



Proceedings Experimental Evaluation of the Issuer Coefficients of a Locality in Ecuador

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Abstract: The objective of this research is to evaluate the variation of the discharge coefficients of the emitters provided by the commercial companies. This includes coefficients obtained in an experimental bench test. The testing assembly was composed of the supply unit, the filter, the adduction line, the distribution lines, the selected emitters, analogue volume meters and digital sensors to obtain the pressure and flow rate. There were two sectors in the plot, the first was low-pressure sector operated by gravity and the second was high-pressure, supplied by a pump. Nine types of emitters (drippers, micro-sprinklers, sprinklers) were used, including some self-compensating ones. Using an electronic data acquisition system, the pressure and flow rate are obtained and used to generate the characteristic curves of emitters. This makes it possible for the characteristic curves to be determined by using the discharge equations of the emitters selected for this study. Subsequently, the network is modelled using the discharge coefficient and exponent obtained for each emitter. The results show which of the tested emitters meet the technical specifications of the local suppliers.

Keywords: emitters (drippers, micro-sprinklers, sprinklers); Ke discharge coefficients; comparative analysis

1. Introduction

With 767 million people still living in extreme poverty (Ending poverty and hunger by investing in agriculture and rural areas, 2017), investments in agriculture prove very effective in reducing economic hardship. This is one reason why there exists an urgent need to promote innovative technologies for the optimal management of irrigation systems and water resources. It is possible for an irrigation system to be dynamically adjusted to the water demand of each crop (Fernandes et al., 2020), by implementing a network of pipes terminated by emitters that deliver water to the soil as droplets or spray (Cruz-Mayo & Ariosto., 2022). Irrigation sprinklers are the most basic component of such a system and vary from one-piece sprinklers to highly complex designs such as a transmitter with multiple assemblies working together as a single unit (Pazmiño-Mayorga et al., 2017). It is important to understand the features of each emission source to best design a solution to meet the water demand of a crop (Liotta M, 2000).

The main emitters selected for field work in this research are sprinklers, micro-sprinklers, and drippers. High pressure sprinklers are designed to cover large irrigation diameters from 20 m to 40 m and typically require operation at more 20 m water column (mwc). Micro-sprinkler allows water to be discharged to the ground in a circular pattern, and the irrigation diameter is smaller: from 3 m to 15 m. These work from 10 mwc to 35 mwc.

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Copyright: © 2022 by the authors. Submitted for possible open access publication under the terms and conditions of the Creative Commons Attribution (CC BY) license (https://creativecommons.org/licenses/by/4.0/). Compared to sprinklers and micro-sprinklers, drippers are designed to use water most efficiently from 4 mwc to 25 mwc and maintaining optimal plant humidity (Chamba et al., 2020).

The discharge coefficient Ke is determined as a function of the flow rate and working pressure of the emitter. Ke is fundamental for the proper modelling and control of irrigation systems because it includes both the hydraulic performance of the emitter and its discharge under different pressure conditions (Rodríguez et al., 2018), which ultimately reflects the amount of water delivered to the plant. To obtain homogeneous and high-yield of agricultural products, the available water resources must be used effectively (Muñoz R., 2004).

2. Methods

To explain the methodology, the Mini Woobler micro-sprinkler (1/2'') was used, and the following sequence was applied:

2.1. Recognition and Topographical Mapping

This mainly includes field work, identifying and analyzing the characteristics of the study area. A topographical mapping of the study area was conducted to obtain the topographical features of the sector and to establish the final topological structure of the irrigation system pipe network.

2.2. Network Design

For the study network design, the hydraulic gradient method was used. The design and analysis considered the nominal flow demand of the emitter with the highest hydraulic requirements, and the continuous and local losses in the network. As a result, two networks were created. One was low pressure gravity fed and the other used a high-pressure pumping system.

2.3. Installation of Irrigation System with the Emitters to Be Evaluated and Calibration of Electronic Equipment

It consisted of the installation of the materials and equipment of the study network followed by the calibration of the sensors used to measure the pressure and flow rate of the emitters deployed.

2.4. Obtaining Experimental Data

The pressure and flow data were measured electronically, and the logged values were constantly double-checked with analogue measurements. The data collection time for each emitter was 30 min, in the following order (Figure 1):

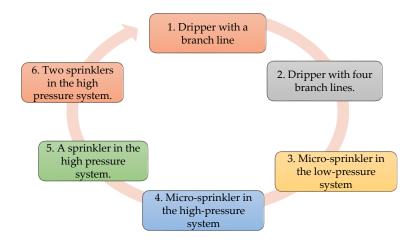


Figure 1. Obtaining experimental data.

2.5. Calculation and Analysis of Ke Discharge Coefficients of Selected Emitters

To calculate the emitter Ke flow coefficient, the flow equation proposed by Keller and Karmeli (1974) Equation (1) was used:

$$CU = 100 * \frac{q_{25\%h}}{q_{medd}} \tag{1}$$

where *CU* is the coefficient of uniformity (application) $q_{25\%h}$ indicates the average flow rate of the 25% of the emitters with the lowest flow rate (L/h) and q_{medd} is the average design flow rate (L/s).

For MegaNet nozzle (orange 650 L/h), the following specification was available.

Table 1. Data.

| DATA | | | | |
|--------|--|--|--|--|
| 29.832 | | | | |
| 0.2034 | | | | |
| | | | | |

Replacing in the discharge equation of this emitter Equation (2)

$$Q = Ke * P^{\chi} \tag{2}$$

where Q is the discharge flow rate of the emitter in (L/h), *Ke* is the discharge coefficient of the emitter (dimensionless), *P* is the hydraulic inlet pressure of the water at the emitter, in mwc or KPa and finally \times is the discharge exponent (dimensionless).

Replacing values in Equations (1) and (2), the value of Ke Equation (3) is obtained:

$$Ke = 134.037 \left(\frac{l}{h * mca}\right) \tag{3}$$

2.6. Modelling of the Ke Coefficient of Sprinklers and Micro-Sprinklers in the Study Network Using the Free Software EPANET 2.0 v.E.

The K_e coefficients obtained from the emitter discharge equation were used, and the Epanet 2.0 software tool was used to model the research network with the implementation of sprinklers, micro-sprinklers, and drippers to analyze their hydraulic performance (Figure 2) (Tello, 2016) (Tello, 2016).

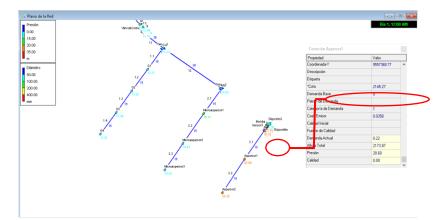


Figure 2. Analysis network modelled with calculated discharge coefficients.

2.7. Obtaining the Real Flow Rate Discharged by the Emitters in the Laboratory and Comparing it with That Obtained by Sensors

The realized flow rate was verified using the electronic data acquisition system, and the actual flow rate discharged by each emitter was quantified in the laboratory. For this purpose, the volume of water delivered by the emitter was collected over a period of 10 min.

3. Results and Discussion

3.1. Results

Table 1 shows the factory and field data of the Mini Woobler micro-sprinkler and the discharge coefficients obtained. The coefficients show greater variation if the working pressure is very low or very high. It is therefore recommended to work at pressures between 1.5 bar and 2.5 bar. With the pressure and flow data obtained in the field, the characteristic equation for this emitter is obtained (Equation (4)):

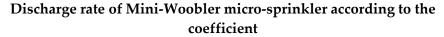
$$Q = 0.0154 * P^{0.546} \tag{4}$$

Equation (4) represents the flow rate obtained under different pressures; the exponent discharge is close to 0.5 so it operates in a turbulent regime.

| Micro-Sprinkler: MINI WOOBLER (1/2" VERTICAL) | | | | | |
|---|--------|--------|--------|--------|--------|
| Factory Pressure (bar) | 1 | 1.5 | 2 | 2.5 | 3 |
| Factory pressure (mwc) | 10.197 | 15.296 | 20.395 | 25.494 | 30.592 |
| Theoretical factory flow rate (L/s) | 0.060 | 0.070 | 0.080 | 0.090 | 0.100 |
| Theoretical Ke coefficient (L/h*mwc) | 67.641 | 64.433 | 63.772 | 64.170 | 65.087 |
| Discharge exponent (x) | | | 0.500 | | |
| Field pressure (mwc) | 13.703 | 13.974 | 14.420 | 34.564 | 35.390 |
| Field flow rate (L/s) | 0.0637 | 0.0649 | 0.0674 | 0.1045 | 0.1085 |
| Ke field coefficient (L/h*mwc) | 61.982 | 62.536 | 63.866 | 63.970 | 65.673 |
| Ke factory coefficient (L/h*mwc) | 65.435 | 65.265 | 64.984 | 61.936 | 61.829 |
| Percentage of variation (%) | 5.57 | 4.36 | 1.75 | 3.18 | 5.85 |

Table 1. Ke discharge coefficients of Mini Woobler Micro Sprinkler (1/2").

Figure 3 shows the difference between the discharge flow rate values obtained in the field and the flow rate values provided by the manufacturer operating at various working pressures, resulting in a minimum variation of 1.75% and a maximum variation of 7.46%.



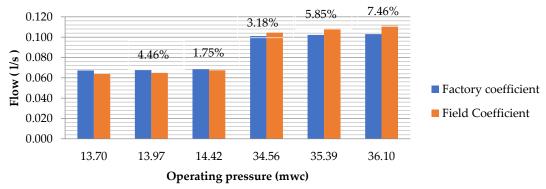
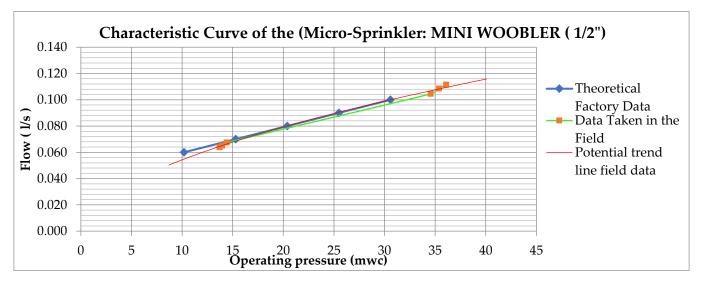


Figure 3. Comparison of micro-sprinkler discharge rates Mini Woobler.



The characteristic curve and trend line of field-measured flow and pressure of the 1/2" Mini Woobler micro-sprinkler (Figure 4) showed a significant variation especially when the working pressure of the emitter was either very low or very high.

Figure 4. Comparison of characteristic curve of Mini Woobler micro sprinkler (factory and field data).

3.2. Discussion

3.2.1. Variation of Discharge Coefficients of Used Emitters

Figure 5 shows the types of drippers that were analysed and the maximum and minimum percentage of variation between the *Ke* discharge coefficients which were obtained with the factory data and those resulting in the field. It was verified that the self-compensating PCJ dripper presents less variation in the data provided by the manufacturer.



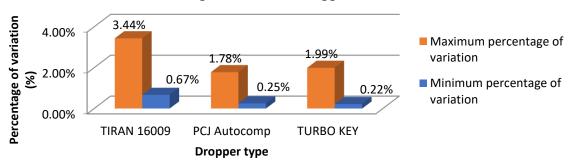
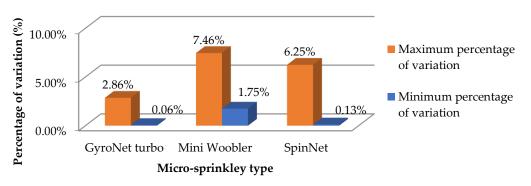


Figure 5. Comparison between drippers according to the percentage variation of the coefficients obtained.

Figure 6 shows the maximum and minimum percentage variation of Ke values considering the factory and field data for all types of micro-sprinklers that were examined. It was observed that the GyroNet turbo micro-sprinkler is the most efficient and presents the lowest percentage of variation.



Comparison between micro-sprinklers

Figure 6. Comparison of micro-sprinklers according to the percentage variation of the coefficients obtained.

Figure 7 shows the maximum and minimum percentage variation that each type of sprinkler presented with respect to their discharge coefficients and a comparison was made between them. As a result, it was found that the Naan 5022 sprinkler has less variation between the data obtained in the field and the data provided by the manufacturer.

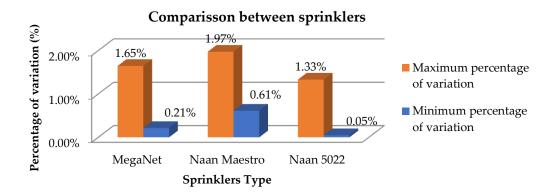


Figure 7. Comparison between sprinklers according to the percentage variation of the coefficients obtained.

3.2.2. Modelling Results in Epanet 2.0 Discharge Coefficients

Table 3 shows the results of the flow variation of the emitters tested in the field and the flows modelled in Epanet 2.0 software. The variation is minimal, so it is affirmed that the modelling carried out with the discharge coefficients calculated correctly represents the hydraulic performance of the emitters in the field.

Table 3. Comparison of field measured and modelled discharge flow rates in Epanet 2.0 micro sprinklers.

| FLOW COMPARISON (FIELD VS EPANET 2.0) | | | | |
|---------------------------------------|-----------------------------|--------------------------|-------------------|-----------|
| Micro-Sprinkler Type | Operating Pressure (mwc) | Field Flow Rate (L/s) | Epanet Flow (L/s) | Variation |
| Correction to the second second | 15.01 | 0.048 | 0.05 | 4.44% |
| GyroNet turbo | 36.03 | 0.073 | 0.07 | 4.29% |
| Mini Woobler | 13.97 | 0.065 | 0.06 | 7.60% |
| | 35.39 | 0.109 | 0.11 | 1.36% |
| SpinNet | 16.51 | 0.016 | 0.02 | 6.94% |

| 36.75 | 0.022 | 0.02 | 9.65% |
|-------|-------|------|-------|
| | | | |

Table 4 shows the comparison between the flow rates measured in the field and those resulting from the modelling in the Epanet 2.0 software. These data show a minimal variation between them, which allows us to confirm that the Ke discharge coefficients calculated are suitable for obtaining accurate results when modelling the hydraulic characteristics of an irrigation network.

Table 4. Comparison of field measured and modelled discharge flow rates in Epanet 2.0 sprinklers.

| FLOW COMPARISON (FIELD VS EPANET 2.0) | | | | | |
|---------------------------------------|--------------------------------|--------------------------|----------------------|-----------|--|
| Sprinkler Type | Operating Pressure (mwc) | Field Flow Rate (L/s) | Epanet Flow (L/s) | Variation | |
| MegaNet | 29.83 | 0.20 | 0.2 | 1.65% | |
| | 33.35 | 0.21 | 0.21 | 0.96% | |
| Naan Maestro | 28.63 | 0.22 | 0.21 | 2.96% | |
| | 33.20 | 0.23 | 0.23 | 0.23% | |
| Naan 5022 | 26.15 | 0.250 | 0.25 | 0.10% | |
| | 31.77 | 0.277 | 0.28 | 1.21% | |

4. Conclusions

Nine types of emitters were evaluated (three sprinklers, three micro sprinklers and three drippers). The pressure heads with the lowest percentage variation between the technical specifications of the catalogue and the data obtained in the field were determined, including Naan 5022 head, the maximum percentage variation was 1.33%, GyroNet micro head, the maximum variation value corresponded to 2.86% and the self-compensating dripper PCJ obtained a maximum variation of 1.78%. Moreover, it was possible to obtain their corresponding discharge equations.

Using the flow and pressure data of each emitter, characteristic curves were generated. It was evident that the flow coefficients are close to 0.5, which indicates that these nozzles worked in a turbulent state for the sprinklers and micro-sprinklers and some drippers tested. The PCJ dripper is a self-compensating type, and its characteristic curve was different. Its discharge rate value was close to zero and its characteristic curve corresponded to a straight line within the range of the working pressure.

The data obtained in situ using the electronic data acquisition system were evaluated in the laboratory using the actual emitter emission rate. The analysis showed that the variation of the discharge coefficients between field and catalogue data for all emitters is less than 2%, which ensured that the field data used in this research was reliable and representative.

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Data Availability Statement:

Conflicts of Interest:

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