

Thermodynamic analysis of a power plant integrated with fogging inlet cooling and a biomass gasification



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Outline

1. Introduction
2. System Description
3. Thermodynamic Modeling
4. Results and Discussions
5. Conclusions



1. Introduction



Why fog cooling?

The performance of a gas turbine, particularly output power and energy efficiency, is significantly affected by ambient temperature, especially during hot and humid summer periods when power demands often peak

The fog inlet cooling, which is one of way to increase energy efficiency, involves spraying water droplets into the compressor inlet air to reduce its temperature towards the corresponding wet-bulb temperature

1. Introduction



What is biomass

- Biomass is a renewable energy source that is derived from living or recently living organisms.
- Biomass includes biological material, not organic material like coal.
- Energy derived from biomass is mostly used to generate electricity or to produce heat.
- Biomass can be chemically and biochemically treated to convert it to a energy-rich fuel.

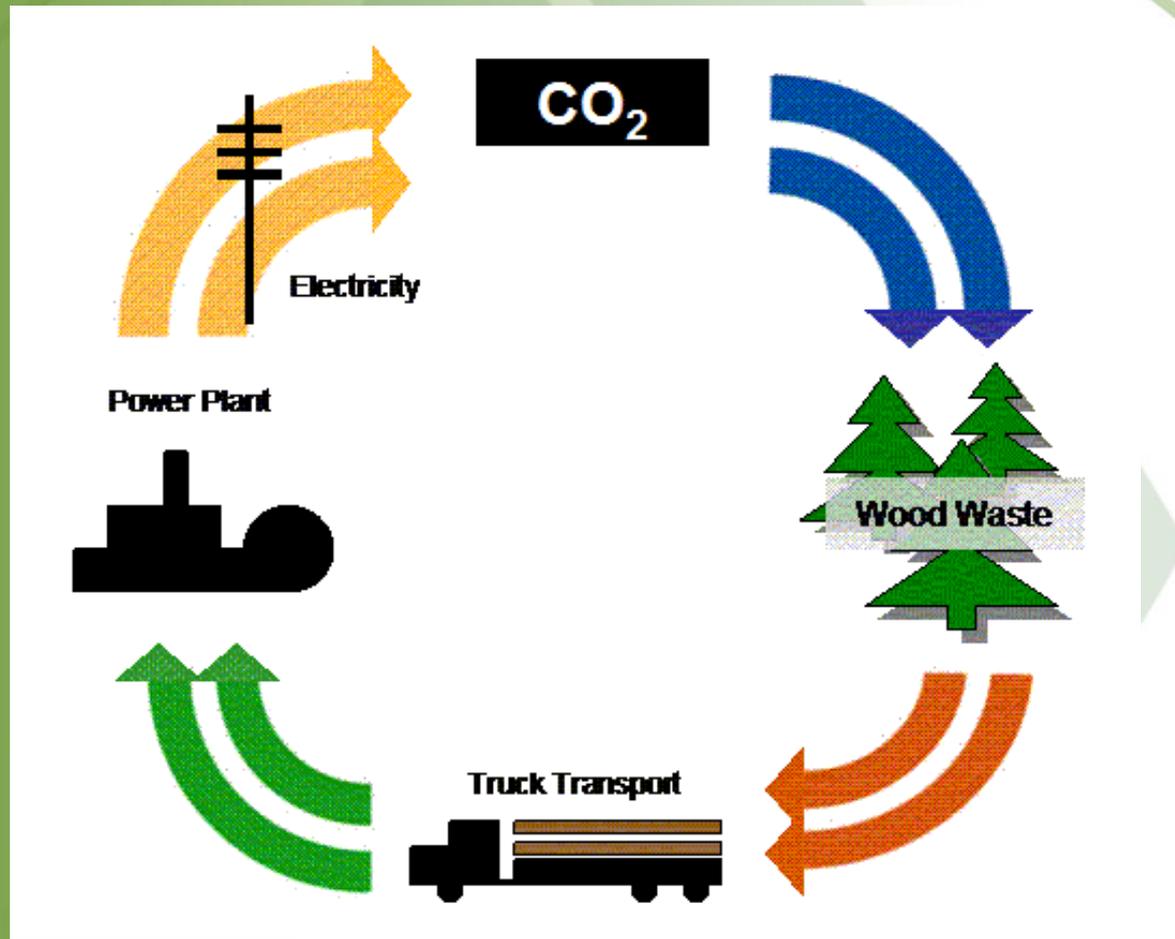
1. Introduction



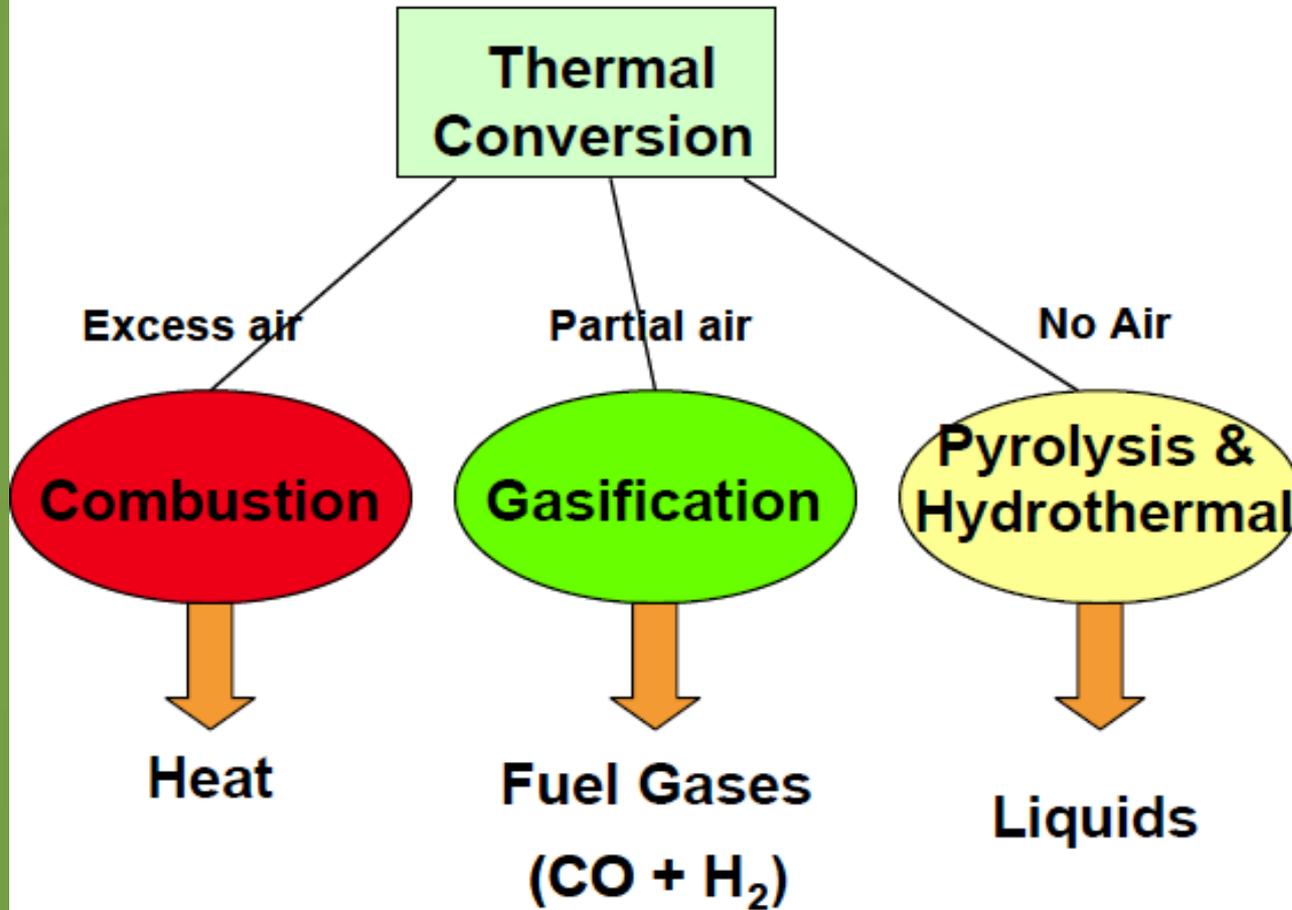
What makes it green (ideally)?

- CO₂ emissions/per energy produced is similar to petroleum.
- However, CO₂ released is recaptured by next years crops. So, there is no net CO₂ added.

1. Introduction



1. Introduction



1. Introduction



What is Biomass Gasification?

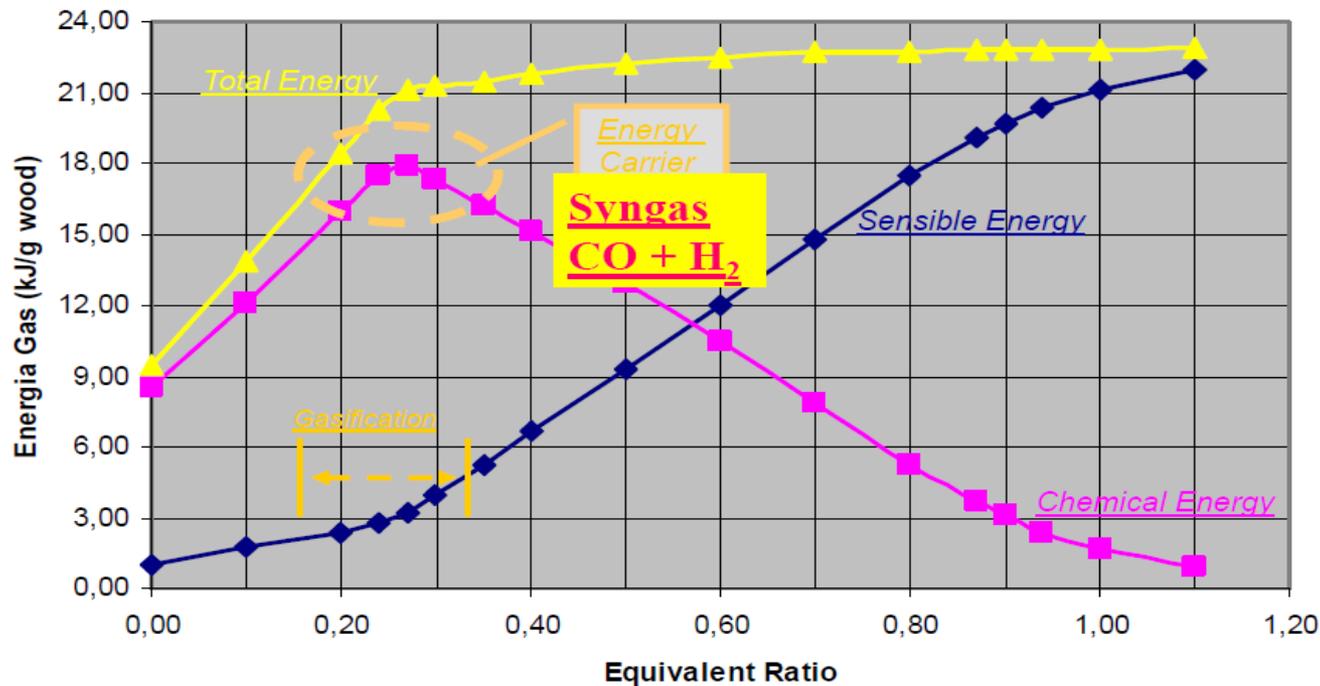
Basic Process Chemistry

- Conversion of solid fuels into combustible gas mixture called producer gas ($\text{CO} + \text{H}_2 + \text{CH}_4$)
- Involves partial combustion of biomass
- Four distinct process in the gasifier viz.
 - Drying
 - Pyrolysis
 - Combustion
 - Reduction

1. Introduction



WHY GASIFICATION



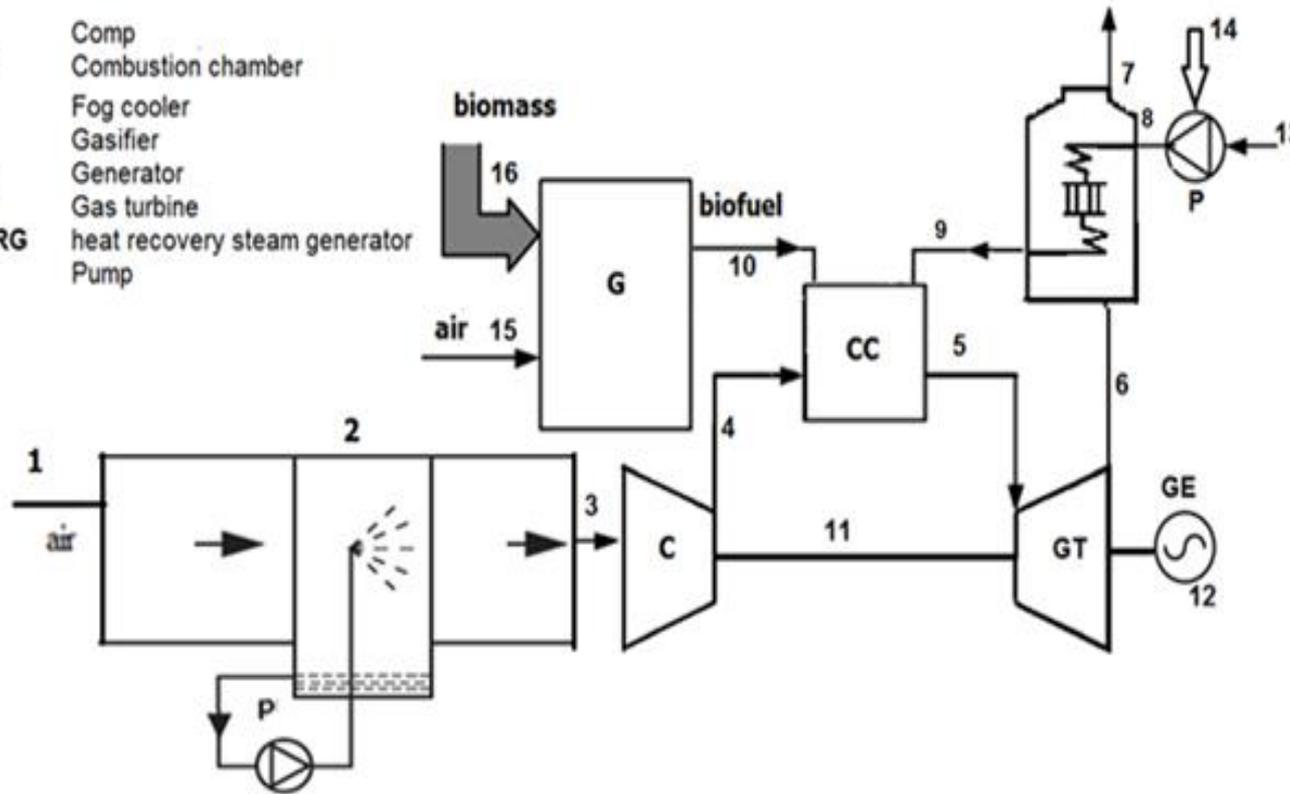
It maximize the Chemical Energy in the produced gases

2. System Description



Legend:

C	Comp
CC	Combustion chamber
F	Fog cooler
G	Gasifier
GE	Generator
GT	Gas turbine
HSRG	heat recovery steam generator
P	Pump



Gas turbine cycle with steam injection and inlet fogging cooler (BIFSTIG)

2. System Description



BIFSTIG (biomass integrated fog cooling steam injection gas turbine)

FSTIG (fog cooling steam injection gas turbine with firing of natural gas)

BISTIG (biomass integrated gas turbine with steam injection)

BIFGT (biomass integrated gas turbine with fog cooling)

BIGT (biomass integrated simple gas turbine)

3. Thermodynamic Modeling



$$\dot{m}_{a3} h_{a3} + \dot{m}_{v3} h_{v3} + \dot{m}_{f3} h_{f3} = \dot{m}_{a1} h_{a1} + \dot{m}_{v1} h_{v1} + \dot{m}_w h_w$$

The both side of equation are divided by \dot{m}_{a3} or \dot{m}_{a1} (because they are equal to each other)

(W (specific humidity) is equal to \dot{m}_v / \dot{m}_a and overspray is equal to $\dot{m}_{f3} / \dot{m}_{a3}$)

$$h_{a3} + w_3 h_{v3} + (\dot{m}_{f3} / \dot{m}_{a3}) h_{f3} = h_{a1} + w_1 h_{v1} + (\dot{m}_w / \dot{m}_{a3}) h_w$$

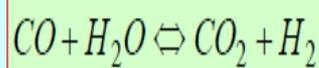
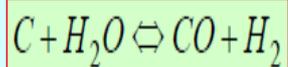
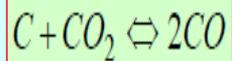
$$\dot{m}_w = \dot{m}_3 + \dot{m}_{f3} - \dot{m}_1 \text{ (In point 3 there are air and liquid water)}$$

$$h_{a3} + w_3 h_{v3} + \text{overspray} \times h_{f3} = h_{a1} + w_1 h_{v1} + (w_3 - w_1 + \text{overspray}) h_f$$

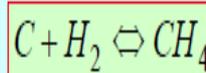
3. Thermodynamic Modeling



Equilibrium model^[1]



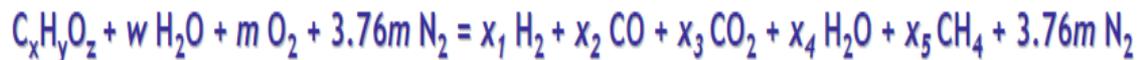
$$K_2 = \frac{P_{CO_2} P_{H_2}}{P_{CO} P_{H_2O}}$$



$$K_1 = \frac{P_{CH_4}}{(P_{H_2})^2}$$

K_i : equilibrium constants for methane formation and shift reaction

Global gasification process can be expressed as the global reaction:



3. Thermodynamic Modeling



Part A: Fogging cooler			Part B: Biomass gasification			
Comparison conditions	Comparison of reported and computed results for selected conditions: TIT = 1122°C, compressor pressure ratio = 11.84, inlet mass rate of turbine = 374.59 kg/s, overspray = 2%		Comparison conditions	Comparison between model and experimental constituent breakdown (in %) for wood at 20% moisture content and a gasification temperature of 800 °C		
Parameter	Reported in [6]	Computed here	Parameter	Computed here	Reported in [26]	Reported in [25]
CIT (°C)	30.00	30.08	Hydrogen	18.01	15.23	21.06
CDT (°C)	293	286.9	Carbon monoxide	18.77	23.04	19.61
\dot{W}_{net} (MW)	133	136	Methane	0.68	1.58	0.64
TOT (°C)	553	577	Carbon dioxide	13.84	16.42	12.01
Heat rate (kJ/kWh)	10,609	10,653	Nitrogen	48.7	42.31	46.68
			Oxygen	0.00	1.42	0.00

3. Thermodynamic Modeling



Thermodynamics

- The First Law
 - The energy of the universe is constant
- The Second Law
 - The Entropy of the universe is constantly increasing.

3. Thermodynamic Modeling



Energy-based methods are not suitable for answering some questions because the only thermodynamic inefficiencies identified by energy-based methods are the transfer of energy to the environment. However, *the inefficiencies caused by the irreversibilities within the system* being considered are, in general, by far the most important thermodynamic inefficiencies and are identifiable with the aid of an exergetic analysis.

Exergy-based methods reveal the location, the magnitude and the sources of inefficiencies and costs impact and allow us to study the interconnections between them.

3. Thermodynamic Modeling



Exergetic Variables: E_p and E_F

Exergy of product: \dot{E}_p

The desired result, expressed in exergy terms, achieved by the system (the k -th component) being considered.

Exergy of fuel: \dot{E}_F

The exergetic resources expended to generate the exergy of the product.

The concepts of product and fuel are used in a consistent way not only in *exergetic analyses* but also in the *exergoeconomic* and *exergoenvironmental* analyses.

3. Thermodynamic Modeling



Exergetic Variables: E_D and E_L

Exergy destruction: \dot{E}_D

Exergy destroyed due to irreversibilities within a system (the k -th component).

Exergy loss: \dot{E}_L

Exergy transfer to the system surroundings. This exergy transfer is not further used in the installation being considered or in another one.

Exergy balance:

$$\dot{E}_F = \dot{E}_P + \dot{E}_D (+ \dot{E}_L)$$

\dot{E}_D and \dot{E}_L are absolute measures of the thermodynamic inefficiencies.

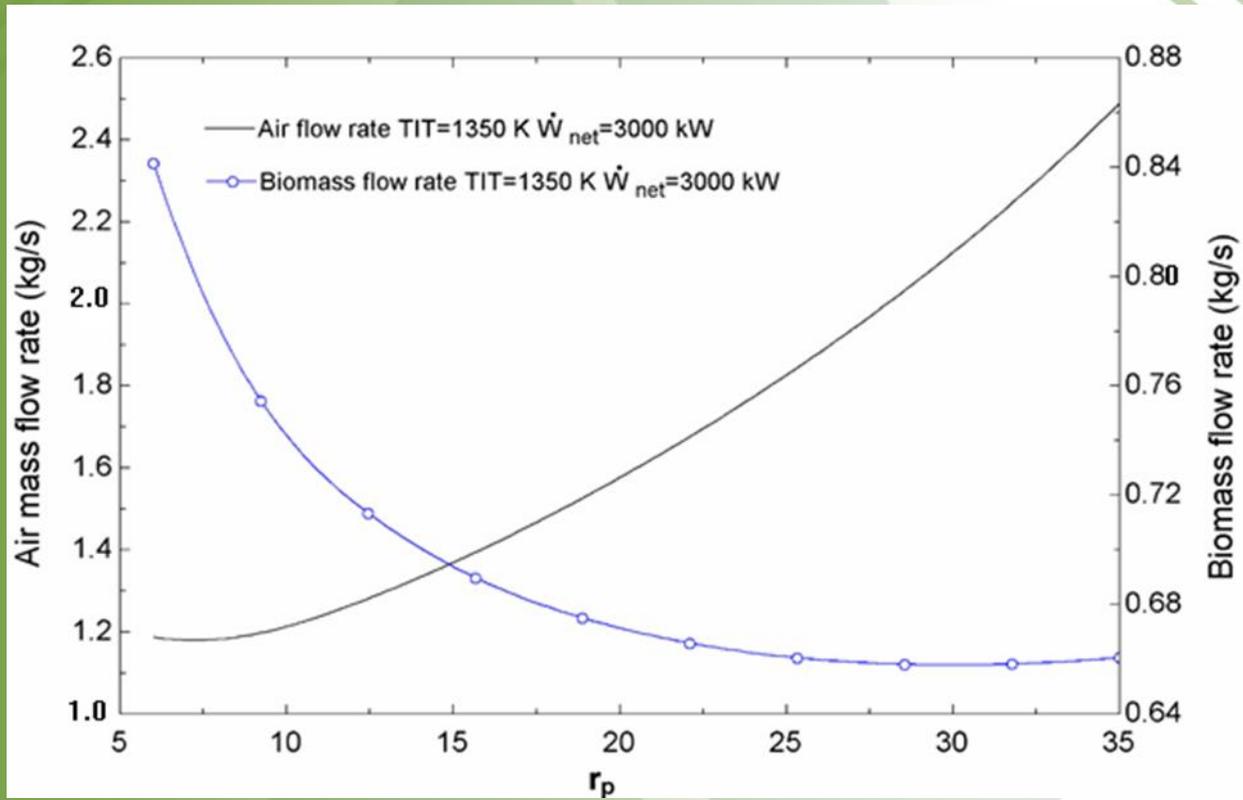
3. Thermodynamic Modeling



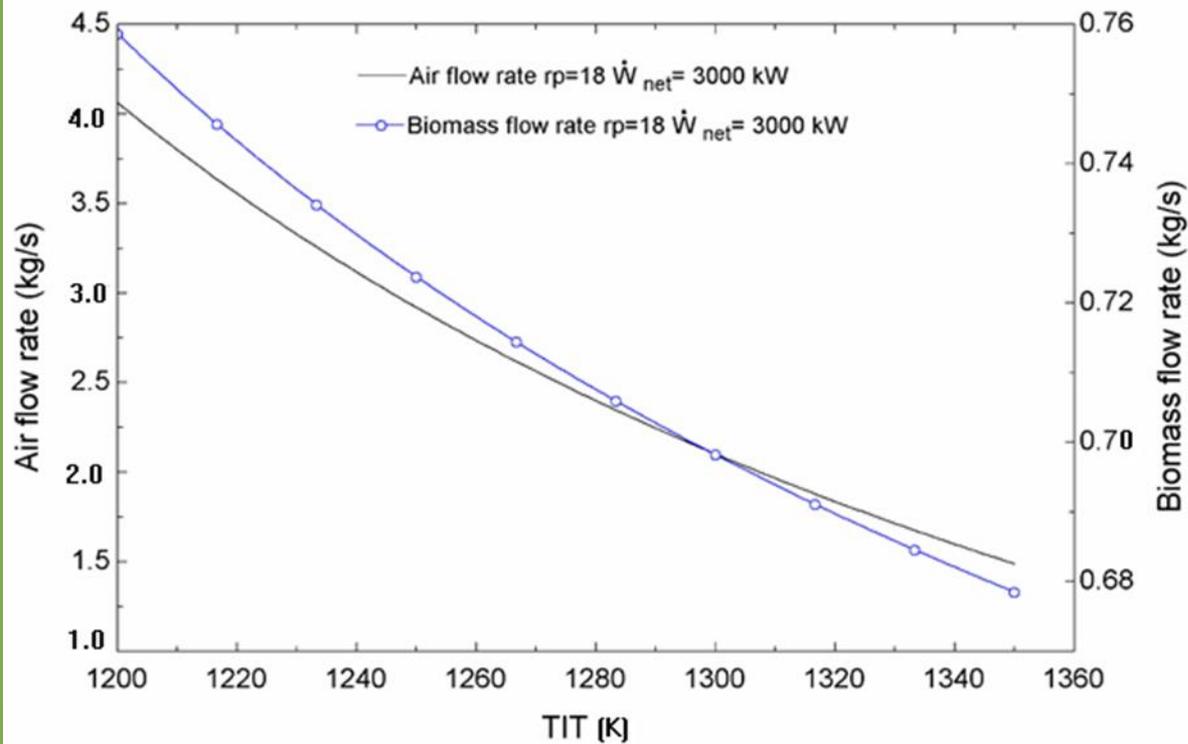
$$\eta = \frac{\dot{W}_{\text{net,cycle}}}{\dot{m}_{\text{fuel}} \text{LHV}_{\text{fuel}}}$$

$$\varepsilon = \frac{\dot{W}_{\text{net,cycle}}}{\dot{E}_{\text{in,cycle}}}$$

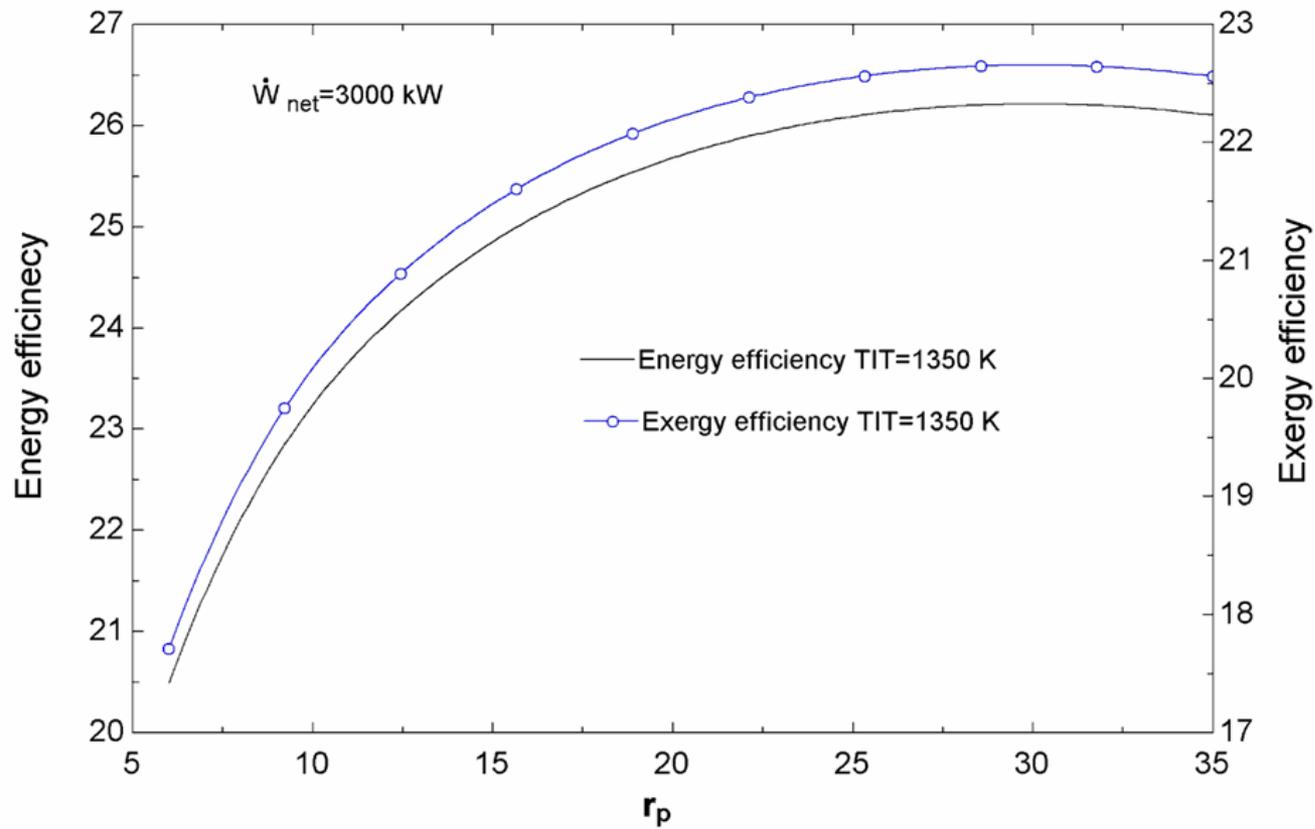
4. Results and discussions



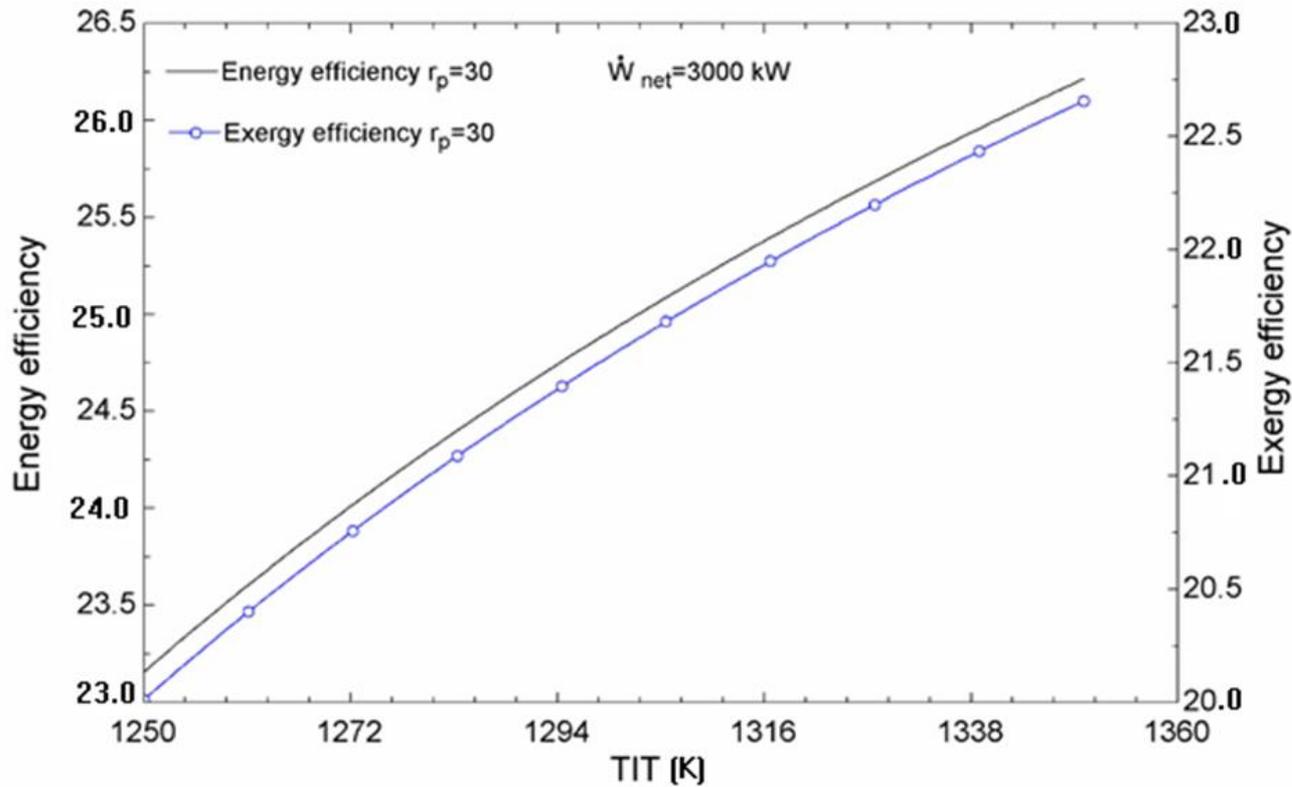
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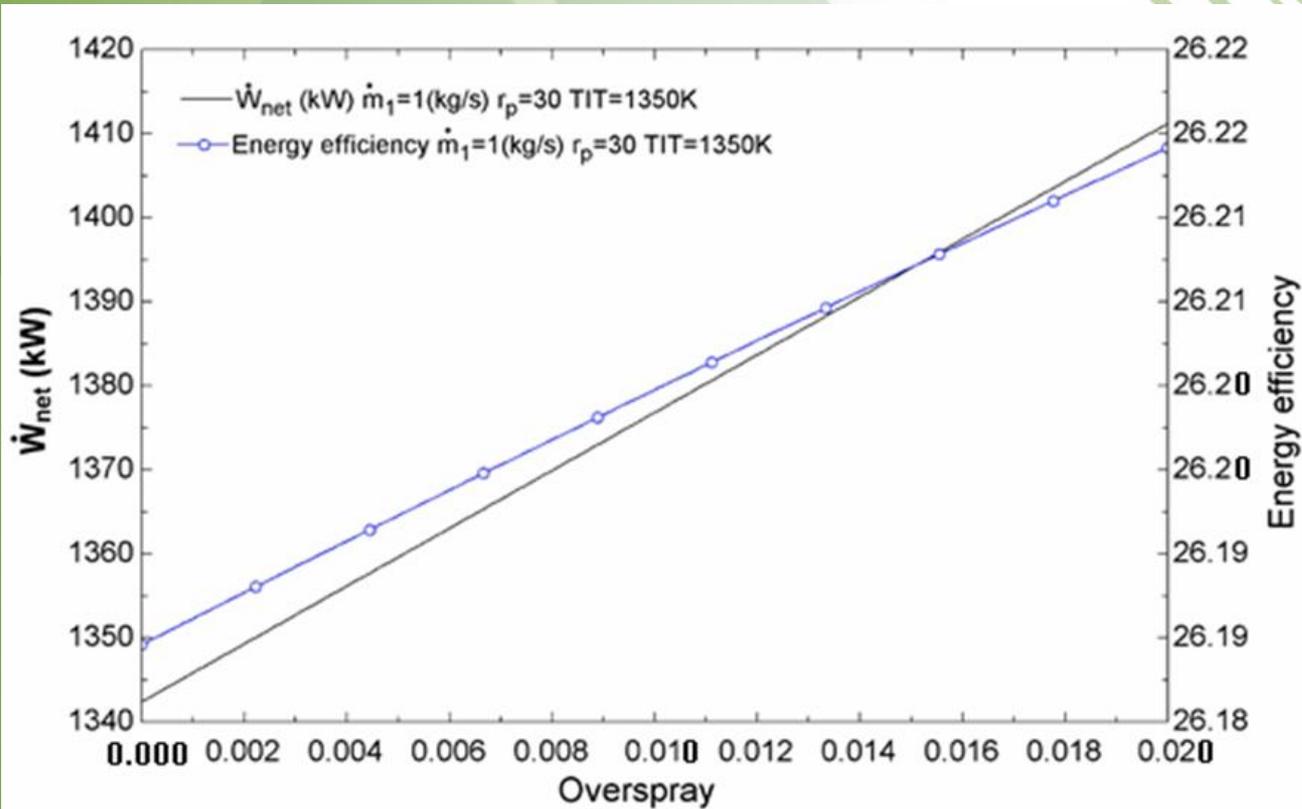
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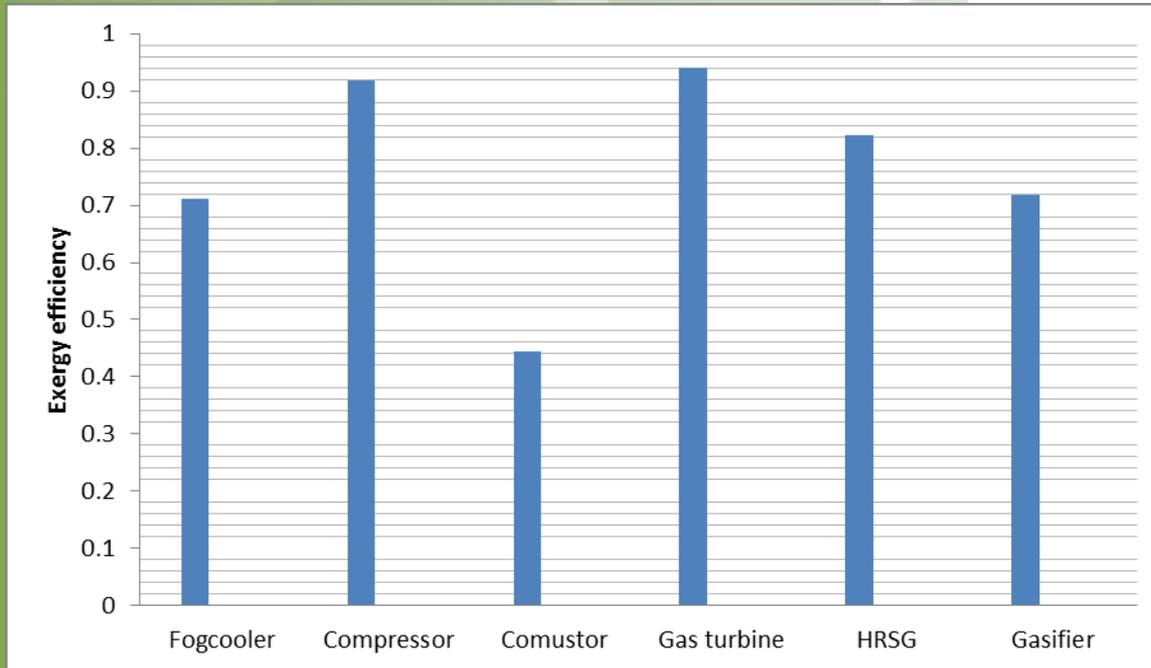
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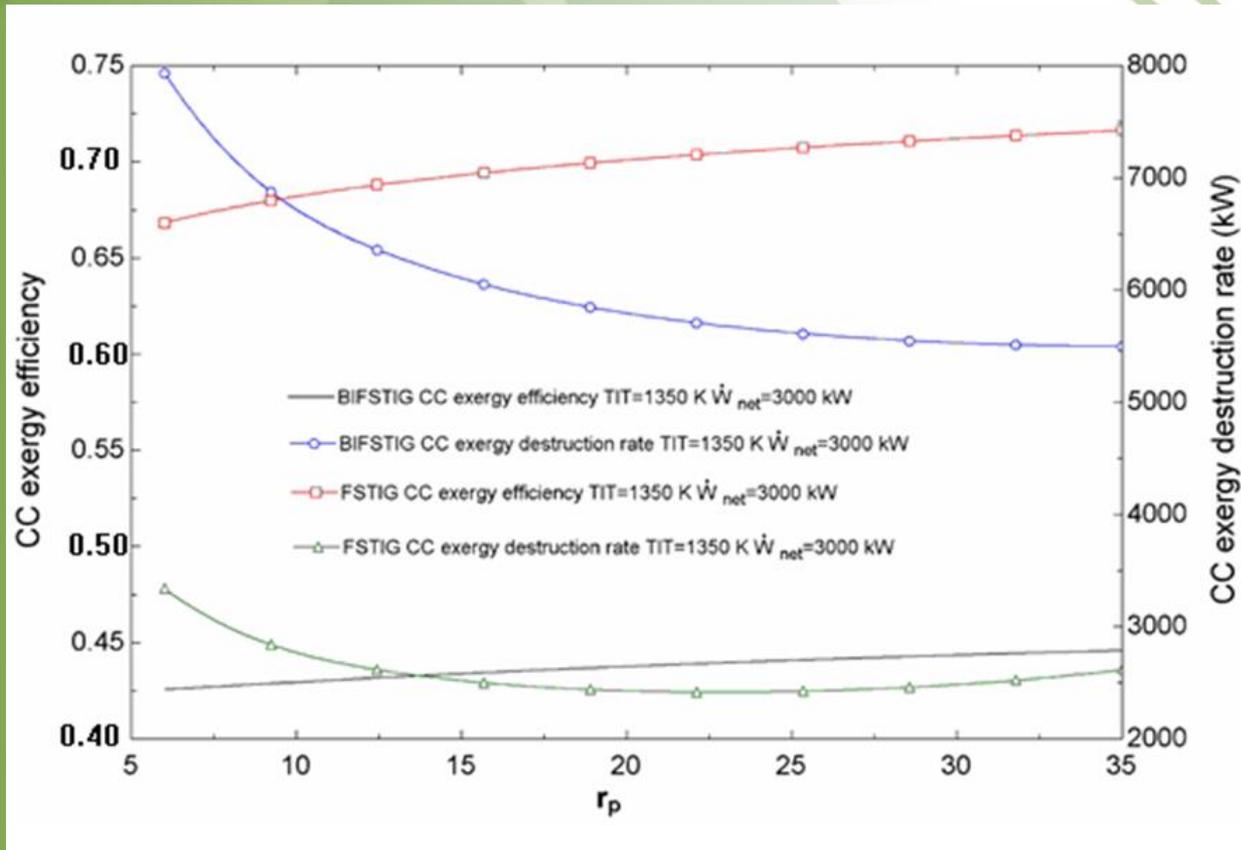
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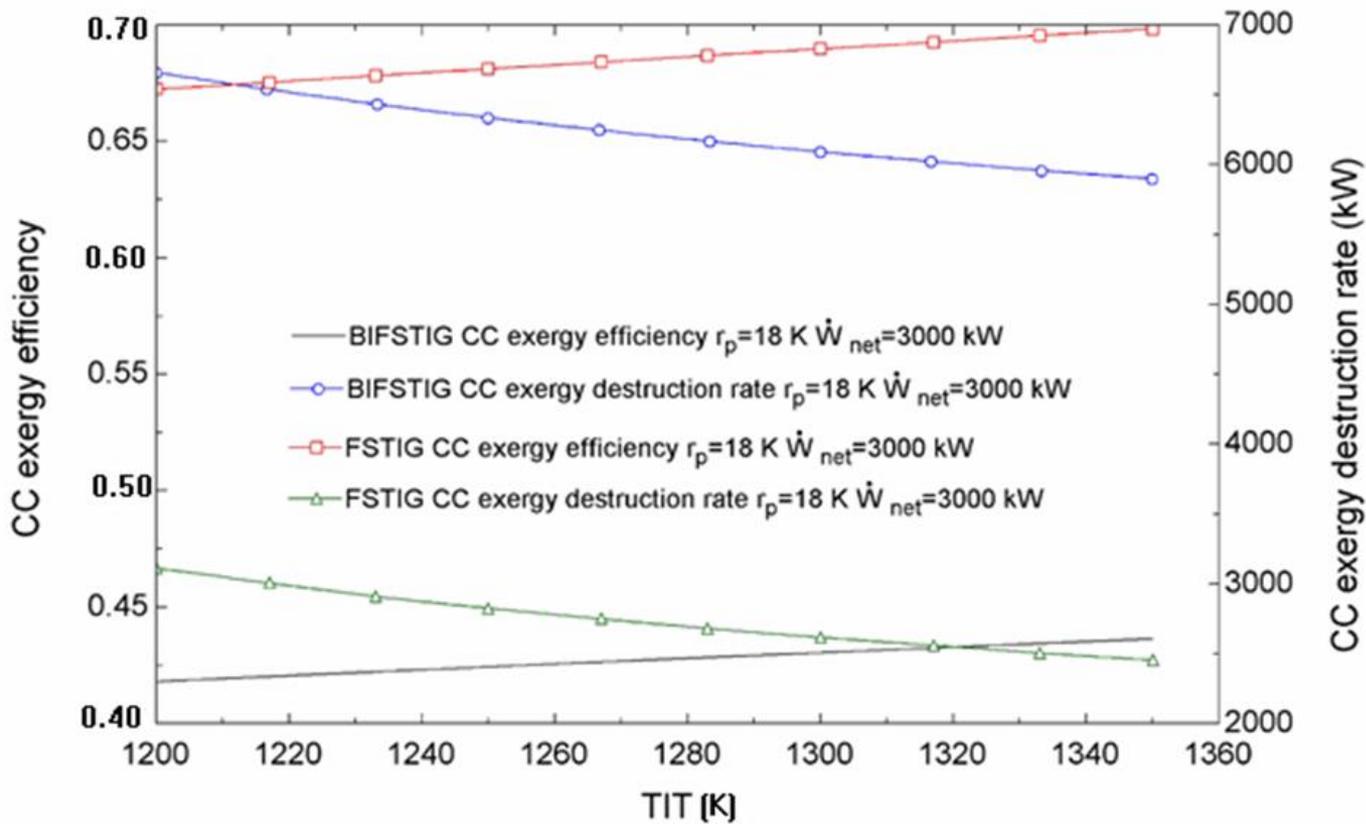
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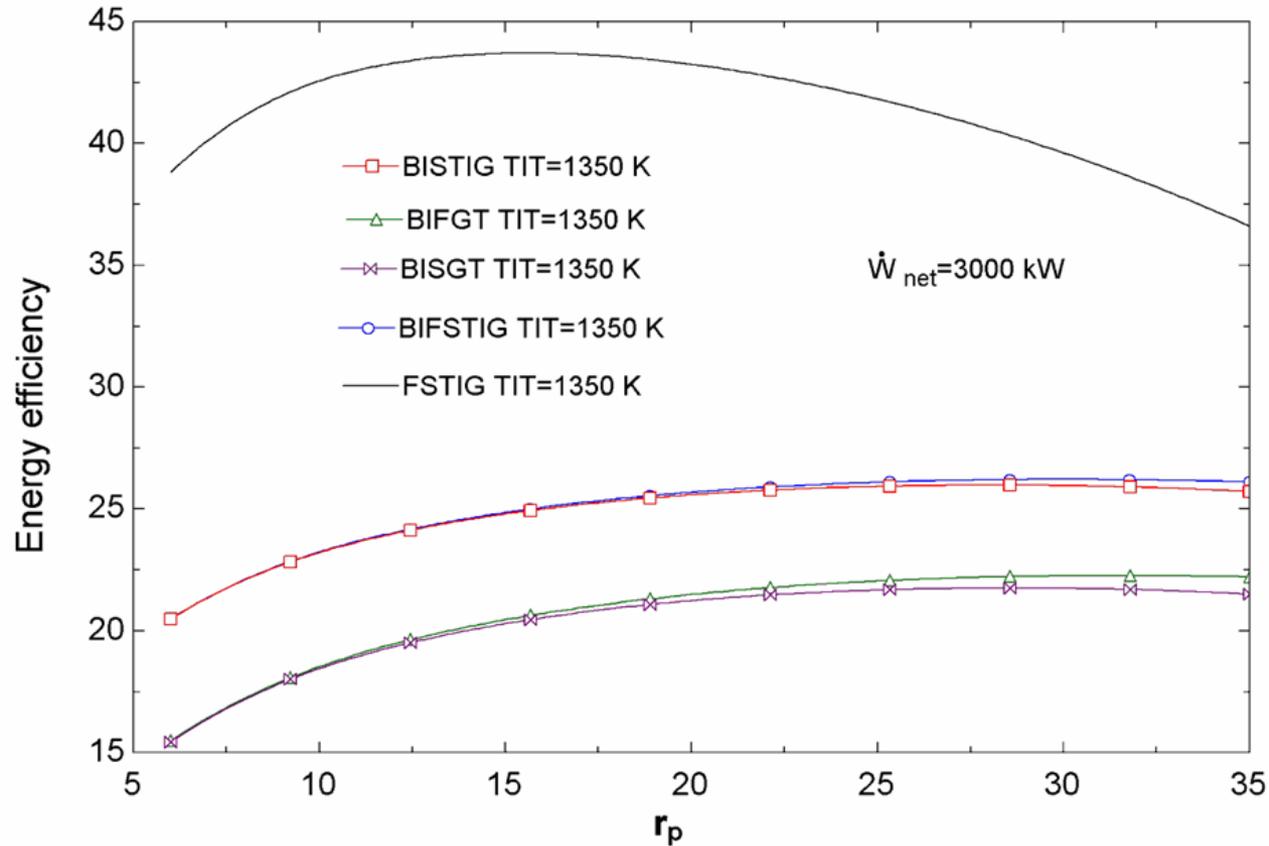
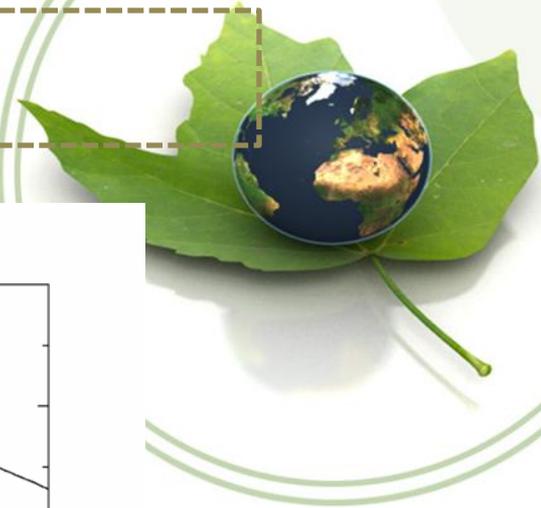
4. Results and discussions



4. Results and discussions



4. Results and discussions



5. Conclusion

- Increasing the compressor pressure ratio and gas turbine inlet temperature increases the energy and exergy efficiencies.
- Also, increasing compressor pressure ratio and gas turbine inlet temperature decreases the biomass flow rate, while the air mass flow rate increases with increasing compressor pressure ratio and decreases with increasing gas turbine inlet temperature.
- Overspray raises the net power output and the energy efficiency, with the influence on former being more significant.



5. Conclusion

- Increasing the compressor pressure ratio and gas turbine inlet temperature raises the combustor exergy efficiency for the BIFSTIG plant, while increasing the pressure ratio raises the energy efficiency. However, there is an optimum point in terms of a specific pressure value in the natural gas fired plant (FSTIG).
- For the maximum energy efficiency condition of the BIFSTIG plant, the component exergy efficiency is highest for the turbine and the lowest for the combustor. The BIFSTIG combustor exergy efficiency is lower than for a similar plant fired with natural gas.



*Many thanks for your
attention*

