Proceeding

Characterization of the modal parameters of composite laminates using innovative ultrathin polymer waveguide sensor foils †

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Abstract: The use of composite materials, like glass- and carbon- fiber reinforced polymers, is expected to increase exponentially in the coming years. Consequently, in order to monitor the structural health of these materials, the development of new sensing devices is rapidly accelerating. For this purpose, our research groups have recently developed new ultra-thin polymer waveguide sensors which can be exploited to measure both uni- and multi-axial strains occurring in composite components. These sensing foils are manufactured by creating Bragg gratings in waveguides realized in flat polymeric substrates, which makes their placement and alignment easier compared to traditional fiber optic sensors. Moreover, using a non-straight waveguide it is possible to spatially multiplex the sensing gratings in such a way that an optical strain rosette can be created. This paper investigates the suitability of the proposed polymer waveguide sensors for the estimation of the modal parameters of composite components.

Keywords: Bragg gratings; composite materials; polymer sensor foils;;, strain based modal analysis.

1. Introduction

According to market forecasts, the use of composite materials, like glass- and carbon- fiber reinforced polymers (GFRP and CFRP), will be exponentially increasing in the coming years. In the wind energy sector, for instance, the number and size of GFRP wind blades produced per year are in constant grow. As a consequence, the demand of sensor systems for the structural health monitoring of such massive composite structures is also increasing. For this purpose, optical fiber (OF) sensors, such as fiber Bragg gratings (FBG) [1], have recently started to be used as a valid alternative to electrical sensors. OF sensors offer several advantages compared to electrical sensors. For instance, they are small in size and they can be embedded in the composite components during their manufacturing [2] with negligible effects on the material strength. Up to now, most of the FBG sensor networks exploited for this monitoring activity have been based on silica fibers, mainly because these fibers allow low signal attenuation and reduced losses on very long distances. However, polymer optical fiber (POF) sensors [3], like polymer FBG sensors, have also been proposed and tested. POF are in general more competitive than silica OF in terms of costs (the fiber and associated optical links and connectors are generally less expensive); they can be used in applications where large elongations are expected and they have higher thermal sensitivity. Similarly to silica OF, conventional POF sensors are mainly sensitive along the fiber direction, and therefore they require an accurate placement and a precise alignment along the desired measurement direction. In order to decrease the

error measurements associated with OF misplacement and misalignment, optical sensors with planar configuration could be employed. Recently, our research groups have developed new ultra-thin polymeric photonic films which exploit the same sensing principle of conventional FBG being at the same time planar [4]. These foils consist of polymer waveguides (PWGs) realized in flat substrates and inscribed with one or more Bragg gratings. When light is driven inside a PWG, only one wavelength is reflected back, in agreement with the Bragg equation [5]. When a strain acts on the PWG, the reflected Bragg wavelength shifts in the wavelength domain, allowing therefore to measure the applied strain.

Thanks to a smart manufacturing process, the proposed PWG sensors can have a final thickness of 100 μm or lower. Therefore, besides being used as surface glued sensors, they can be embedded in composite laminates in a very low intrusive manner. Apart from the easiness of placement, the developed polymer sensor foils offer the additional advantage of having multiple wavelength-multiplexed gratings inscribed in a single non straight-waveguide, which can be read out using commercial FBG interrogators. This means that, by using a single waveguide, it is possible to achieve multiaxial sensing capabilities and construct a sort of optical equivalent of strain rosette [6].

This article shows how the PWG sensor foils can be used to measure and monitor the dynamic strains occurring in vibrating composite components. This is achieved by performing the estimation of the modal parameters of several composite components. In particular, the following cases are investigated:

CASE 1. GFRP beam-like coupon with surface mounted PWG
CASE 2. CFRP reinforced composite plate with surface mounted PWG
CASE 3. CFRP plate with surface mounted PWG rosette

The article is structured as follows. Section "Materials and Methods" presents the manufacturing of the polymer waveguide sensors, the production of the composite components, the setup and procedure for the experimental campaigns. Section "Results and Discussion" reports and discusses the experimental results for each of the cases under investigation. Section "Conclusions" collect the conclusive remarks.

2. Materials and Methods

The PWG sensors used for this work were manufactured by imprinting Bragg gratings in waveguides obtained in flat polymeric supports. For the un-axial PWG sensors, the support was made of epoxy, while Ormocer® was adopted for the PWG rosette.

The uni-axial PWGs were manufactured by spin-coating a glass substrate (previously treated with a release layer) with a 50 μm thick layer of EpoClad. The EpoClad was softened via heat treatment and imprinted with a stamp to create the desired grating lines. Then, it was cover by a 5 μm thick layer of EpoCore in which 5 μm × 5 μm waveguides were created via selective UV exposure. Successively, a second layer of EpoClad (50 μm in thickness) was spin-coated on top of the waveguides. Finally, the created PWG sensor foil was released from the glass support and cut in several uni-axial PWG sensors using a laser.

The multi-axial PWGs were manufactured by spin-coating on a PET substrate an 18 μm thick layer of OrmoClad in which waveguide channels were created using a stamp. The shape of the stamp was such that non-straight waveguides were created. The stamp was kept in place and the OrmoClad was cured with UV light. The stamp was then removed and the OrmoClad was covered with a 5 μm thick layer of OrmoCore (filling the channels and forming the core) in which three gratings were imprinted by means of a second polymeric stamp. The three gratings were oriented in a $0°$, $45°$, $90°$ configuration. The nominal pitches Λ of the three gratings were slightly different (502 nm, 506 nm, 510 nm) for wavelength multiplexing purposes and chosen to be compatible with commercial interrogators.

One of the uni-axial PWG sensors (planar dimensions 10 mm × 30 mm) was embedded inside a GFRP beam-like coupon (CASE 1, Figure 1a). The coupon was made of 4 layers of UD glass fiber infused with a mix of epikote MGS RIM135 and epicure MGS RIMH137. The PWG sensor was embedded in the midplane. The coupon was cured at room temperature for 24 hours and successively

postcured at 80 °C for 15 hours. Finally, the coupon was trimmed to the desired planar dimensions (40 mm × 110 mm) and the PWG sensor was connected to a single mode fiber (SMF 28) through an in-house developed connector.

A second uni-axial PWG sensor (planar dimensions 5 mm × 30 mm) was glued on top of a CFRP stiffened panel (CASE 2, Figure 1b) made of a flat plate (470 mm × 470 mm) with two omega-shaped stiffeners both made of M10/T300 pre-impregnated material. The plate and the stiffeners were manufactured separately, cured for 8 hours at 120 °C and then assembled with an aerospace adhesive. Finally, the uni-axial PWG was connected to a standard single mode fiber with an in-house developed connector.
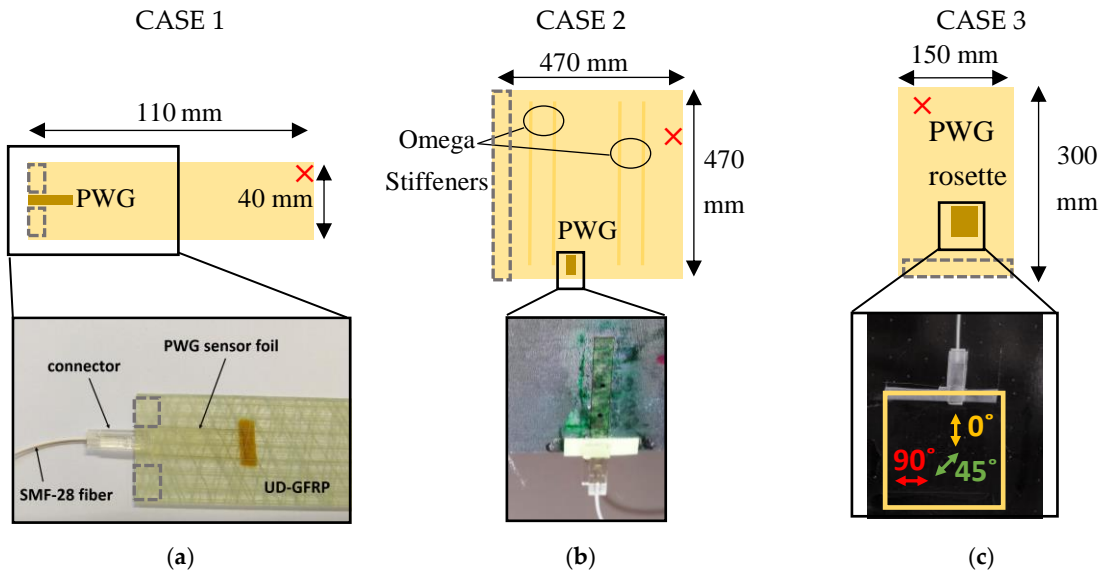

(**a**)   (**b**)   (**c**)

Figure 1. The 3 different cases analyzed. (**a**) schematic representation (top) and particular (bottom) of the beam like GFRP component equipped with an embedded uni-axial PWG sensor. (**b**) schematic representation (top) and particular (bottom) of the CFRP stiffened panel with a surface glued uni-axial PWG sensor. (**c**) schematic representation (top) and particular of the CFRP plate with a surface glued multi-axial PWG. The area enclosed in the dashed rectangles indicate the region used to clamp the components before proceeding with the experiments. The red cross indicates the position of the accelerometer.

The multi-axial PWG sensor was glued on top of a 300 mm × 150 mm CFRP plate (CASE3, Figure1c) with a stacking sequence of (0_8). The plate was manufactured using M10/T300 pre-impregnated material. The PWG rosette was connected to an SMF 28 optical fiber by means of the same type of in-house developed connector mentioned above.

The manufactured composite components instrumented with the PWG sensors were then mounted on rigid supports before proceeding with the modal testing. All three components were clamped (C) along one edge, while the other edges were left free (F), meaning that CFFF type of boundary conditions were selected. In Figure 1, the clamping regions are indicated by the area enclosed by the dashed rectangles in gray. For CASE 1, given the proximity of the PWG sensor to the clamped side and considering the space taken by the optical connector, two metallic spacers were placed between the GFRP coupon and the rigid support. For sake of comparison, an accelerometer was mounted on each of the component (red cross in Figure 1). Then, the components were tested with a roving impact hammer procedure [7]. Figure 2 shows the schematic of the grid points used for each case while Table 1 reports the number of impact locations and averages (per impact location) used in the different cases.

Table 1. Number of impact locations and averages for the three different cases.

	CASE1	CASE 2	CASE 3
# Impact Locations	15	41	18
# Averages per Impact	3	3	3

During the impact, the dynamic strains occurring in the composite components were measured by acquiring the PWGs reflected spectra (acquisition frequency of 1KHz) by means of an FBGS804 [8] interrogator and by processing these spectra with the fast phase correlation algorithm [9]. At the same time, the accelerations were acquired (acquisition frequency of 1KHz) using a NI USB 9234 DAQ and the data acquisition toolbox of Matlab®. Both strain and acceleration data were transformed to the frequency domain and processed via a least-square poly-reference modal parameter estimator (PolyMax) [10]. The results of the modal analysis are reported in the following section.
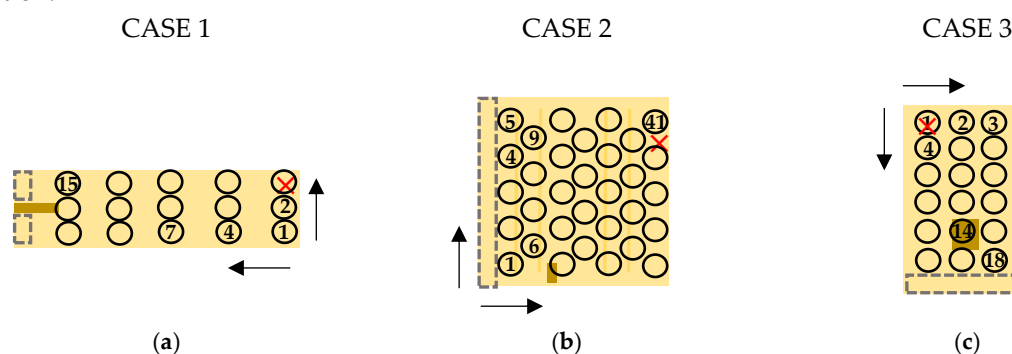

Figure 2. Schematic representation of the locations used during the roving hammer impact test. The circles indicate the impact locations, while the arrows show the movement of the hammer (starting from location 1). For easiness of reading, only few impact point numbers are shown.

3. Results and Discussion

For the estimation of the modal parameters, the frequency bands 0-120 Hz, 0-100 Hz and 0-100 Hz were considered respectively for CASE 1, CASE 2 and CASE 3. Figure 3 shows representative frequency response function (FRF) amplitudes obtained for each of the test cases. Table 2 reports the first three estimated resonance frequencies and damping ratios for both ACC and PWG measurements for all three cases.

A first comparison between the ACC and PWG data shows that, in general, the strain data shows a slightly higher noise content (see dotted-dashed lines in Figure 3). However, the model fitting (Polymax lines) was accurate both for ACC and for PWG. In fact, comparing the resonance frequencies estimated from the PWG data to those obtained from the ACC measurements, the maximum relative difference was limited to: i) 0.237 Hz for the first resonance frequency of CASE 1; ii) 0.241 Hz for the third resonance frequency of CASE 2; iii) 0.32 Hz for the second resonance frequency of CASE 3. Looking at the estimated damping ratios (ζ), the discrepancy was slightly higher due to the fact that the damping estimations are generally more affected by uncertainties. The maximum relative difference on the estimated damping ratios was: i) 0.15% for CASE 1; ii) 1.88% for the first resonance of CASE 2; iii) 0.3% for the first resonance of CASE 3.
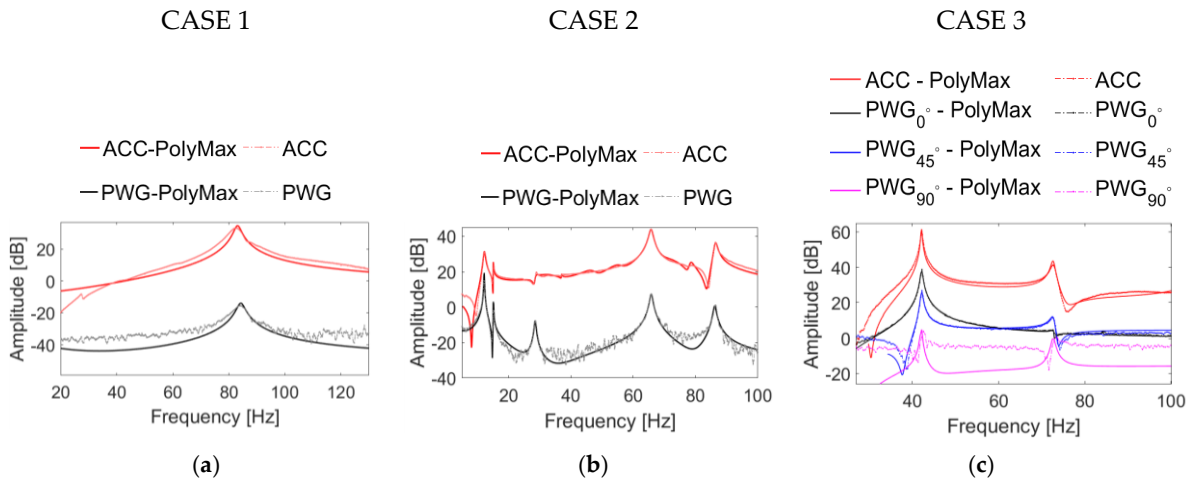
CASE 1   CASE 2   CASE 3

(**a**)   (**b**)   (**c**)

Figure 3. Representative frequency response function amplitudes for the three different cases: (**a**) FRF amplitude obtained for CASE 1 when impacting in location 7; (**b**) FRF amplitude obtained for CASE 2 when impacting in location 4; (**c**) FRF obtained for CASE 3 when impacting in location 14. The continuous line indicates the FRF synthesized by the Polymax estimator while the dotted-dashed line represents the raw data.

The multi-axial sensor shows great sensing capabilities. Looking at Figure 3c, it is clear that, for the first resonance, corresponding to a bending mode in the longitudinal direction of the CFRP plate, the grating oriented $0°$ is more sensitive than the grating at $45°$ which, in turn, is more sensitive than the one in the $90°$ direction. On the other hand, for the second resonance frequency, the gratings at $45°$ and $90°$ are more sensitive than that at $0°$, meaning that the second resonance mode is a torsion around the longitudinal axis of the plate.

Table 2. Estimated resonance frequencies from PWG and ACC data for all three cases.

# Resonance	PWG Frequency f (Hz)					ACC Frequency f (Hz)		
	CASE					CASE		
	1	2	3			1	2	3
			$0°$	$45°$	$90°$			
1	83.22	12.17	42.16	42.15	42.08	82.98	12.21	42.09
2	-	15.14	72.80	72.83	72.66	-	15.08	72.51
3	-	28.68	-	-	-	-	28.44	-

Table 3. Estimated damping ratios from PWG and ACC data for all three cases.

# Resonance	PWG damping ratio ζ (%)					ACC damping ratio ζ (%)		
	CASE					CASE		
	1	2	3			1	2	3
			$0°$	$45°$	$90°$			
1	1.60	0.62	0.62	0.63	0.41	1.45	2.5	0.33
2	-	0.17	0.80	0.70	0.57	-	0.34	0.68
3	-	0.75	-	-	-	-	1.67	-

3. Conclusions

This paper presents for the first time the use of ultrathin polymer photonic sensor foils for assessing the modal characteristics of vibrating composite components. The analysis conducted on GFRP and CFRP components and the comparison with accelerometer data show the suitability of the developed sensors which, in addition, offer the possibility to measure uni- and multi-axial strains both on the surface and inside the composite components.

Conflicts of Interest: The authors declare no conflict of interest. The founding sponsors had no role in the design of the study; in the collection, analyses, or interpretation of data; in the writing of the manuscript, and in the decision to publish the results.

References

1. Luyckx, G.; Voet, E.; Lammens, N.; Degrieck, J. Strain Measurements of Composite Laminates with Embedded Fibre Bragg Gratings: Criticism and Opportunities for Research. *Sensors* **2011**, *11*, 384-408, doi:10.3390/s110100384. Available online: http://www.mdpi.com/1424-8220/11/1/384 (accessed on 17 April 2018).

2. Chiesura, G.; Lamberti, A.; Yang, Y.; Luyckx, G.; Van Paepegem, W.; Vanlanduit, S.; Vanfleteren, J.; Degrieck, J. RTM Production Monitoring of the A380 Hinge Arm Droop Nose Mechanism: A Multi-Sensor Approach. *Sensors* **2016**, *16*, 866, doi:10.3390/s16060866. Available online: http://www.mdpi.com/1424-8220/16/6/866/htm (accessed on 17 April 2018).

3. Peters, K. Polymer optical fiber sensors-a review. *Smart Mater. Struct.* **2010**, *20(1),* 013002, doi:10.1088/0964-1726/20/1/013002. Available online: http://stacks.iop.org/0964-1726/20/i=1/a=013002 (accessed on 17 April 2018).

4. Missinne, J.; Teigell Beneitez, N.; Chiesura, G.; Luyckx, G.; Degrieck, J.; Van Steenberge, G. Flexible thin polymer waveguide bragg grating sensor foils fors train sensing. In Proceedings of the SPIE Photonics West, San Francisco, United States, 28/01/2017; SPIE 101010; 101010X-1-6.

5. Kashyap, R. *Fiber Bragg Gratings*, 1st ed.; Academic Press: London, UK, 1999; pp 153

6. Missinne, J.; Teigell Beneitez, N; Lamberti., A.; Chiesura, G.; Luyckx, G.; Mattelin, M.A.; Van Paepegem, W.; Van Steenberge, G. Thin and Flexible Polymer Photonic Sensor Foils for Monitoring Composite Structures. *Advanced Engineering Materials* **2018**, *20*, 1701127. Available online: https://doi.org/10.1002/adem.201701127 (accessed on 23 February 2018).

7. Allemang, R.J.; Brown, D.L. *Experimental Modal Analysis*, 2nd ed.; VCH Publisher, USA, 1993; pp. 635-750.

8. FBG Scan 804. Available online: http://www.fbgs.com/productsadv/be-en/7/detail/item/17/page/1/ (accessed on 30 November 2017).

9. Lamberti, A.; Vanlanduit, S.; De Pauw, B.; Berghmans, F. A novel fast phase correlation algorithm for peak wavelength detection of fiber Bragg grating sensors. *Opt. Express*, **2014**, 22, 7099-7112, doi:10.1364/oe.22.007099. Available online: http://www.opticsexpress.org/abstract.cfm?URI=oe-22-6-7099 .

10. Peeters, B.; Van der Auweraer, H.; Guillaume, P.; Leuridan, J. The PolyMAX Frequency-Domain Method: A New Standard for Modal Parameter Estimation? *Shock and Vibration*, 2004, *11*, 395-409, doi:10.1155/2004/523692. Available online: http://dx.doi.org/10.1155/2004/523692.