The 6th International Electronic Conference on Applied Sciences



09-11 December 2025 | Online

Eddy Current Testing of a Steam Generator with a Support Plate

Dounia Sedira¹, Oussama Nouar², Abdelouhab Boussenoune², Nassira Ferkha¹, Mohamed Chelabi¹

¹Laboratory of Electrical Engineering and Industrial Electronics (L2EI), Faculty of Science and Technology, University of Jijel, Jijel, Algeria

² Electrical Engineering Departement, Faculty of Science and Technology University of Jijel, Algeria

INTRODUCTION & AIM

Steam generators play an important role in a variety of industries, including chemical and petrochemical production, engineering and nuclear applications. Steam generator tubes are subjected to high pressures, making them prone to corrosion and vibration; as a result, they are held in place with supports named tube support plates (TSPs). However, TSPs are regarded as disturbing signals for , nondestructive testing (NDT) techniques. In this study, the influence of the support plates on eddy current testing (ECT) of a steam generator tube made of Inconel 600 with a defect is explored. The modeling of eddy current testing is based on solving a 2D axisymmetric finite element formulation under steady-state conditions via Comsol Multiphysics Software. The impedance of the differential coil is calculated using the direct method, and the difference impedance signal is obtained from two simulations: with flaw and without flaw.

METHOD

Nondestructive problem modelling using eddy current testing

$$rot\left(\left(\frac{1}{\mu}\right)rot(A)\right) + \sigma\left(\frac{\partial(A)}{\partial t}\right) = J_e \tag{1}$$

In harmonic analysis, the time derivative $\frac{\partial (A)}{\partial t}$ is replaced by the complex expression $j\omega A$ $(j^2=-1)$

 $rot\left(\left(\frac{1}{\mu}\right)rot(A)\right) + \sigma(j\omega A) = J_e$ (2)

In an axisymmetric problem, the components of the current density $\bf J$ and the vector potential $\bf A$ are:: $\bf J$ (0, $\bf I_{\phi}$, 0) and $\bf A$ (0, $\bf A_{\phi}$, 0) Equation (2) becomes [1]:

$$-\frac{\partial}{\partial r} \left(\frac{1}{r\mu_r} \cdot \frac{\partial(\mathbf{A})}{\partial r} \right) - \frac{\partial}{\partial z} \left(\frac{1}{r\mu_r} \cdot \frac{\partial(\mathbf{A})}{\partial z} \right) + j \frac{\omega \cdot \sigma \cdot \mu_0}{r} \cdot (\mathbf{A}) = \mu_0 \cdot \mathbf{J}_{\varphi}$$
 (3)

The 2D axisymmetric frequency-domain equation (3) is solved through the finite element method via COMSOL Multiphysics Software.

Impedance evaluation of a differential coil via the finite element modelling

Consider two coils with Ns turns, connected in a differential configuration and carrying equal and opposite currents. An axisymmetric finite element analysis allows to calculate the impedance according to expression [2]:

$$Z_{\text{bobine}} = \frac{j\omega \cdot 2\pi \cdot J_{s}}{I_{s}^{2}} \cdot \left(\sum_{1}^{n_{a}} r_{ci} \cdot A_{ci} \cdot \Delta_{i} - \sum_{1}^{n_{b}} r_{ci} \cdot A_{ci} \cdot \Delta_{i} \right)$$

$$(4)$$

 Δ_i : is the area of the element under consideration.

 $\vec{A_I}, \, A_I \, {\rm et} \, A_K$: are the values of the vector potential A at nodes I, J, and K

 $r_{\rm I}, r_{\rm J}$ et $r_{\rm K}$: are the values of the radius r of nodes I, J, and K with respect to the axis of symmetry.

The modeling of the system to be inspected is carried out in the case of the existence of the defect and with the absence of the defect; the differences in impedance, reactance, and resistance are given by the following equations:

$$\Delta Z = \sqrt{\Delta R^2 + \Delta X^2}$$

$$\Delta X = Xd - X0$$

$$\Delta R = Rd - R0$$

Xd: Sensor reactance with defected piece[Ω].

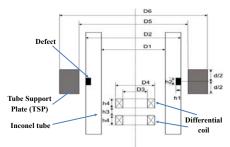
X0: Sensor reactance of a defect free piece[Ω].

Rd: Sensor resistance with defected piece $[\Omega]$.

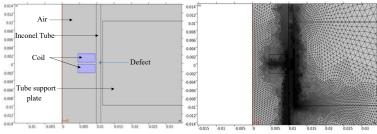
R0: Sensor resistance of a defect free piece $[\Omega]$

RESULTS & DISCUSSION

Simulated Steam Generator

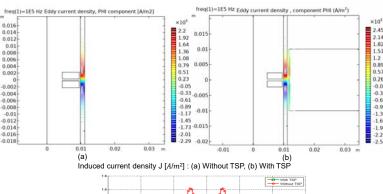


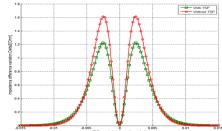
Eddy current reference problem of a steam generator proposed by WFNDEC [3]



Axisymmetric representation of the simulated device

Geometry discretization using comsol





Variation of the impedance difference as a function of the position of the differential coil sensor

CONCLUSION

The presence of a support plate alters the eddy current distribution and therefore the measured impedance. Fault detection is visible at the scan point corresponding to z=0. The results obtained have proven that the support plate is a disturbing element that influences the fault detection signal.

FUTURE WORK / REFERENCES

[1]Nait-Said, F. Z. L. N., & Drid, S. (2006). Numerical analysis of electromagnetic axisymmetric problems using element free galerkin method. Journal of Electrical Engineering, 57(2), 99-104.

[2]Palanisamy, R., & Lord, W. (2003). Prediction of eddy current probe signal trajectories. IEEE Transactions or Magnetics. 16(5), 1083-1085.

(3)Nogueira, A. F. L., Weinert, R. L., & Maldonado, L. J. A. S. (2021). An Introductory Note on Finite Element Problems Based on the Eddy Current Testing Approach. Journal of Electromagnetic Analysis and Applications, 13