## **WEF** The First World Energies Forum 2020 Current and Future Energy Issues

# Characteristics of ammonia/hydrogen premixed combustion in a novel Linear Engine Generator

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- Introduction
  - Background
  - Objectives
- Methodology
- Mechanism selection
- Results
  - Premixed laminar Flame speed
  - Ignition delay time
  - Flame species
- Summary & conclusions

#### Introduction – background

- Linear Engine Generator (LEG) a novel hybrid–powertrain solution
  - Simpler and more compact structure
  - Lower friction loss
  - More control freedom
  - Wider fuel adaptability
- Ammonia as a fuel carbon-free alternative fuel and potential hydrogen carrier
  - High gravimetric and volumetric hydrogen density
  - Well-established industry of production, storage, transportation and utilization
  - Renewable production technologies are available



[1] Jia, B., et al., *Dynamic and thermodynamic characteristics of a linear Joule engine generator with different operating conditions.* Energy Conversion and Management, 2018. **173**: p. 375-382.



[2] Kobayashi, H., et al., *Science and technology of ammonia combustion*. Proceedings of the Combustion Institute, 2019. **37**(1): p. 109-133.

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- A more detailed and extensive investigation under engine-operation condition is still required to better support the combustion system of the target LEG prototype.
- Identify an ammonia chemical kinetic reaction mechanism
- Parametric study on the effects of equivalence ratio, hydrogen blending ratio, initial temperature and initial pressure on premixed laminar flame speed, ignition delay and flame species

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ANSYS CHEMKIN PRO	
Premixed laminar flame speed modelling	
Ignition delay time modelling	$\bigcirc$
Burner-stabilized flame structure modelling	

Mechanism selection

#### Parametric study

**Chemical kinetic reaction mechanism** 

Otomo's mechanism<sup>3</sup>

Duynslaegher's mechanism<sup>4</sup>

Nakamura's mechanism<sup>5</sup>

Factor	Range
Equivalence ratio	0.8 - 1.6
Hydrogen blending ratio	0.0 - 0.6
Initial temperature	300 – 700 <i>K</i>
Initial pressure	1 – 20 bar

[3] Otomo, J.; Koshi, M.; Mitsumori, T.; Iwasaki, H.; Yamada, K., Chemical kinetic modeling of ammonia 436 oxidation with improved reaction mechanism for ammonia/air and ammonia/hydrogen/air combustion. 437 *International Journal of Hydrogen Energy* **2018**, 43, (5), 3004-3014.

[4] Duynslaegher, C.; Contino, F.; Vandooren, J.; Jeanmart, H., Modeling of ammonia combustion at low 443 pressure. *Combustion and Flame* 2012, 159, (9), 2799-2805.

[5] Nakamura, H.; Hasegawa, S.; Tezuka, T., Kinetic modeling of ammonia/air weak flames in a micro flow 461 reactor with a controlled temperature profile. Combustion and Flame 2017, 185, 16-27.

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#### **Mechanism selection**

Premixed laminar flame speed:  $E\% NH_3 = 20\%$ , 50%, • 80%

10

 $10^{0}$ 

10-"

 $10^{-2}$ 

4.5

5

Ignition delay time [ms]

11atm

Ignition delay: 1.4, 11, 30 atm •

E% NH<sub>3</sub>=80%

Kumar et al.

Otomo et al.

0.6

-Nakamara et al.

-Duynslaegher et al.

30

25

10

5

0

Main species:  $NH_3$ ,  $N_2$ ,  $H_2$ , NO,  $N_2O$ ,  $NH_2$ •



0.8

 $\phi$  [-]

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#### **Results – premixed laminar flame speed**

- increases significantly and non-linearly as more hydrogen is introduced
  - Comparable to the flame speed of methane (~37cm/s) as  $\phi = 1.1$ ,  $x\% H_2 = 0.4$
- peaks when  $\phi$  is around 1.1 1.2•
- Increases with the increasing initial temperature and decreases with the increasing initial pressure ٠
  - Less sensitive to initial pressure under high pressure conditions



x%H<sub>2</sub>=0.0

700

600

500

#### **Results – ignition delay**

- Shorten considerably with hydrogen addition
  - Minor influence as  $x\%H_2$  is over 0.5
- $\phi$  effect is weaker as more hydrogen addition is added
- A high initial temperature and initial pressure environment promotes ignition
  - Minor influence as the initial pressure is over 10 *bar*



#### **Results – flame species**

#### **♦** Equivalence ratio

- *NO* dominates in the *NO*<sub>x</sub> emissions
- With φ increases, NO emission is reduced and H<sub>2</sub> is increased apparently
- *NO* production:
  - HNO + H/OH (fuel-bound NO)
  - $N + O_2/OH$  (thermal NO)
- *NO* consumption:
  - $NO + NH_i/N$
- In the rich flame, the production of fuel-bound *NO* decreases and consumption of *NO* + *N* reaction increases





#### **Results – flame species**

#### Hydrogen blending ratio

- With x%H<sub>2</sub> increases, NO emission slightly increases and H<sub>2</sub> keeps almost unchanged
- *NO* emission increases:
  - Thermal *NO* contribution (production and consumption) increases as  $x\%H_2$  increases
- *H*<sub>2</sub> keeps unchanged:
  - $H_2$  + OH reaction promotes as  $x\%H_2$  increases



#### **Results – flame species**

## Initial temperature and initial pressure

- *NO* emission decreases as the initial temperature rises
  - the rate of both production and consumption is decreased
- *NO* emission also decreases as the initial pressure rises
  - the consumption of *NH<sub>i</sub>* species via the promoted radical combination reactions under high pressure conditions



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- Nakamura's mechanism is employed for parametric study.
- An optimized equivalence ratio exists around 1.1 1.2.
- Increasing hydrogen will not cause a large increase in *NO* emissions at a certain φ, while helping to promote the flame speed and ignition.
- High-pressure high-temperature environment is favourable for improving ignition and low *NO* emission from  $NH_3/H_2$  combustion.



## Thank you!







