

**LIFE PREDICTION WITHOUT CURVE  
FITTING MODELS:  
USING ENTROPY TO UNIFY NEWTONIAN  
MECHANICS AND THERMODYNAMICS**

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## Presentation Outline

I- Objective

II- Introduction

III- Historical Efforts to Unify Mechanics and Thermodynamics

IV- Theory

V- Mathematical Verifications

VII- Experimental Verifications

VIII- Conclusions

## Objective

Accurately predicting life span of physical bodies - living and non-living - has been humankind's eternal endeavors.

## Newtonian Mechanics versus Thermodynamics

**Newtonian Mechanics** provides the response of physical bodies to external disturbances, but does not take into account past-present-future changes, like aging, microstructural re-organizations and others.

**Thermodynamics**, provides information about the past-present-future changes happening in a physical body over time, but does not give any information about the response of a body to any external disturbance.

## Newtonian Mechanics

Sir Isaac Newton's work in "The Principia," 1687

First law:

an object either remains at rest or continues to move at a constant **velocity** unless acted upon by a **force**

Second law:

the vector **sum** of the **forces**  $F$  on an object is equal to the **mass**  $m$  of that object multiplied by the **acceleration**  $a$  of the object:  $F = ma$ .

Third law:

When one body exerts a force on a second body, the second body simultaneously exerts a force equal in magnitude and opposite in direction on the first body.

## Historical Efforts

In 1850 Rudolf Clausius and William Thompson (Kelvin) formulated both the First and Second Laws of Thermodynamics

between 1872 and 1875 , Using statistical mechanics, Boltzmann's formulated probability equation relating the entropy to the quantity disorder.

1934, Swiss physical chemist Werner Kuhn successfully derived a thermal equation of state for **rubber** molecules using Boltzmann's formula. **[Boltzmann's formulation is not restricted to gasses, as Boltzmann indicates]**

## Historical Efforts to Introduce Thermodynamics into Mechanics

Since Newtonian mechanics does not account for past, present and future. There were many attempts to introduce degradation into mechanics, such as:

- Stress-Number of Cycles (S-N) curve
- Miner's Rule
- Coffin-Manson
- Paris' Law
- Gurson Model
- Gurson-Tvergaard-Needleman Model
- Johnson-Cook Model
- Structural Fragility Curves
- "Kachanov" Damage Mechanics Models- damage potential surface

## Problem with Historical Efforts

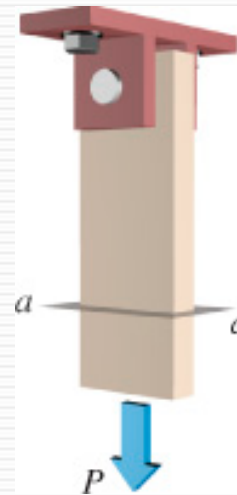
- ❑ They are all based on phenomenological curve fitting techniques. Degradation response is needed before-hand to generate a polynomial.
- ❑ Most do not satisfy laws of thermodynamics, due to using displacement, strain or stress.
- ❑ They are only valid for the test type and specimen size they are obtained for.
- ❑ They require linear superposition of many damage mechanisms due to different load types (Miner's rule)
- ❑ Results cannot be extrapolated to any other loading path or outside their range.
- ❑ Most cannot account for past.



## Unified Theory – *MechanoThermodynamics*

Both displacement (or force), entropy generation rate are nodal unknowns.

**Newtonian Mechanics**  $u = P/k$   
*u doesn't change by time*



**MechanoThermodynamics**

New Nodal unknowns

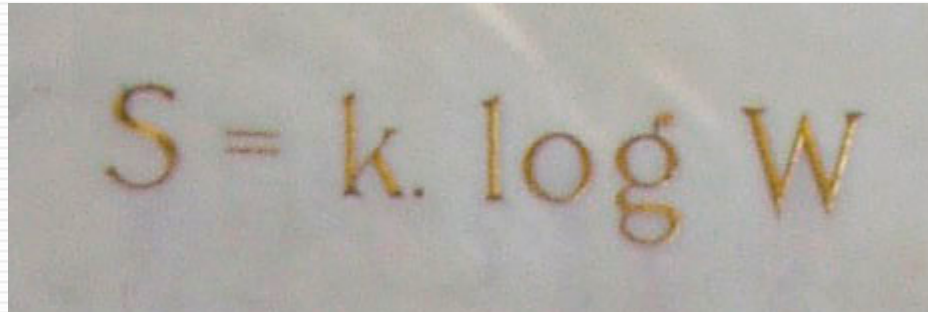
$u, \dot{\gamma}$

**NO CURVE FITTING, or PHENOMENOLOGICAL MODELS**

## 2<sup>nd</sup> Law of Thermodynamics

The Second Law states that there is a natural tendency of any isolated system, living or non-living, to degenerate into a more disordered state.

When **irreversible entropy generation** becomes zero the system reaches “THE END” (fails/dies).



Boltzmann's equation—carved on his gravestone.

The logarithmic connection between entropy and disorder probability was first stated by L. Boltzmann (1872) and put into final form by Maxwell Planck (1900)

*Note that Boltzmann formulates this hypothesis for an arbitrary body, i.e. formulation in the original paper is NOT restricted to gases.*

## Everything in Nature , [living and non-living] is a Thermodynamic System

Entropy ( $S$ ) of a system can be related to probability ( $W$ ) of existence of the system to be at a microstructural (**disorder**) state with respect to all other possible microstructural (**disorder**) states.

## Thermodynamic State Index (TSI):D

Let that probability of a material being in a completely ordered ground state is equal to  $W_0$

under external loads (mechanical, **thermal**, **electrical**, **chemical**, **radiation**, **corrosion** and **environmental**), material deviates from this reference state to another disordered state with a probability of  $W$ .

$$W_0 \text{ -----} \rightarrow W$$

## Irreversible Degradation in Solids

External effects will lead to permanent changes in microstructure of the material described as a positive entropy production. In solids “damage” happens due to irreversible internal entropy production.

Since a disordered state is formed from an ordered state due to “damage” (TSI change), “damage” and entropy (which is a measure of disorder) are related.

## Reference Thermodynamic States

When a material in ground (reference) state, it is free of any possible defects, i.e. damage, it can be assumed that “**damage**” in material is equal to zero. TSI will be  $D = 0$ .

In final stage, material reaches a critical state such that disorder is maximum,  $W_{\max}$ . At this stage, entropy production rate will become zero. TSI will be maximum  $D = 1$ .

## Thermodynamic State Index

In order to relate entropy and damage, consider a system in ground state  $D=0$  with a total entropy of  $S_0$  and an associated disorder probability is  $W_0$

In an alternative disordered (damaged) state,  $S$  is total entropy of the same system with an associated probability of  $W$  and a TSI level of  $D$ .

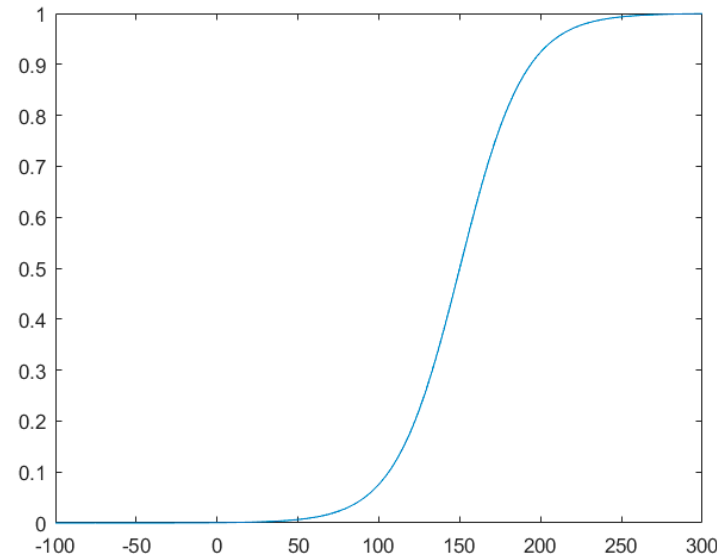
Instantaneous value of TSI can be calculated by the difference in TSI probability from the ground state probability  $D = f(W - W_0)$



## Universal Damage Evolution

TSI value must be normalized w.r.t. disorder probability in current state. Therefore;

$$D = f \left[ \frac{W - W_0}{W} \right]$$



## Multi Physics Entropy Computation

$$\Delta s = \int_{t_0}^t \frac{1}{\rho} \dot{\gamma} dt$$

$$\Delta s = \int_{t_0}^t \left\{ \begin{array}{l} \frac{1}{\rho T^2} k_T |\text{Grad}(T)|^2 + \frac{r}{T} \\ \frac{C_v D_{\text{effective}}}{\rho k_B T^2} \left[ Z_l^* e \rho^* j - f \Omega \nabla \sigma_{\text{spherical}} + \frac{Q^* \vec{\nabla} T}{T} + \frac{k_B T}{c} \vec{\nabla} C \right]^2 \\ + \frac{1}{\rho T} \boldsymbol{\sigma} : \boldsymbol{\varepsilon} \end{array} \right\} dt$$

Irreversible Entropy Production due to

1- Internal heat generation

2- Diffusion mechanisms (Electromigration, stress gradient, thermomigration, and vacancy (chemical) concentration gradient)

3- Internal mechanical work

## Entropy Computation does not Require any Curve Fitting Parameters

Where  $C_v$  vacancy concentration,  $D_{\text{effective}}$  vacancy diffusivity

$Z^*$  is vacancy effective charge number

$f$  is vacancy relaxation ratio

$e$  is electron charge

$\Omega$  is atomic volume

$\rho^*$  is metal resistivity

$k$  is Boltzman's constant

$\mathbf{j}$  is current density (vector)

$T$  is absolute temperature

$C$  is normalized vacancy concentration  $c = C_v / C_{v0}$   $\sigma_{\text{spherical}}$  is spherical part of stress tensor,

$C_{v0}$  equilibrium vacancy concentration

$$\sigma_{\text{spherical}} = \text{trace}(\sigma_{ij}) / 3$$

in the absence of stress field

$Q^*$  is heat of transport

## Mathematical Proof

### Provided in

Leonid A. Sosnovskiy and Sergei S. Sherbakov,  
“Mechanothermodynamic Entropy and Analysis of Damage State  
of Complex Systems”, *Entropy* (2016), 18, 268;

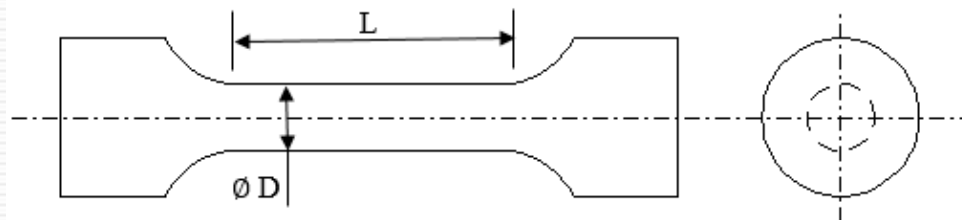
### Based on the Concept first published By

Basaran and Yan, *ASME J. of Electronic Packaging* 120, 379, 384, (1998)

Basaran, C. and Nie, S., “An Irreversible Thermodynamics Theory  
for Damage Mechanics of Solids” *International Journal of Damage  
Mechanics*, Vol. 13—July 2004

## Experimental Verifications

## Fatigue Loading on A-36 Steel



$L=25\text{mm}$

$D=6.4\text{mm}$

$E=210000\text{MPa}$

$\nu=0.3$

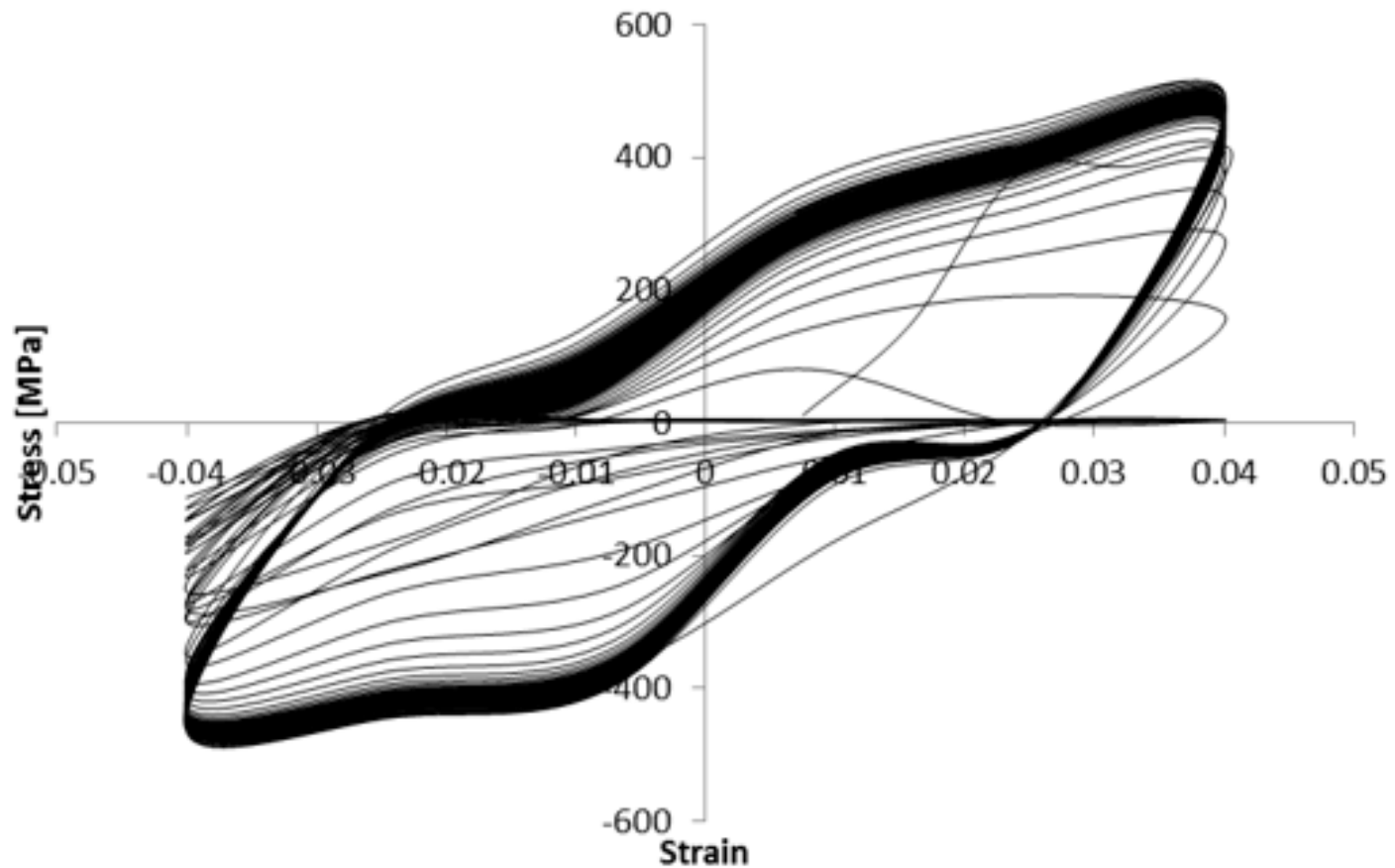
$T=295\text{K}$

$R=8.314\text{J/K}\cdot\text{mol}$

$\rho=7750\text{kg/m}^3$

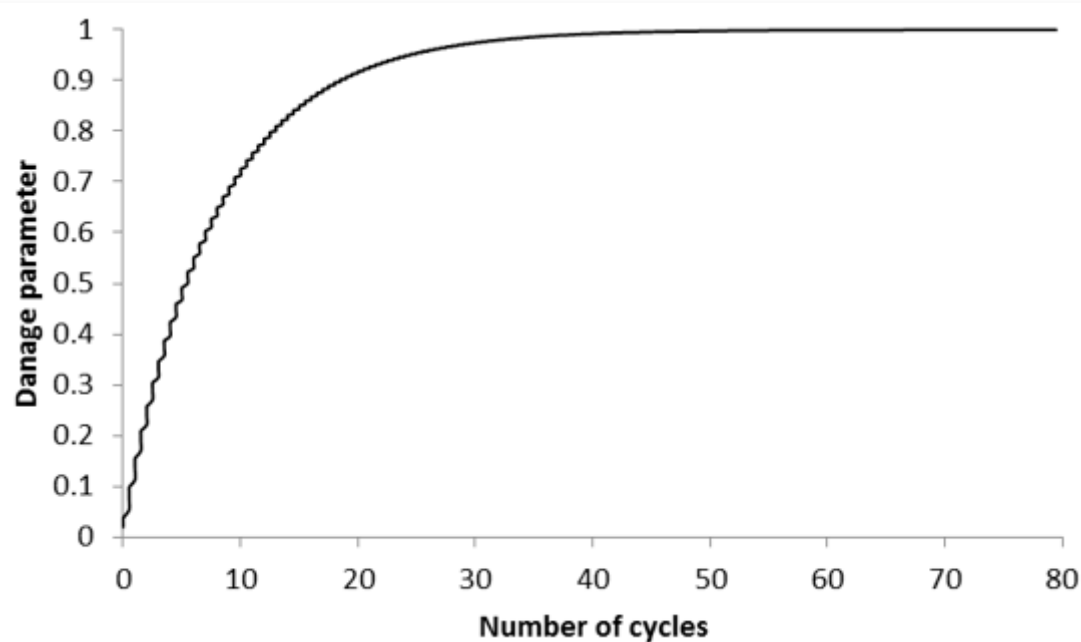
$m_s=55.8\text{g/mol}$

## Fatigue Loading – Displacement Controlled Test



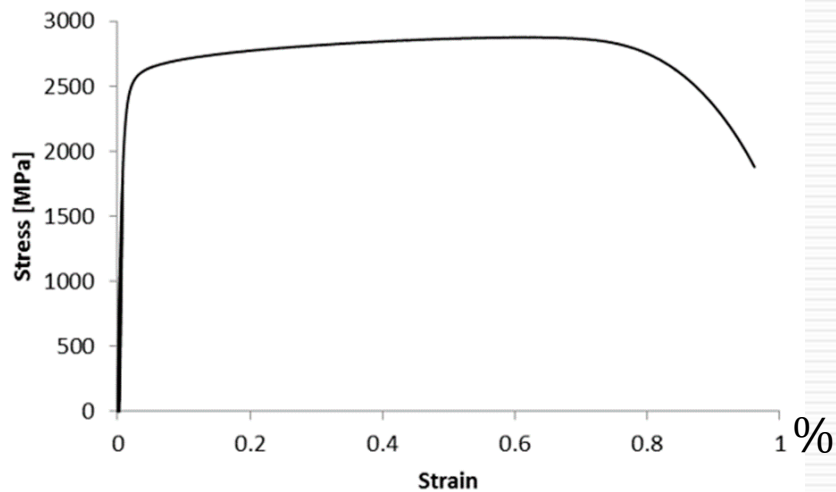
## Damage Evolution - Calculated

$$\Delta\eta = \int_{t_0}^t \frac{\sigma:\dot{\epsilon}^p}{\rho T} dt$$

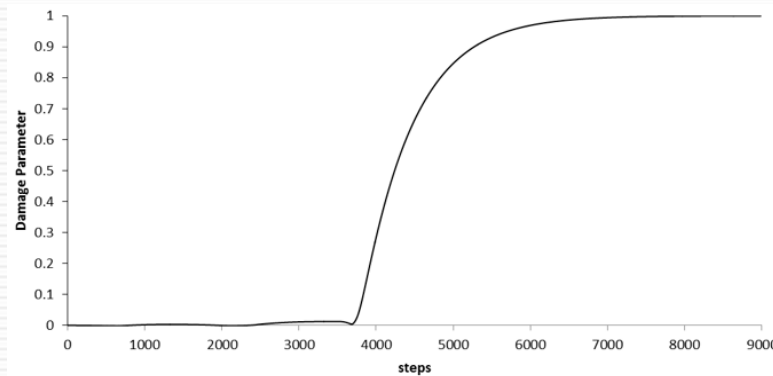




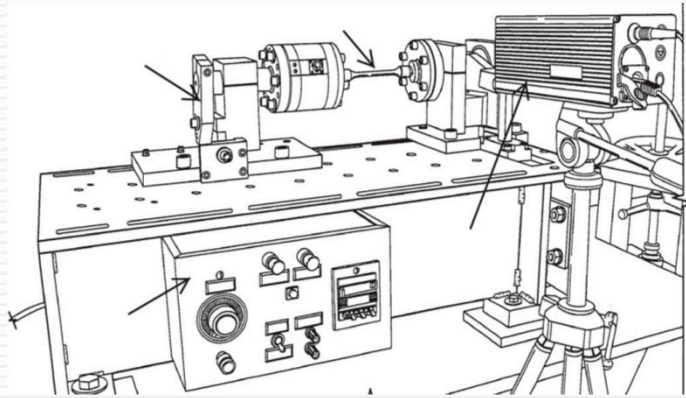
## Monotonic Loading Test



Damage Parameter (Thermodynamic State Index)



M. Naderi, M. Amiri and M. M. Khonsari , On the thermodynamic entropy of fatigue fracture” Proceedings of the Royal Society A (2010) 466, 423-438



‘A thermodynamic approach for the characterization of material degradation, which uses the entropy generated during the entire life of the specimens undergoing fatigue tests is used. Results show that the cumulative entropy generation is constant at the time of failure and is independent of geometry, load and frequency.’”

Imanian, A., Modarres, M., “A Thermodynamic Entropy-Based Damage Assessment with Applications to Prognosis and Health Management”, *Structural Health Monitoring*, (2017) DOI: 10.1177/1475921716689561

“We therefore conclude that entropy generation can be used to assess the degree of damage, the amount of the life of materials expended and the extent of the life remaining”.

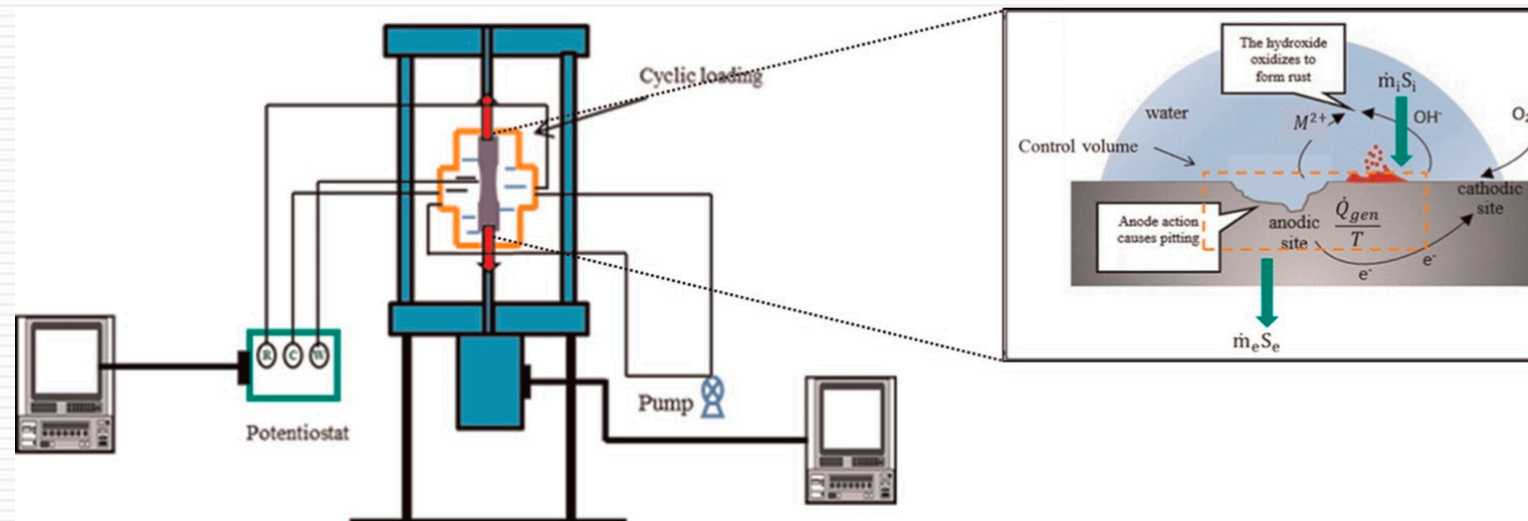
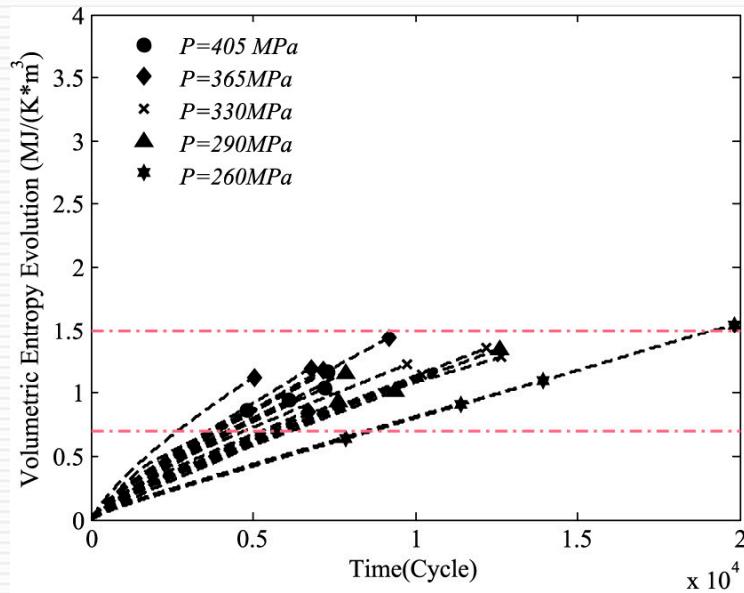
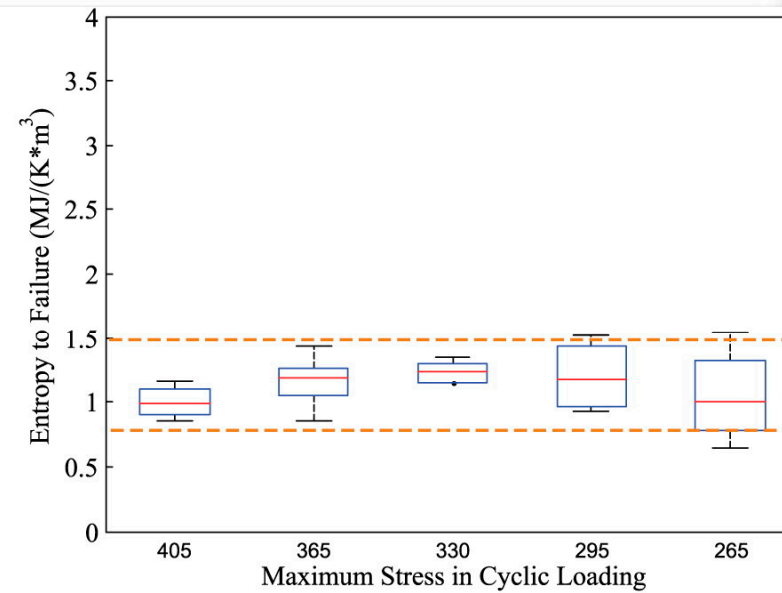


Figure Entropy flow in the control volume under corrosion-fatigue



(a)

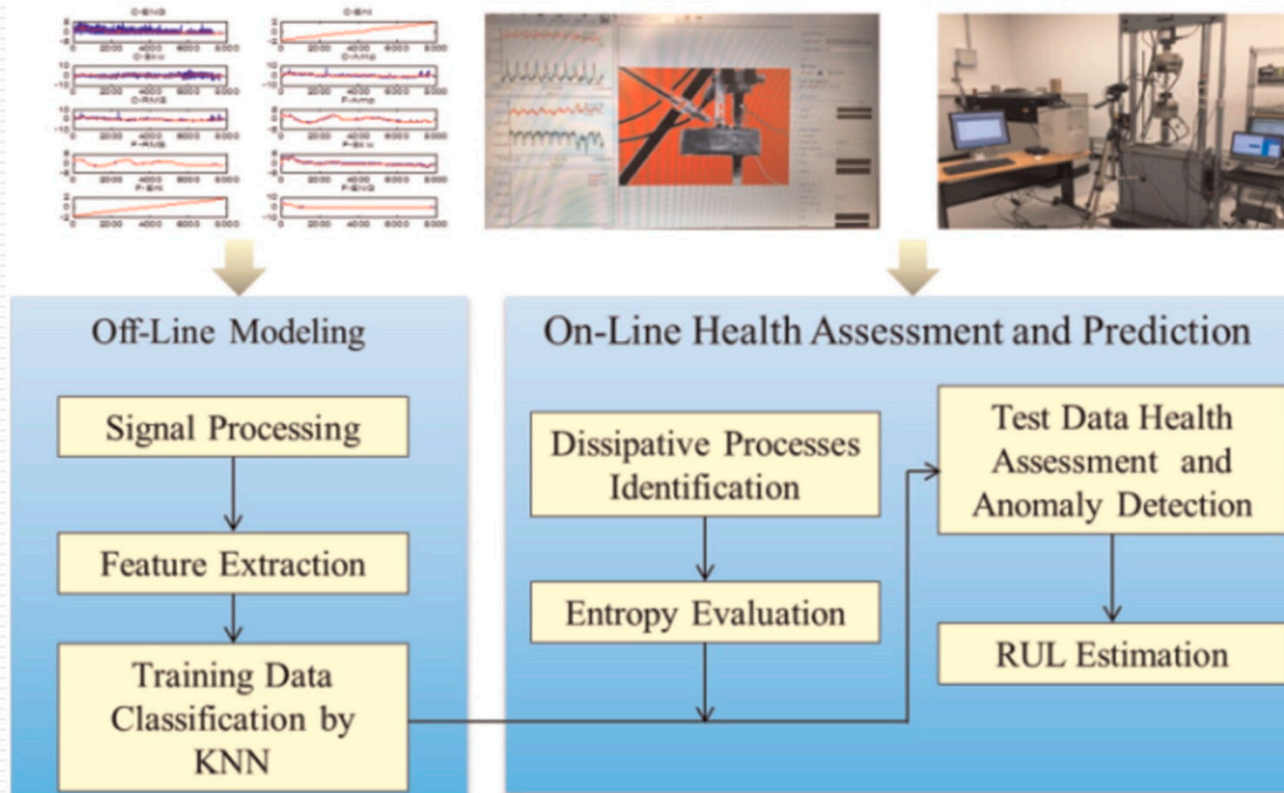


(b)

Volumetric entropy generation evolution. In the Figure 2(a),  $P$  represents the tensile stress.

Imanian, A., Modarres, M., "A Thermodynamic Entropy-Based Damage Assessment with Applications to Prognosis and Health Management", **Structural Health Monitoring**, (2017)

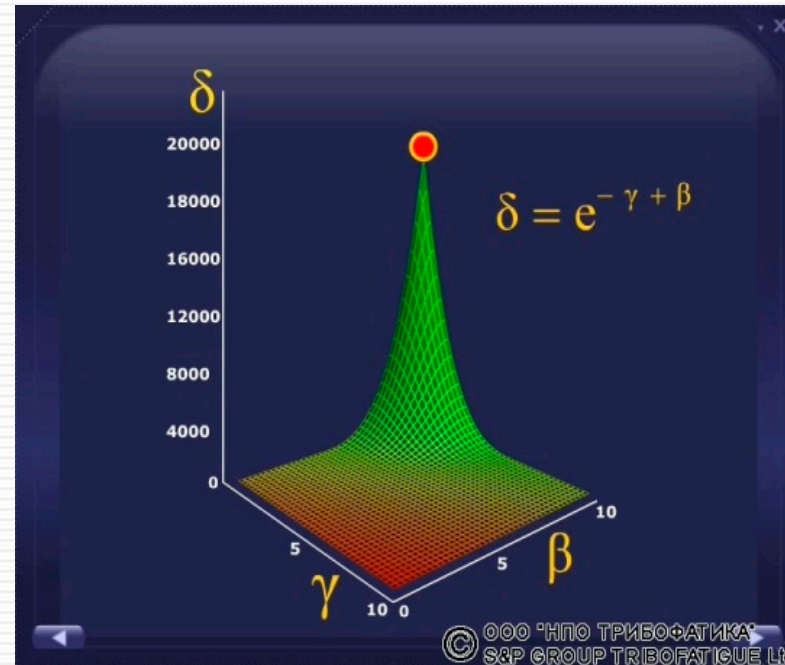
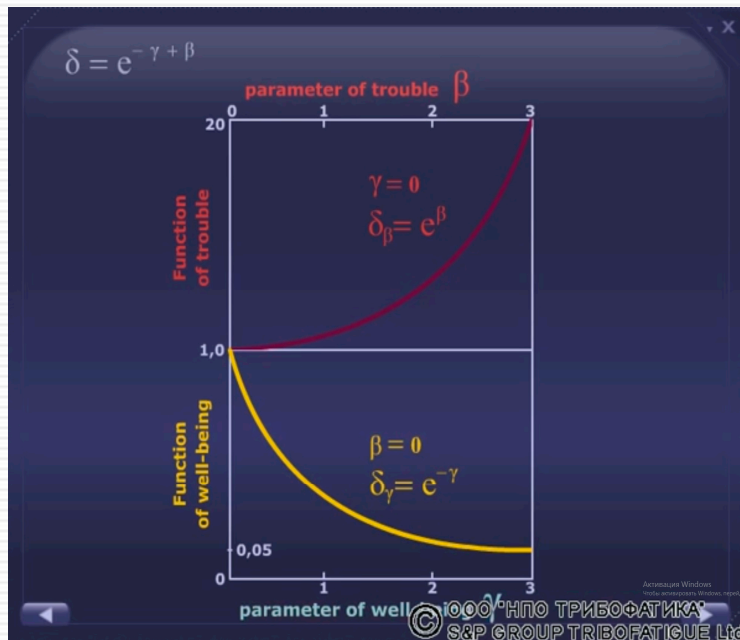
DOI: 10.1177/1475921716689561



The application of the entropy-based Prognosis Structural Health Monitoring

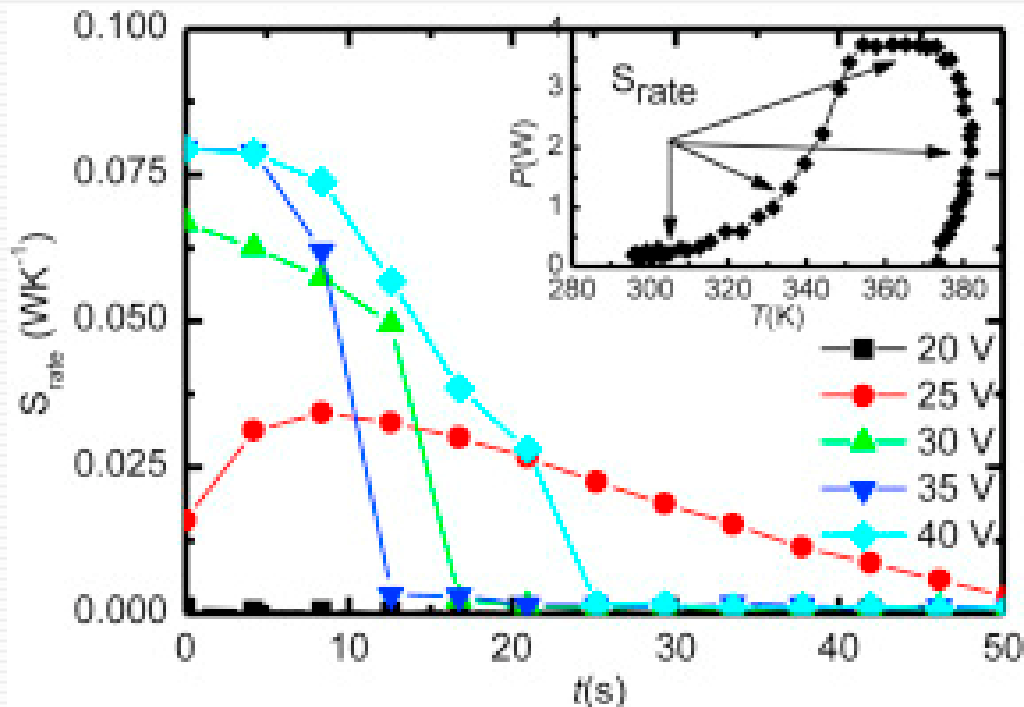
Leonid A. Sosnovskiy and Sergei S. Sherbakov,  
“Mechanothermodynamic Entropy and Analysis of Damage State of  
Complex Systems”, Entropy 2016, 18, 268;

## Healing versus Damage



“Life is a special way of existence of [protein] systems that evolve by the inevitable states of irreversible damage”

Angel Cuadras\*, Ramon Romero, Victoria J. Ovejas  
Entropy characterization of overstressed capacitors for lifetime prediction,  
*Journal of Power Sources*, Volume 336, 30 December 2016, Pages 272-278



“We proposed a method to estimate ageing in electrolyte capacitors based on a measurement of entropy generation rate,  $S_{..}$ .”

Time evolution of, entropy generation rate  $S_{..}$  and capacitance for the capacitor 33 mF capacitor biased with a 4 V pulsed excitation.

Angel Cuadras, Jiaqiang Yao, and Marcos Quilez,”  
Determination of LEDs degradation with entropy  
generation rate” *Journal of Applied Physics* 2018 (in  
print)

## Conclusions

**A correlation between LED's optical fade and entropy  
generation rate was found.**

Note: A Light-Emitting Diode is a two-lead semiconductor light  
source.

It is a p-n junction diode that emits light when activated.



## Applications is Dynamical Systems

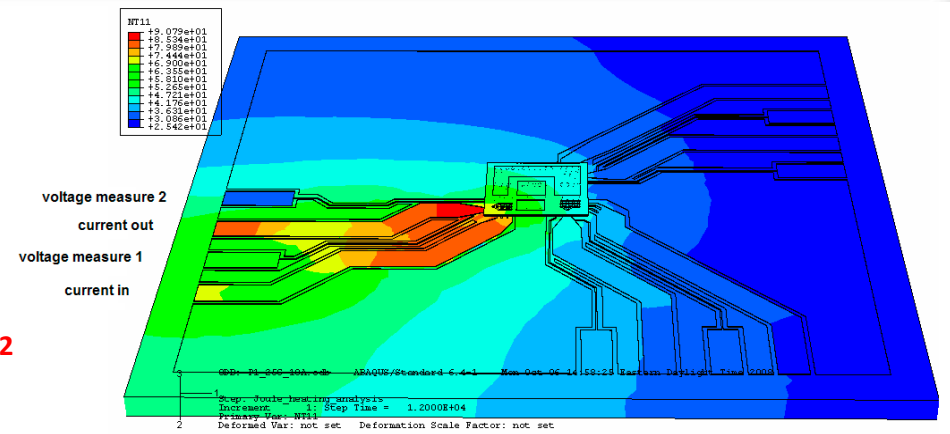
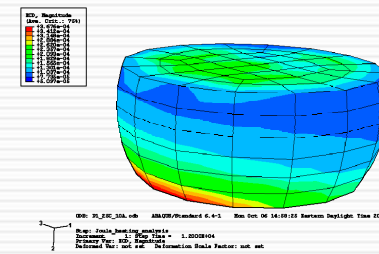
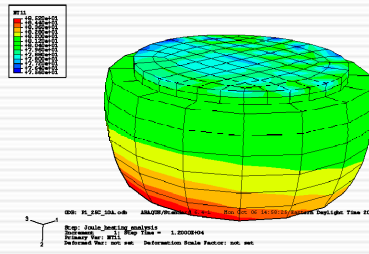
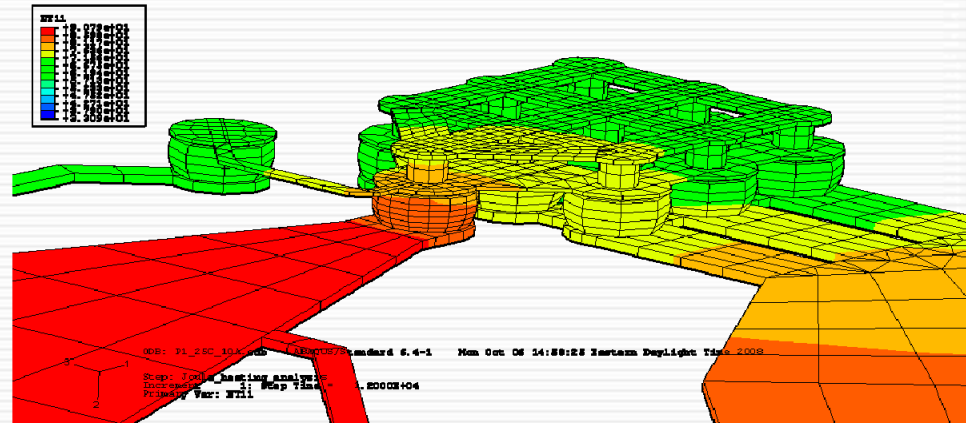
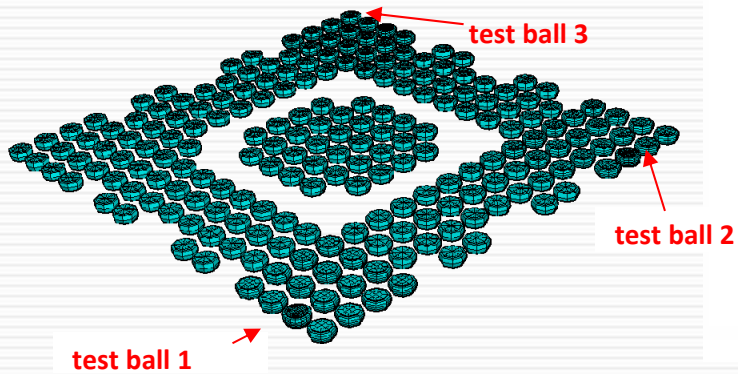
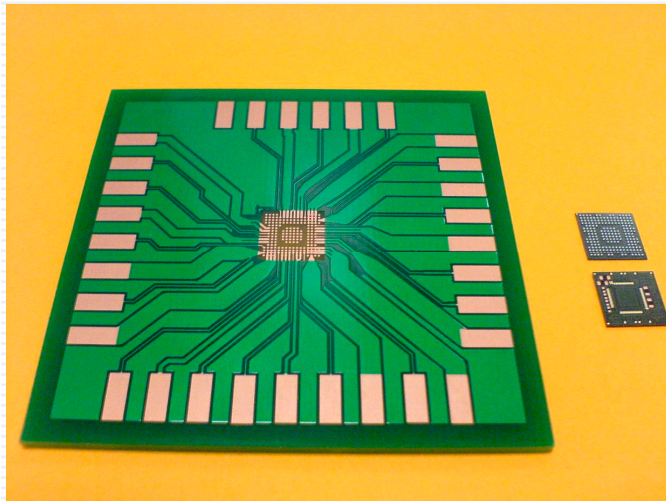
Haddad, W.M. *A Dynamical Systems Theory of Thermodynamics*; Princeton University Press: Princeton, NJ, 2018.

“..... harmonize thermodynamics with classical mechanics [using entropy].”

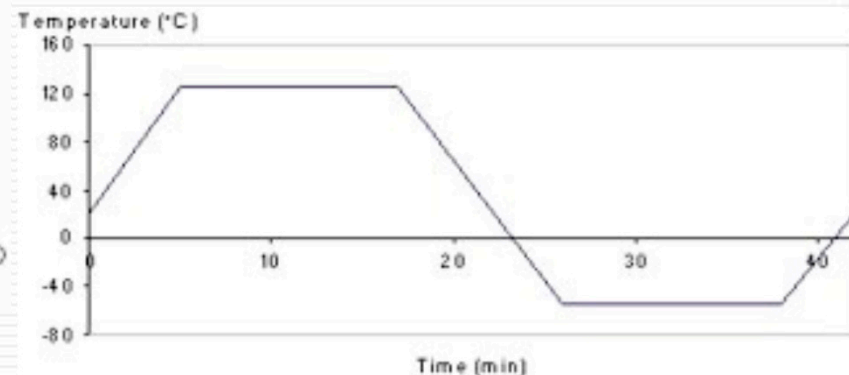
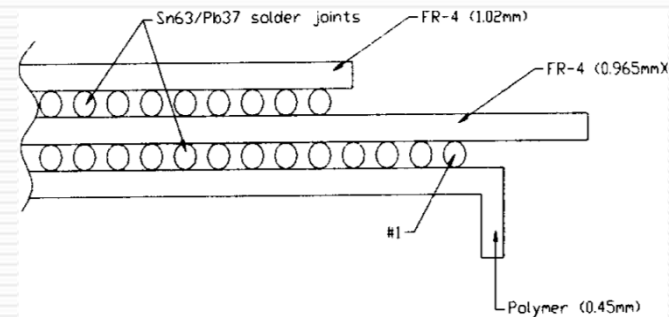
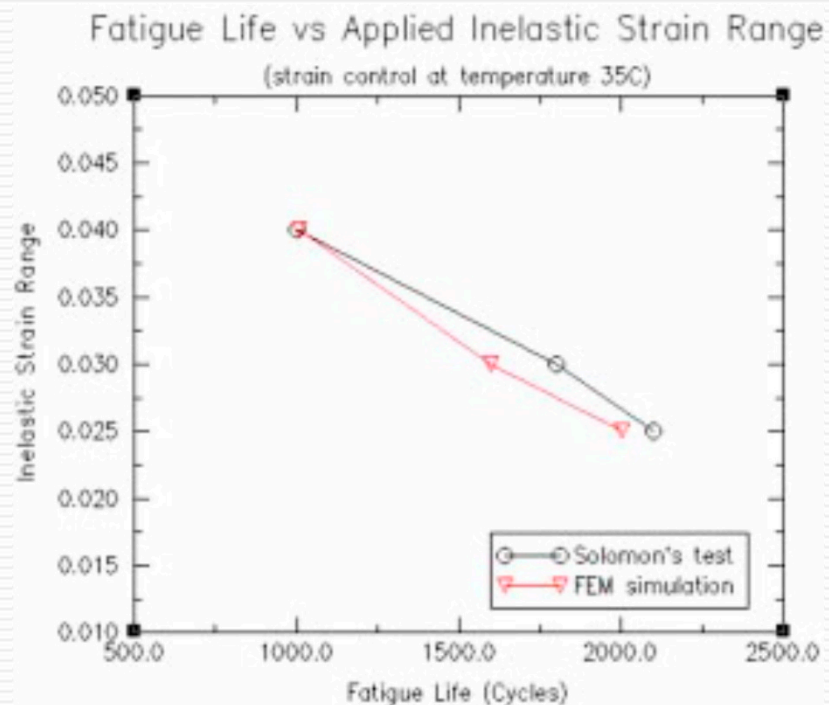
# Electronic Packaging Laboratory

UB University at Buffalo The State University of New York

## Thermal Cycling of a Computer Chip

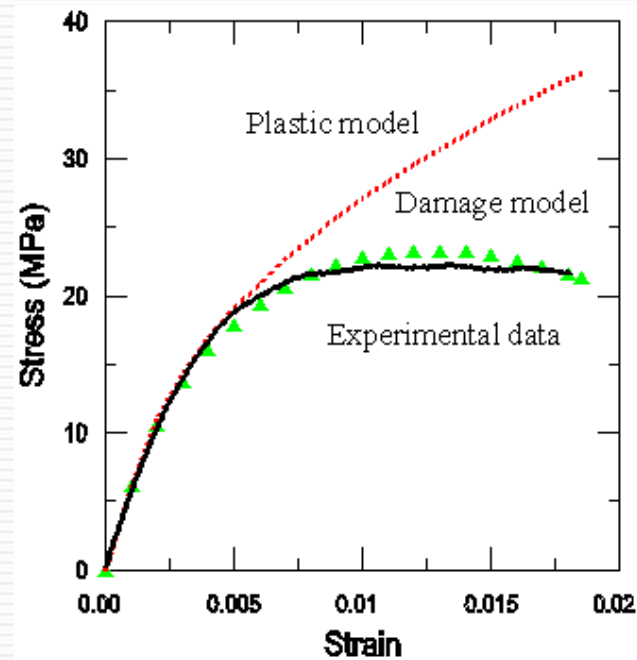
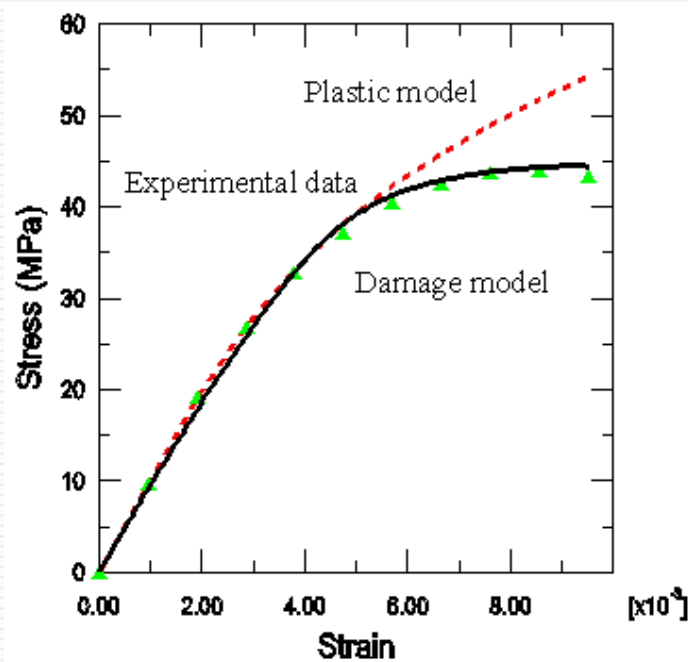
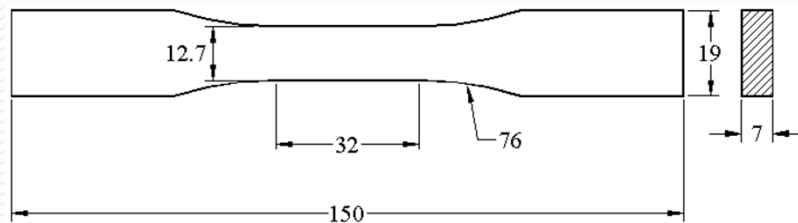


## Fatigue due to Temperature Cycling



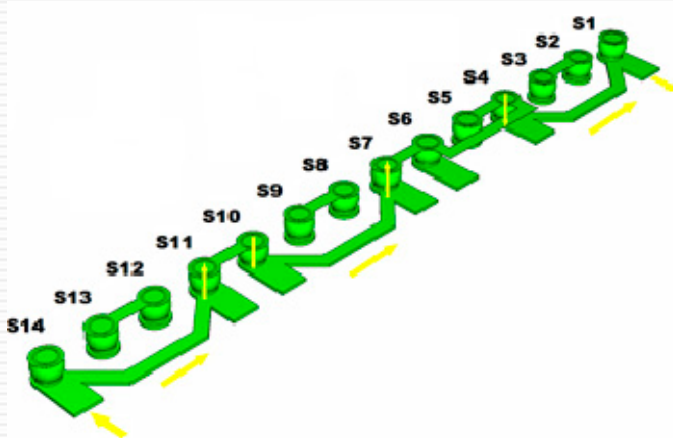
"Implementation of a Thermodynamic Framework for Damage Mechanics of Solder Interconnects in Microelectronic Packaging," *International Journal of Damage Mechanics*, Vol. 11, No. 1, pp. 87-108, January 2002.

## Uniaxial tensile test on Particle Filled Composite

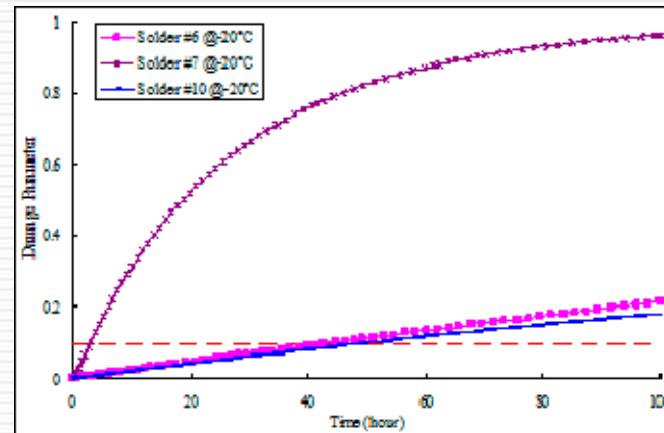


Damage coupled plastic model, Ramberg-Osgood plasticity model and experiment data at 24 °C and 75° C

## DAMAGE Due to Combined ELECTROMIGRATION AND THERMOMIGRATION



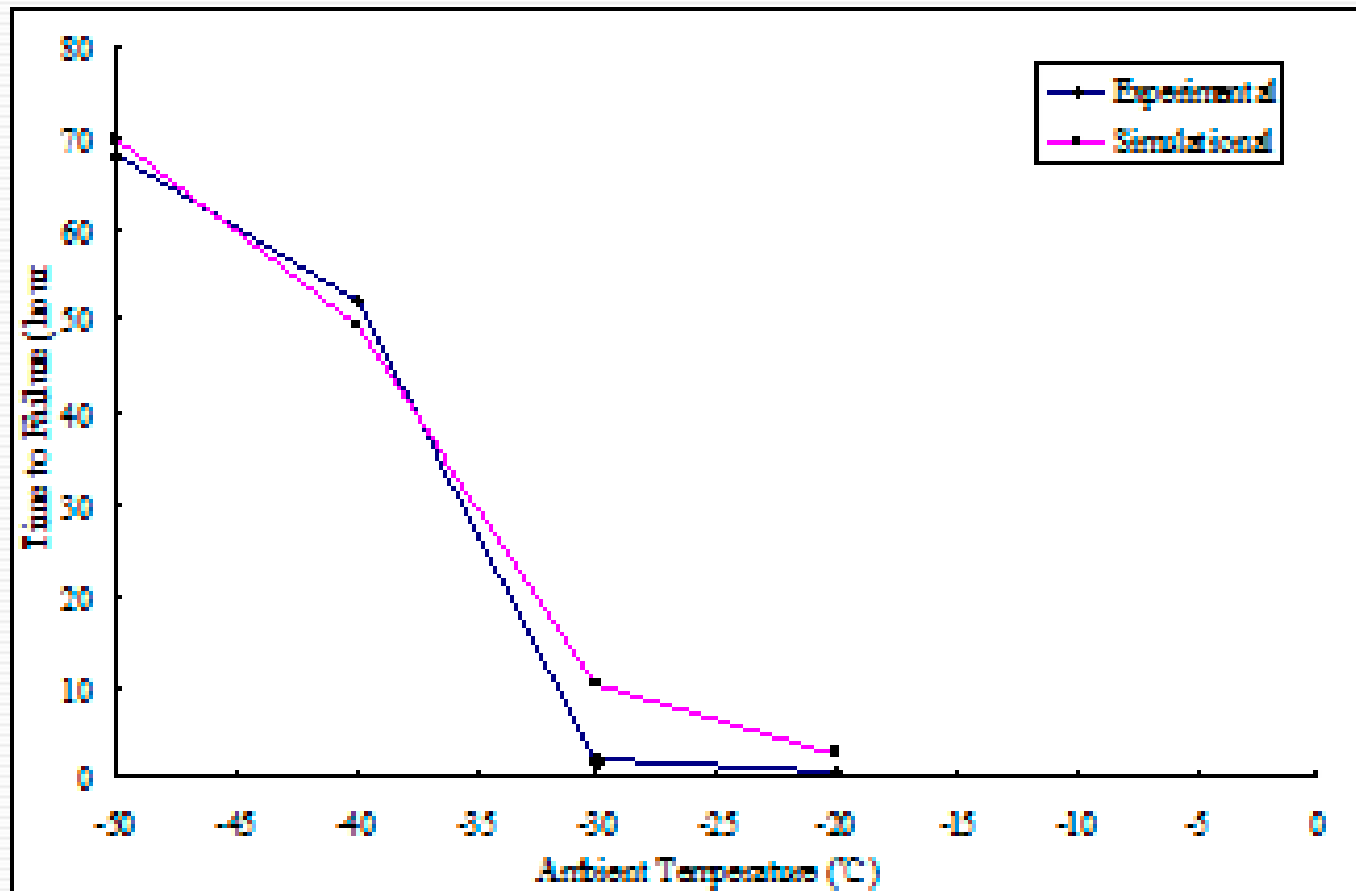
Electrified daisy chain and direction of current



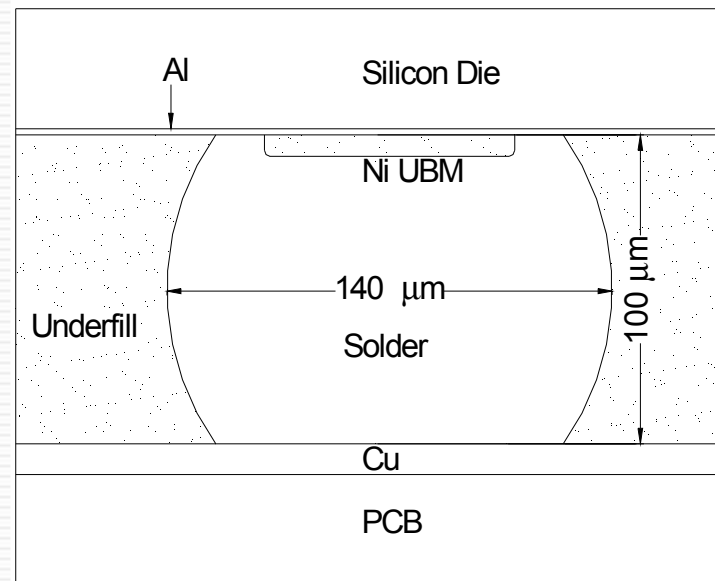
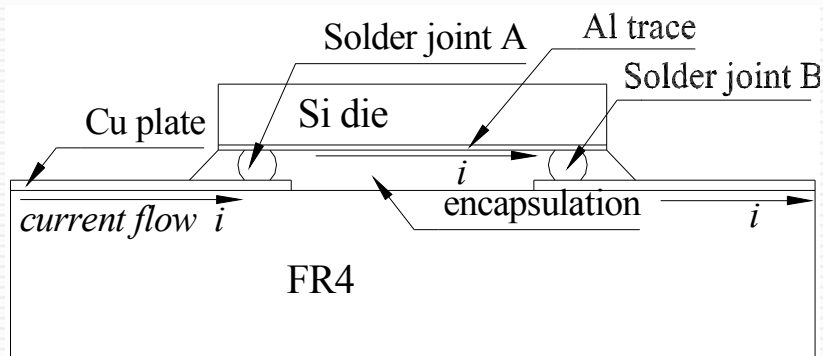
Damage Evolution of 3 solders at  $-20^{\circ}\text{C}$

Comparison of Experiment vs Simulation Results

## Time to Failure under EM + TM for different Ambient Temp



## Damage due to EM + TM

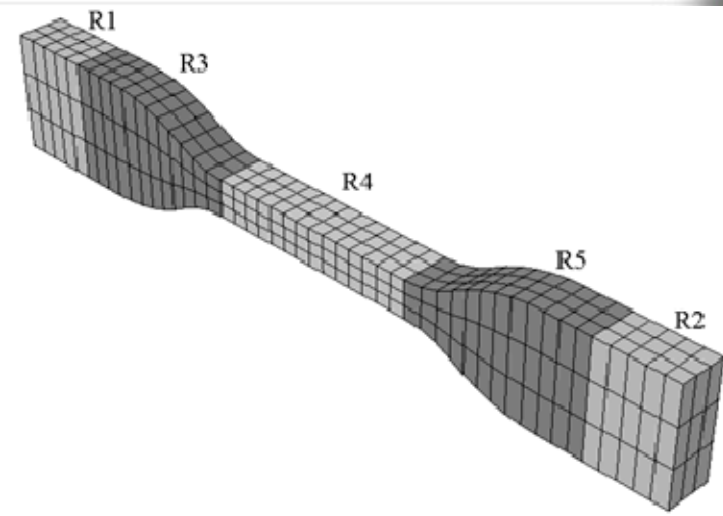
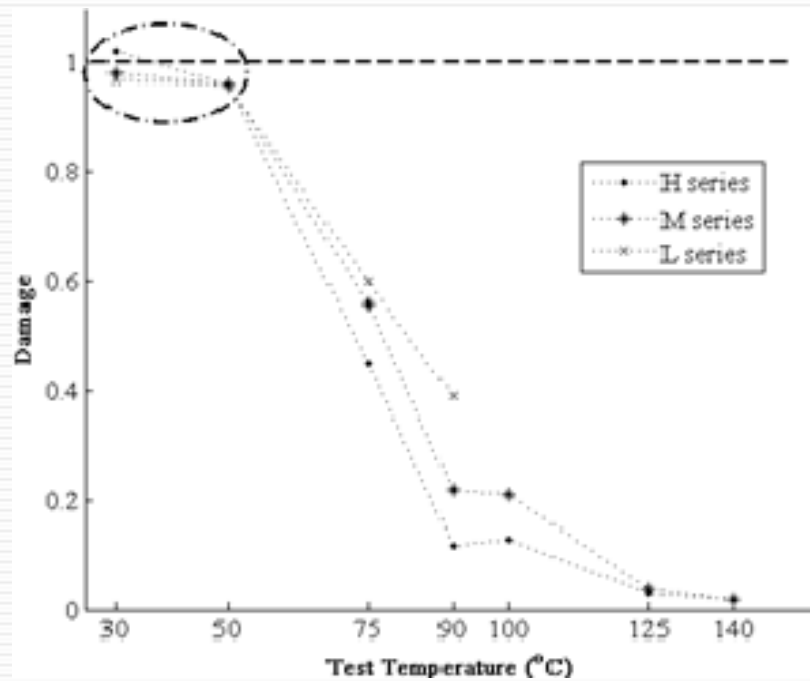


## Time to Failure : Simulation vs. Test Data

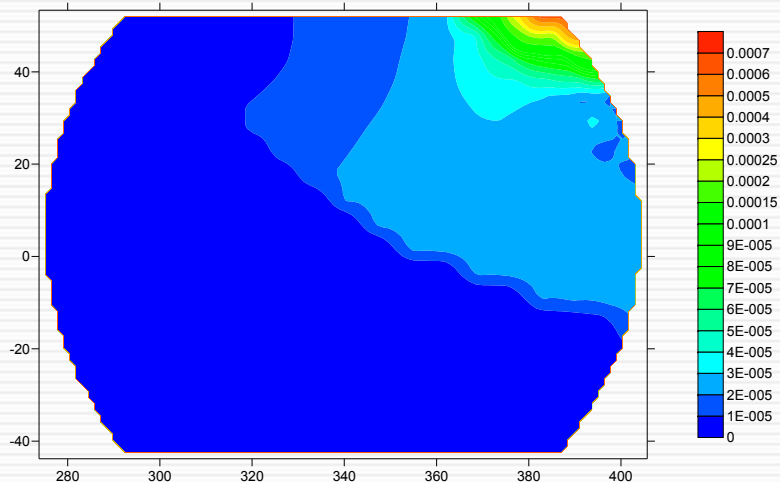
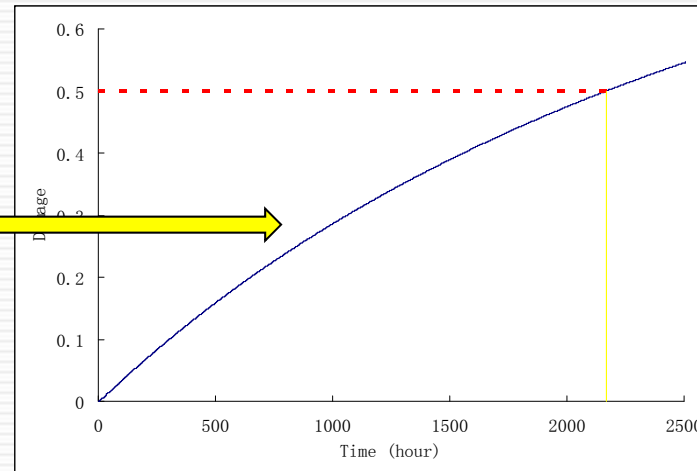
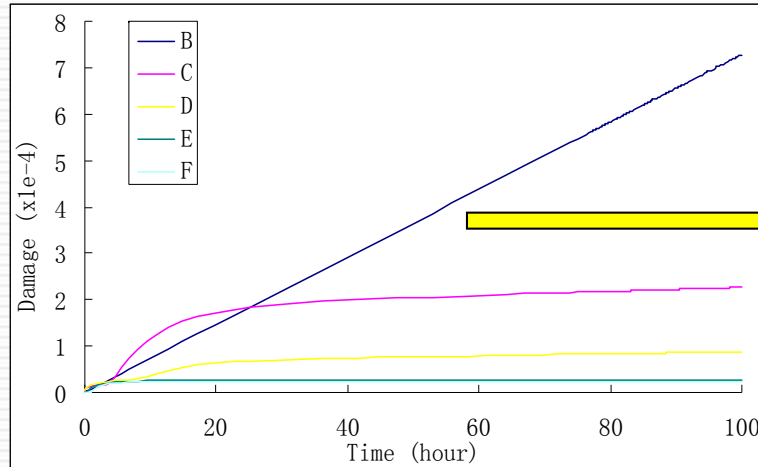
Current Density	Experiment Data $TTF = a/j^3 e^{(b/T)}$	Simulation Results ( $D_{cr} = 1$ )
$1.0 \times 10^4$ Amp/cm <sup>2</sup>	228.7	222.41
$0.8 \times 10^4$ Amp/cm <sup>2</sup>	446.6	435.33
$0.6 \times 10^4$ Amp/cm <sup>2</sup>	1058.7	1098.2



## Simulating Polymer Processing



## Damage Evolution Distribution during TM



➤ damage cease to increase after some time in regions (C, D, E, F)

➤ When the temperature gradient exceeds a threshold, damage will keep accumulating until it fails.

## CONCLUSIONS

- After 150 years of trying a physics based universal degradation evolution model is possible.
- Entropy based model can predict degradation of Inorganic and “organics” systems under any loading including
  - Mechanical
  - Thermal
  - Chemical
  - Electrical
  - Radiation
  - Corrosion
  - Others

## QUESTIONS

