hp TIM was coupled to a DC machine and both of them were firmly bolted to the test bench (Figure 4). The induction motor was driven by the VFD CFW-08 from WEG, which was controlled by a DAQ board NI 6211. The VDF setpoint was generated by an aerodynamic model using two inputs, torque and angular speed. The DC machine current was adjusted using a variable resistive load in order to require different power levels from the TIM, allowing to draw a power vs. angular speed curve.

4.2. Sensors and Acquisition Board

The encoder and torque meter signals were acquired by the same DAQ used to control the VFD. The NI 6211 board has 16 analogue inputs and 16 digital I/O with 16 bits of resolution [13]. The sample rate is 250 kS/s, which satisfies the Nyquist theorem for this work. The rotary encoder was attached to the back of the motor shaft. In addition, the torque meter was coupled between the two machines as shown in Figure 4.



Figure 4. TIM coupled to a CC machine.

Proceedings **2019**, 2019 5 of 6

5. Results

Aiming to analyse the effectiveness of the proposed wind turbine emulator, a scenario of wind speed variation was performed. The experimental validation of the WTE was performed by comparing the experimental results obtained by the test bench with the theoretical aerodynamic behaviour of a real wind turbine.

The results were analysed by the characteristics curves of power vs. angular speed and torque vs. angular speed. Therefore, a 1.8 kW wind turbine with a 1.5 gearbox, 1.1 m radius and 1.225 kg/m³ air density was chosen. For experimental validation, three different wind speeds were applied: 8m/s, 9m/s and 10 m/s. In addition, the pitch angle was fixed at 0° .

The theoretical characteristics of power vs. angular speed and torque vs. angular speed of a real wind turbine is shown in Figure 5. This same test was performed for the proposed WTE and its behaviour is shown in Figure 6.

The comparison between Figure 5 and Figure 6 shows the effectiveness of the wind turbine emulator once the characteristics curves of theoretical and experimental wind turbine presented the same behaviour.

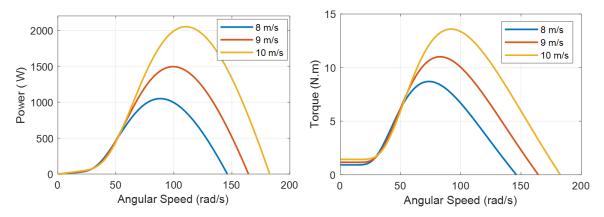


Figure 5. WTE theoretical curves.

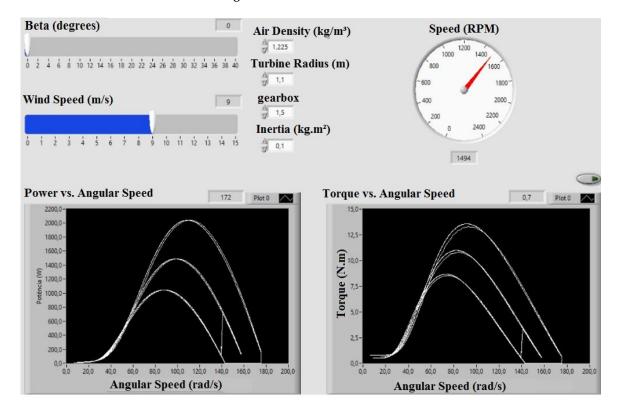


Figure 6. WTE interface and results.

Proceedings **2019**, 2019 6 of 6

6. Conclusion

The proposed system was able to follow the dynamics of a wind turbine with variations of resistive load. In this case, it was possible to obtain the characteristic curves for different wind speeds, which were compared with the theoretical values of a real wind turbine. Therefore, experimental results demonstrated the effectiveness of using the TIM-VFD assembly, once the WTE presented the same behaviour of power vs. angular speed and torque vs. angular speed than theoretical wind turbine.

Author Contributions: all authors contributed in writing, proofreading, and providing suggestions for the improvement of the paper.

Conflicts of Interest: The authors declare no conflict of interest.

References

- Moussa, I.; Bouallegue, A.; Khedher, A. New wind turbine emulator based on DC machine: hardware implementation using FPGA board for an open-loop operation. *IET Circuits Devices Syst.* 2019, 13, 896– 902.
- 2. Gan, L.K.; Shek, J.K.H.; Mueller, M.A. Modeling and Characterization of Downwind Tower Shadow Effects Using a Wind Turbine Emulator. *IEEE Trans. Ind. Electron.* **2017**, *64*, 7087–7097.
- 3. Averous, N.R.; Stieneker, M.; Kock, S.; Andrei, C.; Helmedag, A.; De Doncker, R.W.; Hameyer, K.; Jacobs, G.; Monti, A. Development of a 4 MW Full-Size Wind-Turbine Test Bench. *IEEE J. Emerging Sel. Top. s in Power Electron.* **2017**, *5*, 600–609.
- 4. Guerrero, J.M.; Lumbreras, C.; Reigosa, D.D.; Garcia, P.; Briz, F. Control and Emulation of Small Wind Turbines Using Torque Estimators. *IEEE Trans. Ind. Appl.* **2017**, *53*, 4863–4876.
- 5. Sirouni, Y.; Hani, S.E.; Naseri, N.; Aghmadi, A.; Harouri, K.E. Design and Control of a Small Scale Wind Turbine Emulator with a DC Motor. In Proceedings of the 2018 6th International Renewable and Sustainable Energy Conference (IRSEC); 2018; pp. 1–6.
- Nambiar, A.S.; Raja, G.M.; Harindran, K.; Rajan, P.; Sankar, S.S.; Sankar, V.C.J. Design and development of a maximum power point tracker and its testing setup for wind energy conversion system with laboratory level devices. In Proceedings of the 2017 International Conference on Technological Advancements in Power and Energy (TAP Energy); 2017; pp. 1–5.
- 7. Benaaouinate, L.; Khafallah, M.; Mesbahi, A.; Martinez, A. Development of a useful wind turbine emulator based on permanent magnet DC motor. In Proceedings of the 2017 14th International Multi-Conference on Systems, Signals Devices (SSD); 2017; pp. 44–48.
- 8. Karabacak, M. A new perturb and observe based higher order sliding mode MPPT control of wind turbines eliminating the rotor inertial effect. *Renewable Energy* **2019**, *133*, 807–827.
- 9. Sewwandi, K.M.G.Y.; Senarathna, T.S.S.; Lakshika, K.A.H.; Wong, V.Y.; Hemapala, K.T.M.U.; Lucas, J.R.; Porawagamage, G.D. Wind turbine emulator for a microgrid. In Proceedings of the 2017 Innovations in Power and Advanced Computing Technologies (i-PACT); 2017; pp. 1–6.
- 10. Llano, D.X.; McMahon, R.A. Modelling, control and sensorless speed estimation of micro-wind turbines for deployment in Antarctica. *IET Renew. Power Gener.* **2018**, *12*, 342–350.
- 11. Hoffmann, K. Applying the Wheatstone bridge circuit; HBM Germany, 1974;
- 12. Hagiwara, N.; Suzuki, Y.; Murase, H. A method of improving the resolution and accuracy of rotary encoders using a code compensation technique. *IEEE Trans. Instrum. Meas.* **1992**, *41*, 98–101.
- 13. USB-6211 Specifications National Instruments Available online: http://www.ni.com/pdf/manuals/375195d.pdf (accessed on Oct 22, 2019).



© 2019 by the authors; licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC-BY) license (http://creativecommons.org/licenses/by/4.0/).