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Investigation of guided wave interaction with discontinuities in the axisymmetric damped waveguide

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Introduction:

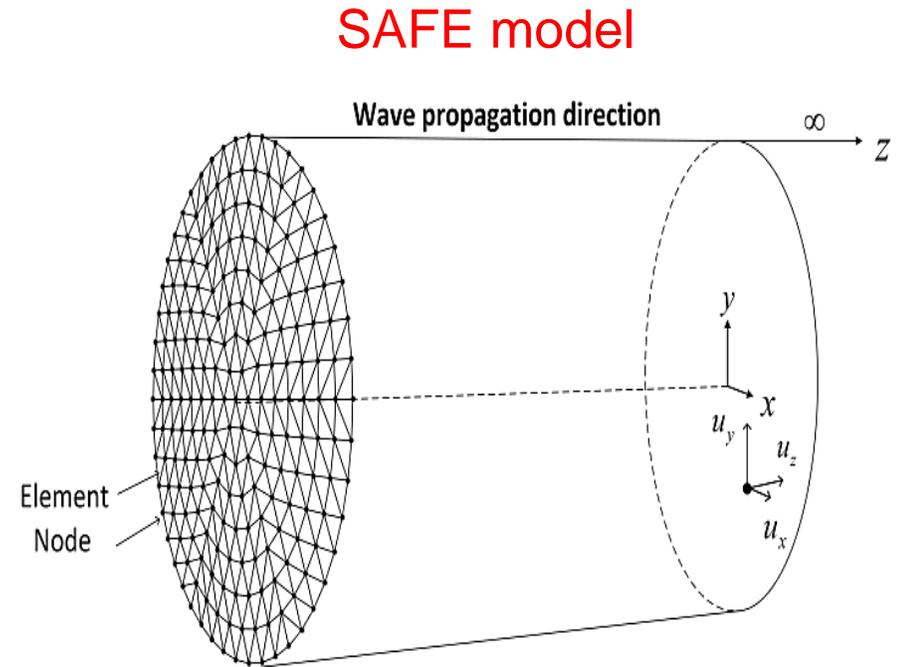
- ✓ SHM and NDE techniques are utilized to monitor wire breakage, and one of the prominent methods is to practice guided **ultrasonic wave propagation** and **acoustic emission (AE)** monitoring.
- ✓ Due to **pitting corrosion** and other breakages, the **load-carrying** capacity of **bridge cables** is affected. It is of paramount importance for the bridge engineers and stakeholders to monitor the existing infrastructures.
- ✓ The **axisymmetric semi-analytical finite element (SAFE) method** is used to study wave properties of a **cylindrical waveguide**, especially, a **high strength steel wire**.
- ✓ This paper discusses the hybrid standard **3D FE and SAFE** method.
- ✓ In this paper, the numerical modeling of **wave scattering** by a **structural discontinuity** (cable damage) in **axisymmetric steel wire - viscoelastic waveguide medium** for analyzing the wave interaction by **inhomogeneity**.

Simulation of scattering and reflection of AE signals

- The **mathematical framework** for an infinitely long, **axisymmetric waveguide** immersed in a vacuum is represented using **the semi-analytical method**.

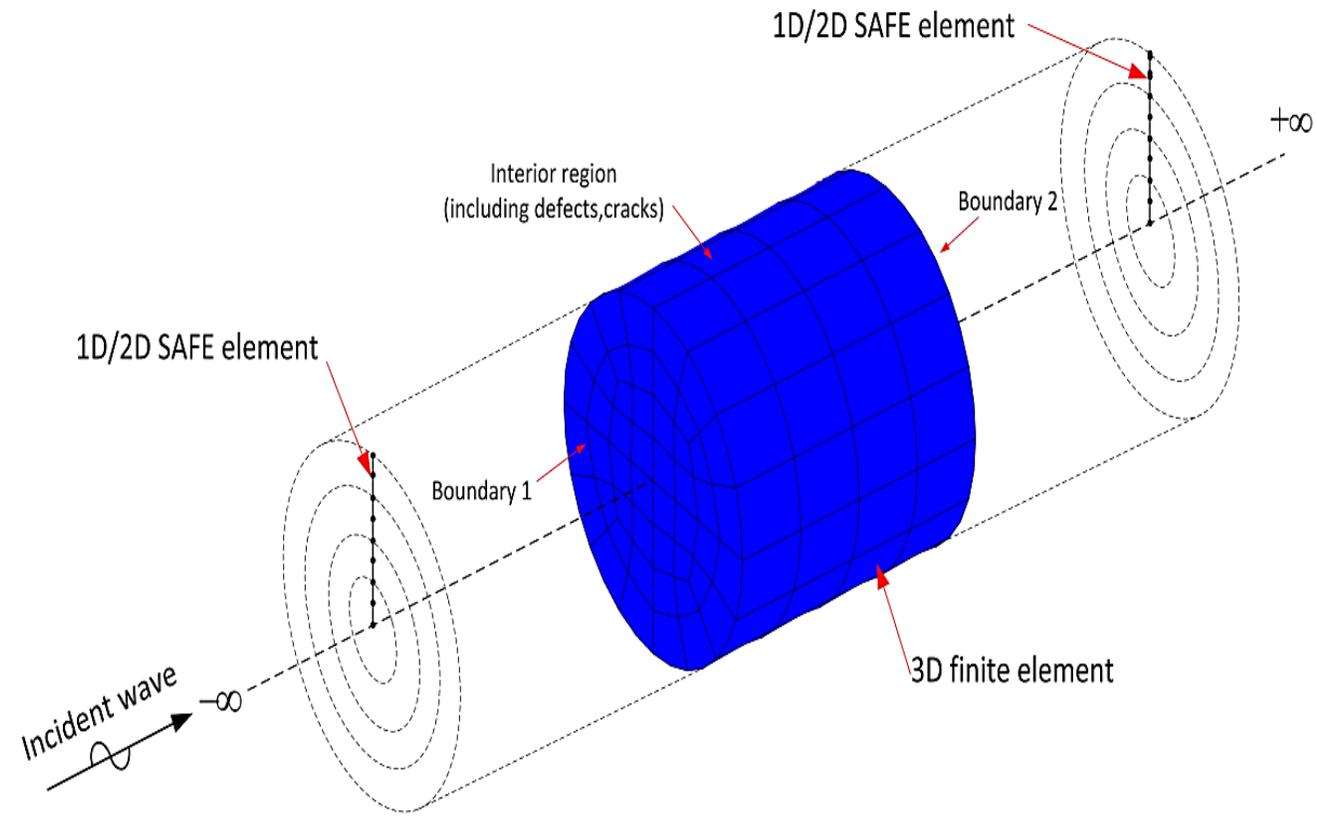
(Hayashi et al., 2003; Bartoli et al., 2006; Marzani et al., 2008)

- The method is established in a **rectangular Cartesian coordinate system**, and the cross-section of the waveguide medium lies in the **x-y plane**.
- Figure shows a **SAFE model** representing fluctuations in the **temporal and spatial** domain along the wave propagation axis z with **wavenumber**, k , and **frequency**, ω .



Mathematical framework for the Hybrid 3D FE-SAFE method

- For the area simulated by the SAFE method, either the **general section method** or the **axisymmetric section semi-analytical method** can be used.
- An example diagram of the **hybrid FE-SAFE**, in which composite parts such as **defects and cracks** need to be included in the **3D-FE area**.
- Consider the **steady-state response** of the 3D-FE area unit under **external excitation** at a particular frequency.



- Basic **structural dynamic formula** used, \mathbf{K} , \mathbf{M} are the general structural stiffness matrix and mass matrix

$$(\mathbf{K} - \omega^2 \mathbf{M}) \mathbf{U}^\omega = \mathbf{F}^\omega$$

$\mathbf{U}^\omega, \mathbf{F}^\omega$ are steady-state structural response & external excitation vectors

Implementation of Hybrid 3D FE-SAFE method

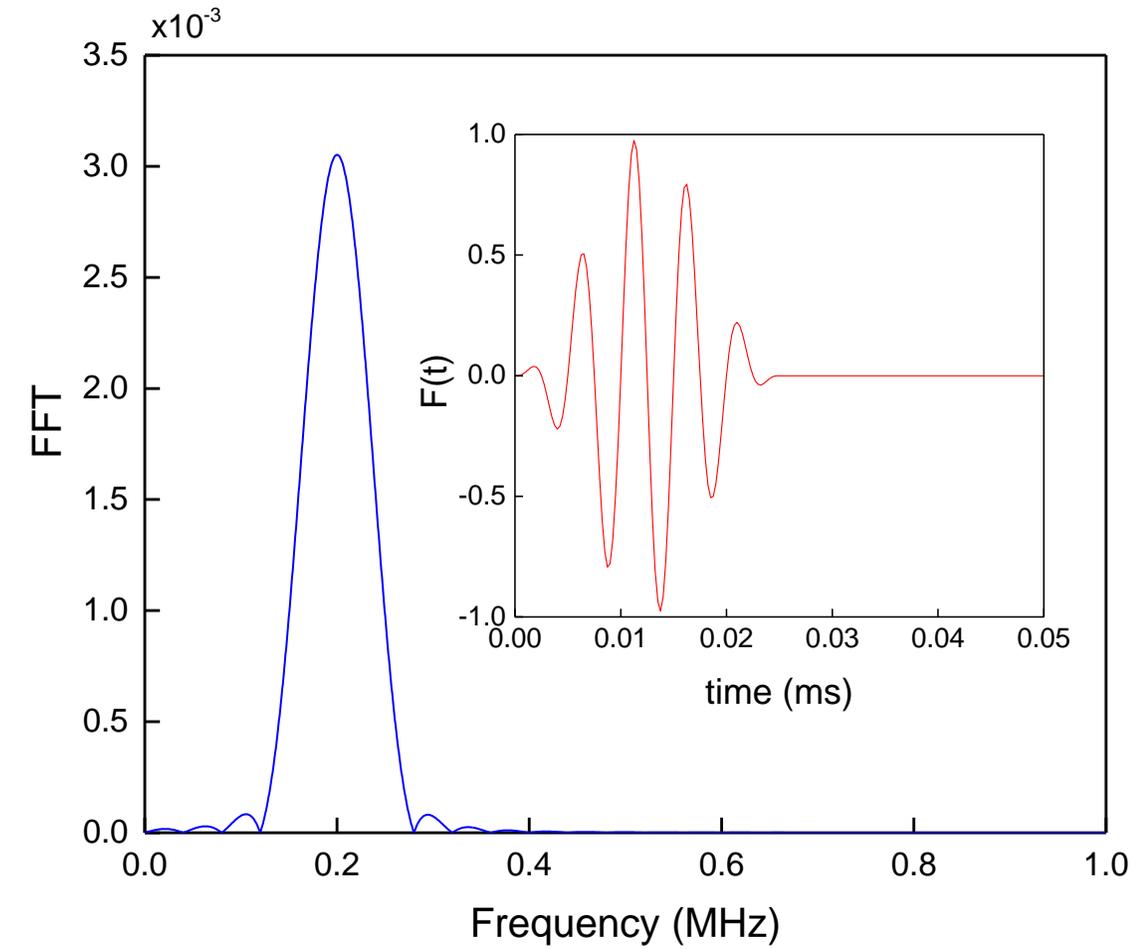
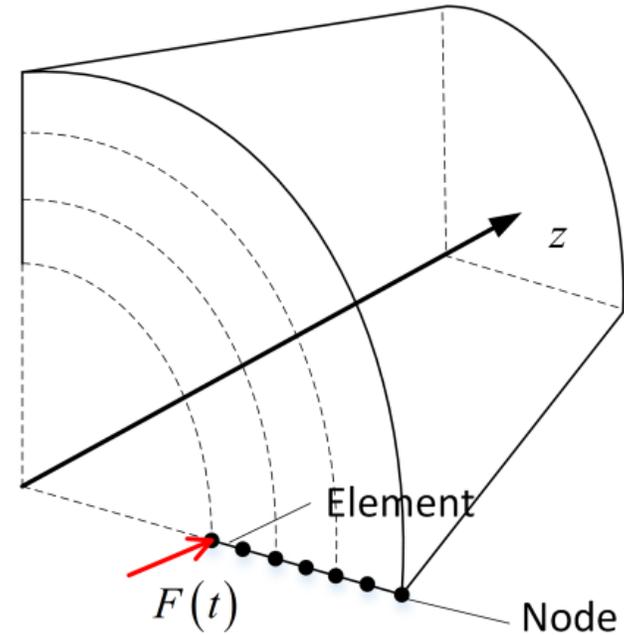
- Theoretically, the **modal superposition method** needs to be applied to the $-\infty$ to B1 or B2 to $+\infty$ cross-section as per the number of available DOF.
- It is computationally expensive, and most evanescent wave components will **attenuate** sharply to **near zero** within the 3D-FE region.
- For the 3D-FE region, the **energy** carried by the **incident wave** (input from the B1 section) should be equal to the **sum of** the energy carried by the **reflected wave** (output from the B1 section) and the **transmitting wave** (output from the B2 section).
- The measure of energy can still use the z-direction **Poynting vector** component. The **total energy ratio** is defined as,

$$R_{eg} = \frac{\operatorname{Re}(P_{refl}^z) + \operatorname{Re}(P_{trans}^z)}{\operatorname{Re}(P_{inc}^z)}$$

P_{refl} , P_{trans} , and P_{inc} are the sum of the z components of the various modal Poynting vectors. The subscripts *refl*, *trans*, and *inc* represent reflected, transmitting, and incident wave, respectively.

Numerical investigations: Analysis of wave propagation

- A high-strength steel wire with a diameter of 5 mm is considered for numerical investigations.

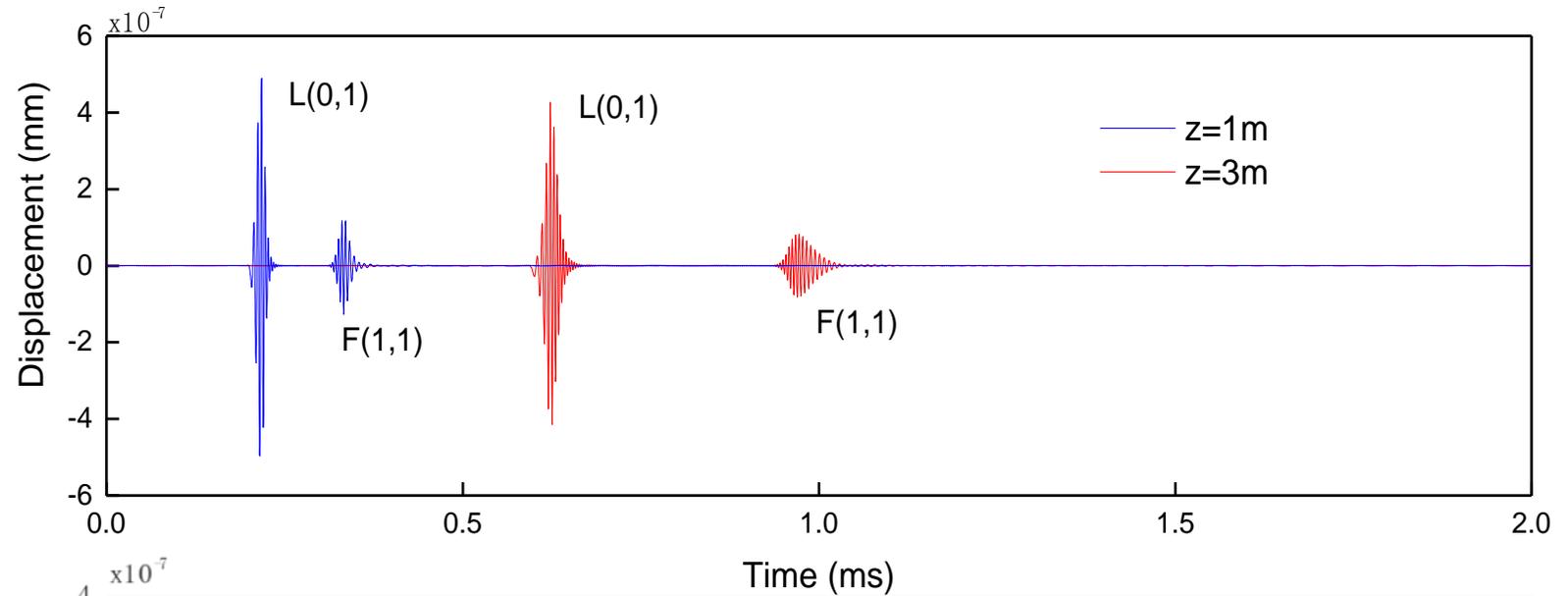


Young's Modulus, E (MPa)	Density, ρ (kg/m ³)	Poisson's ratio, ν	Diameter, d (mm)	Longitudinal wave velocity, C_L (m/s)	Shear wave velocity, C_S (m/s)
2×10^5	7850	0.3	5	5856.4	3130.4

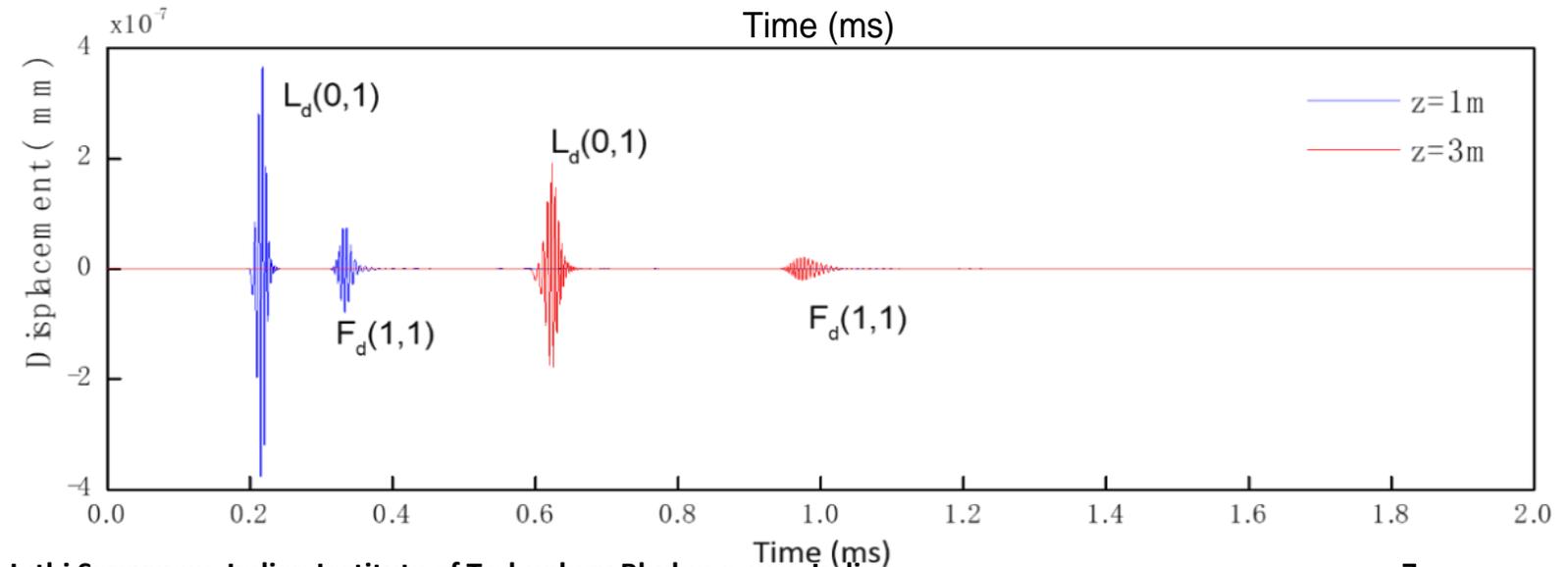
Longitudinal and flexural modes in an undamped and damped steel wire representing axial displacement response

@ distance z equal to 1 and 3 m

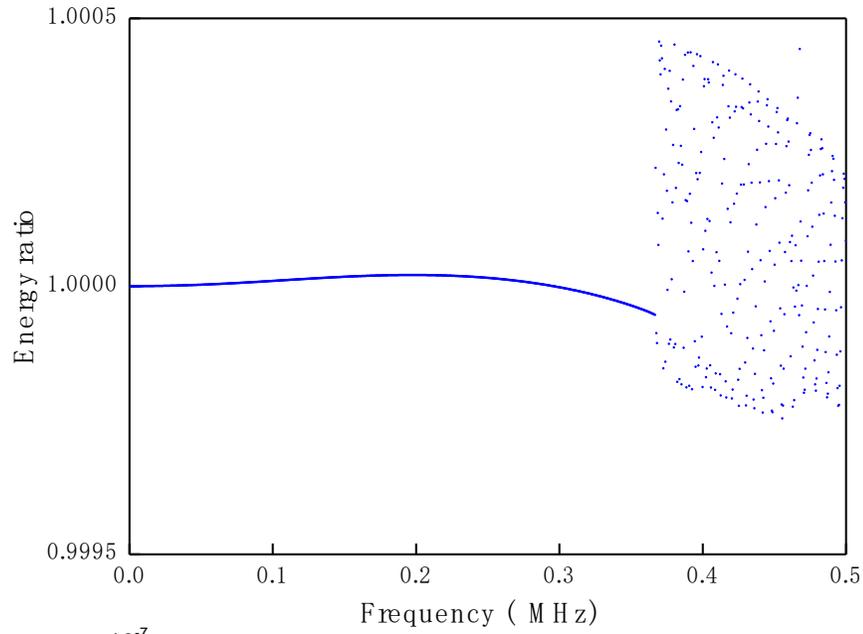
(a) undamped wire



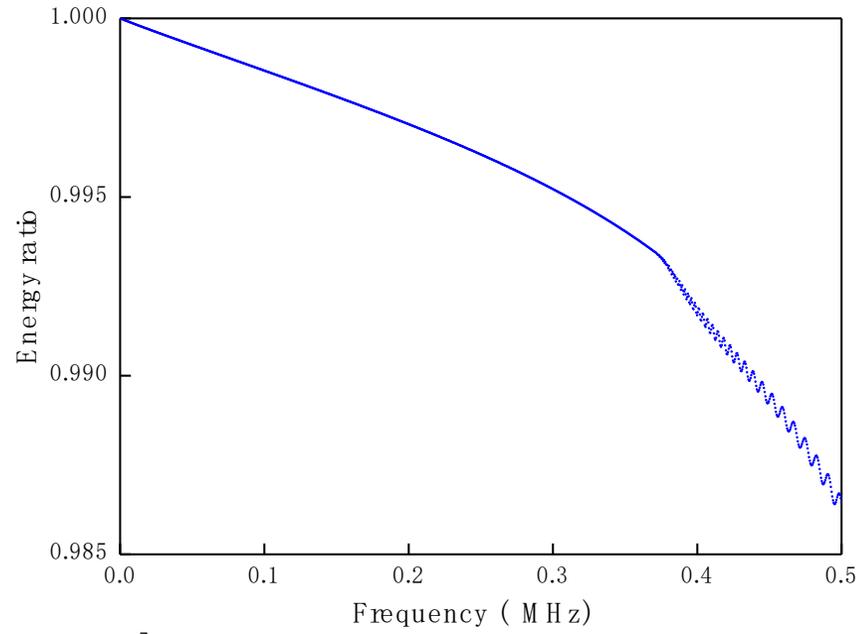
(b) damped wire



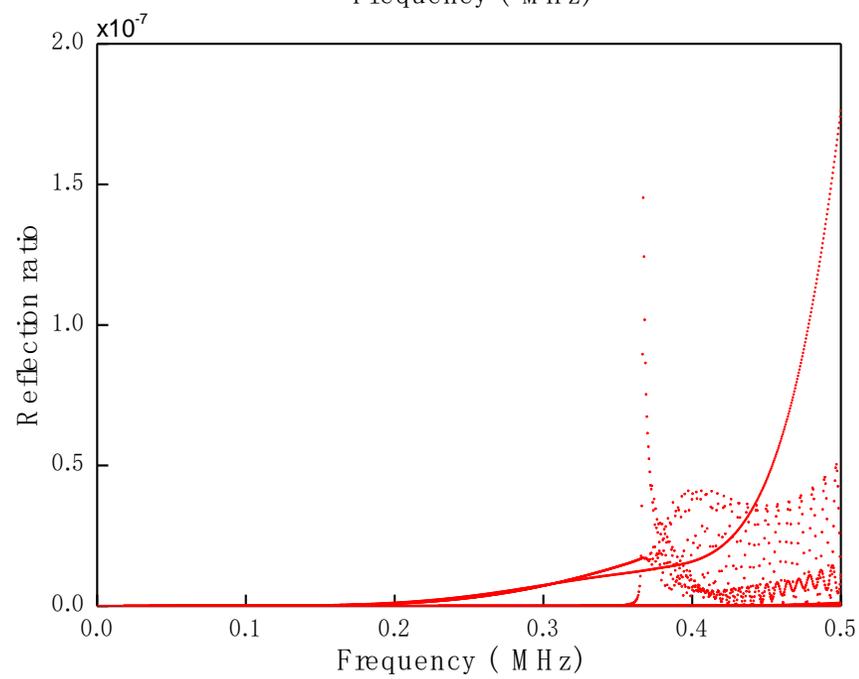
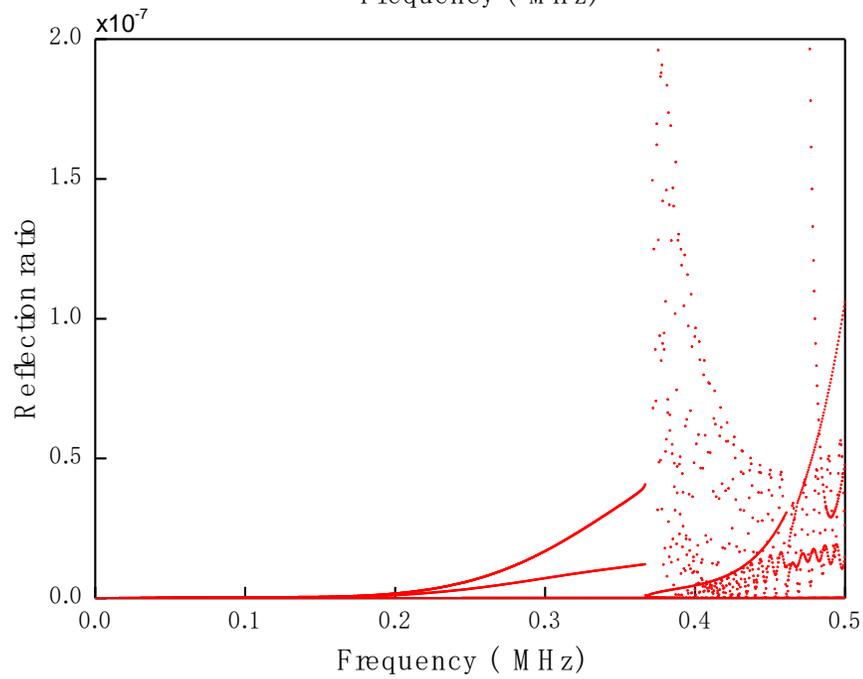
Undamped case



Damped case

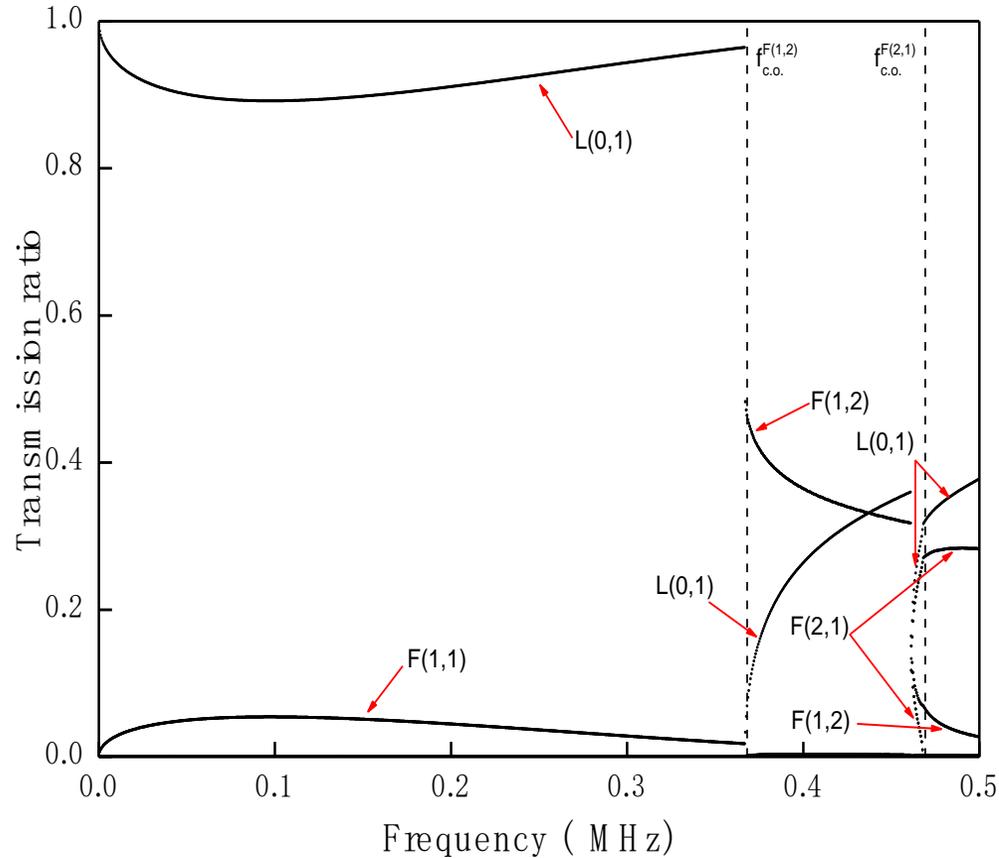


Total energy ratio plot

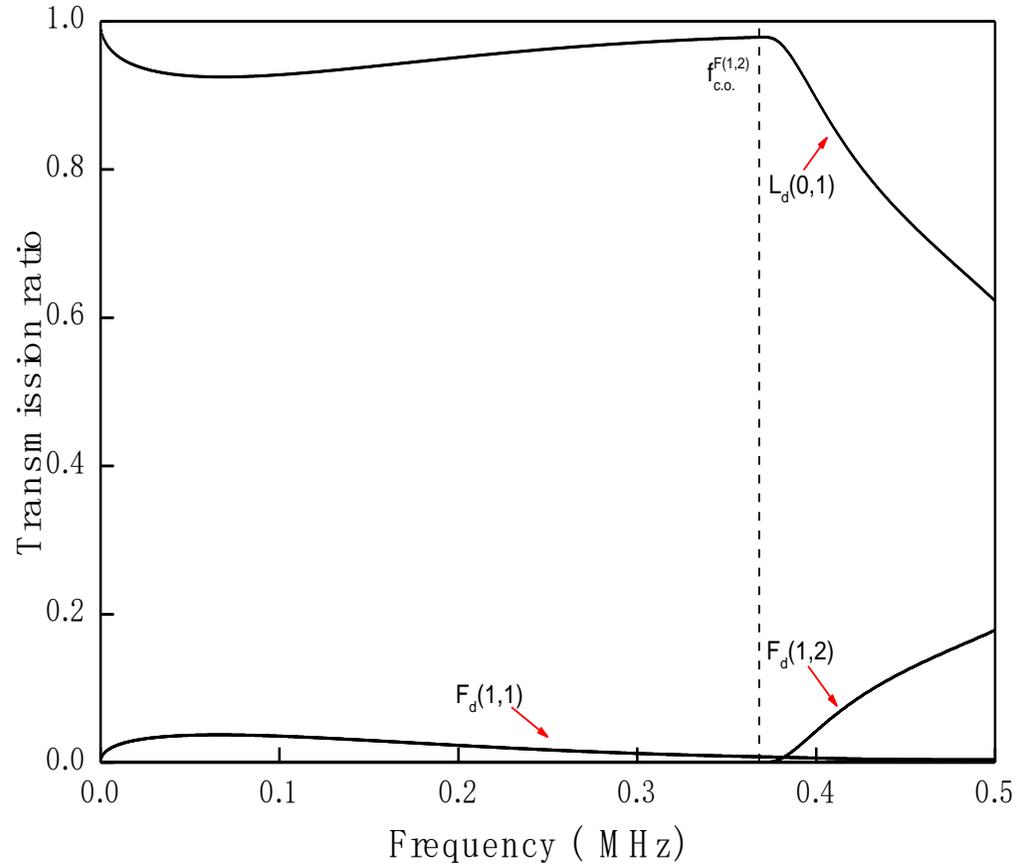


Reflection ratio plot

Undamped case



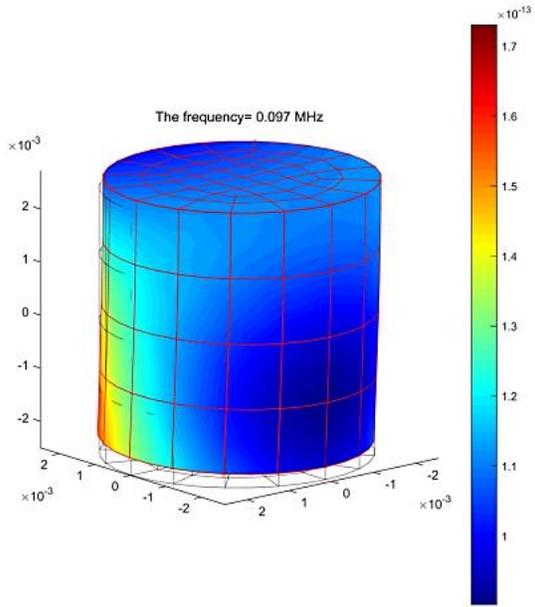
Damped case



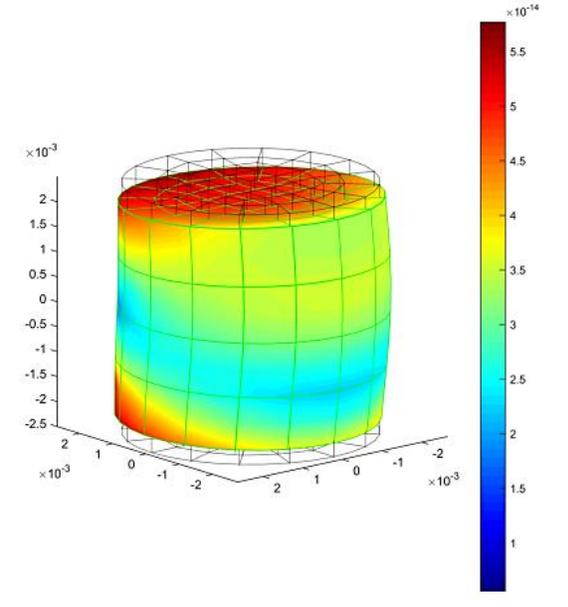
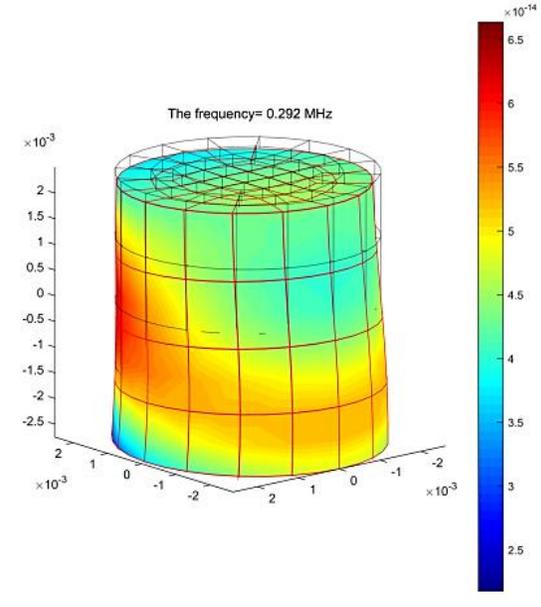
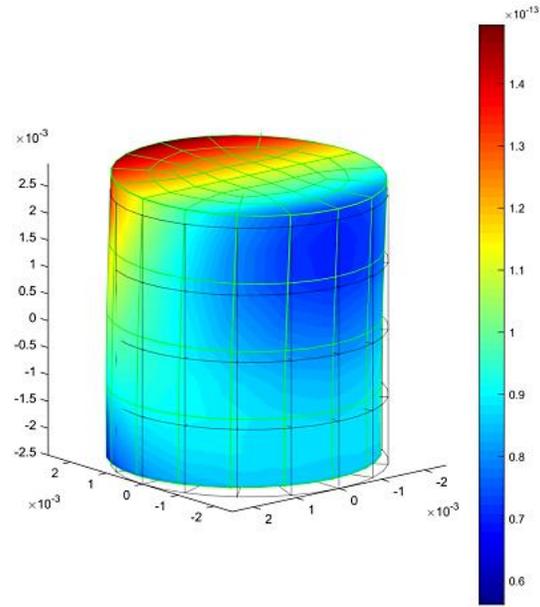
**Transmission
ratio plot**

The curve becomes continuous, and the energy-carrying mode decreases where only $L(0,1)$ and $F(1,1)$ modes appear in the area above 0.37MHz. By considering the material damping, the modes that are initially shown in the undamped case around the cut-off frequency have a huge attenuation factor.

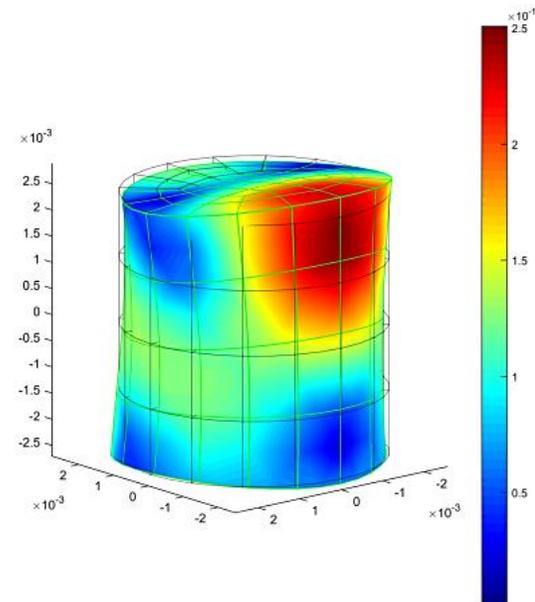
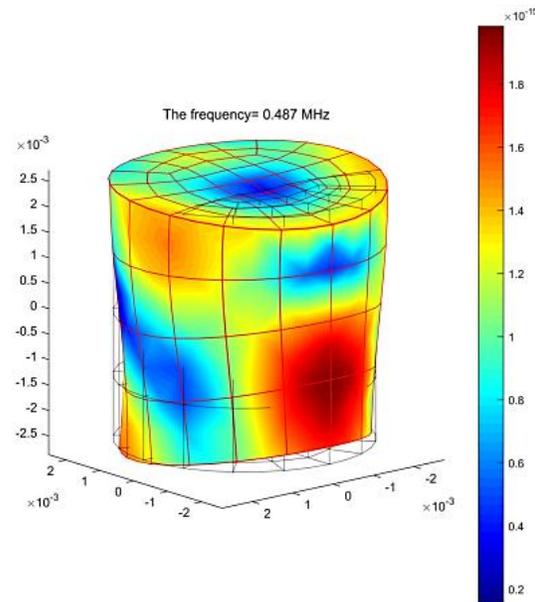
3D-FE area axial-displacement distribution plot at various frequency



At $f = 0.097\text{MHz}$



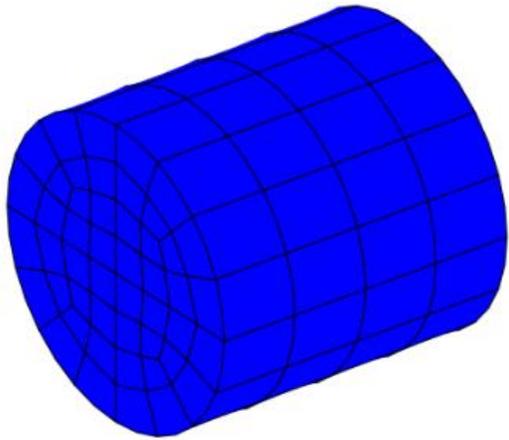
At $f = 0.292\text{MHz}$



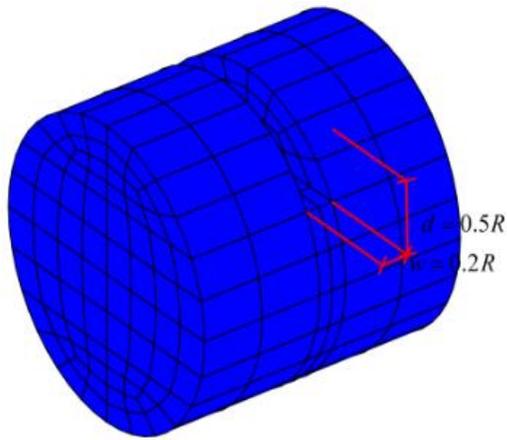
At $f = 0.487\text{MHz}$

Analysis of wave scattering due to structural discontinuity

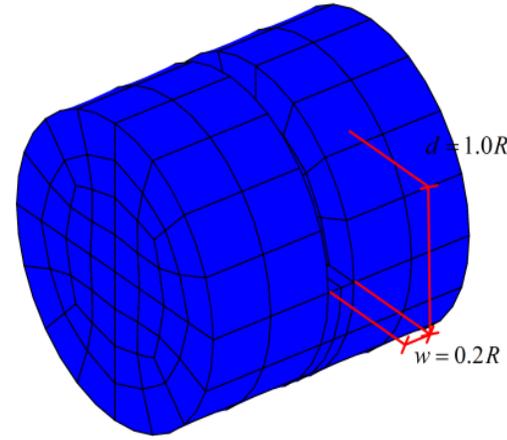
- Pitting corrosion models of steel wire for various depths



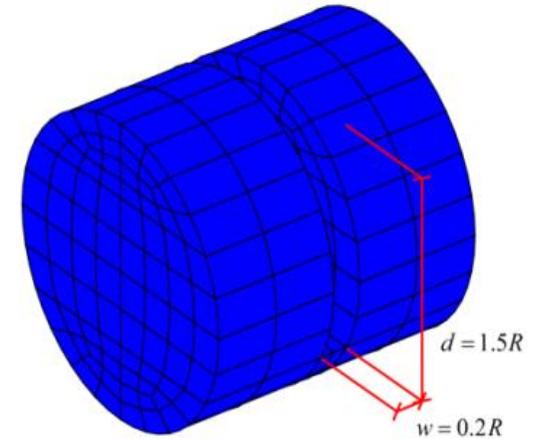
$d=0; w=0$



$d=0.5R; w=0.2R$

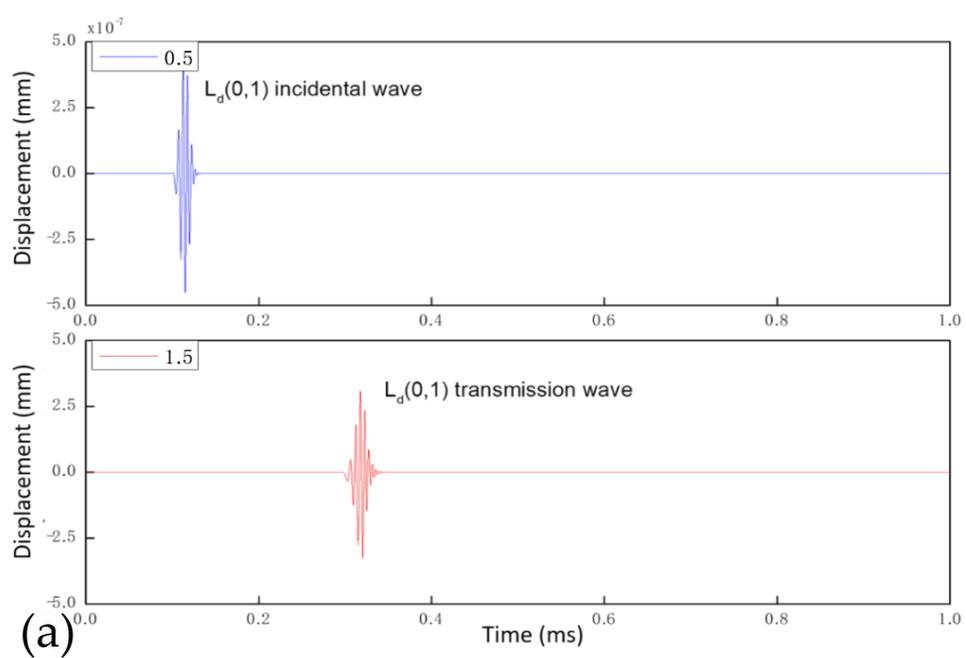


$d=1.0R; w=0.2R$

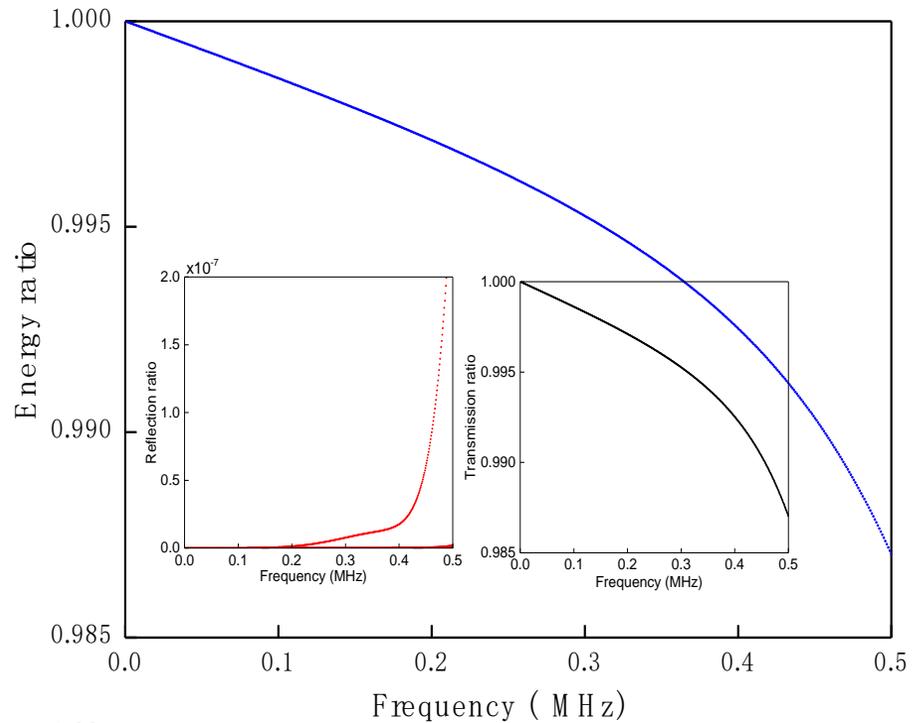


$d=1.5R; w=0.2R$

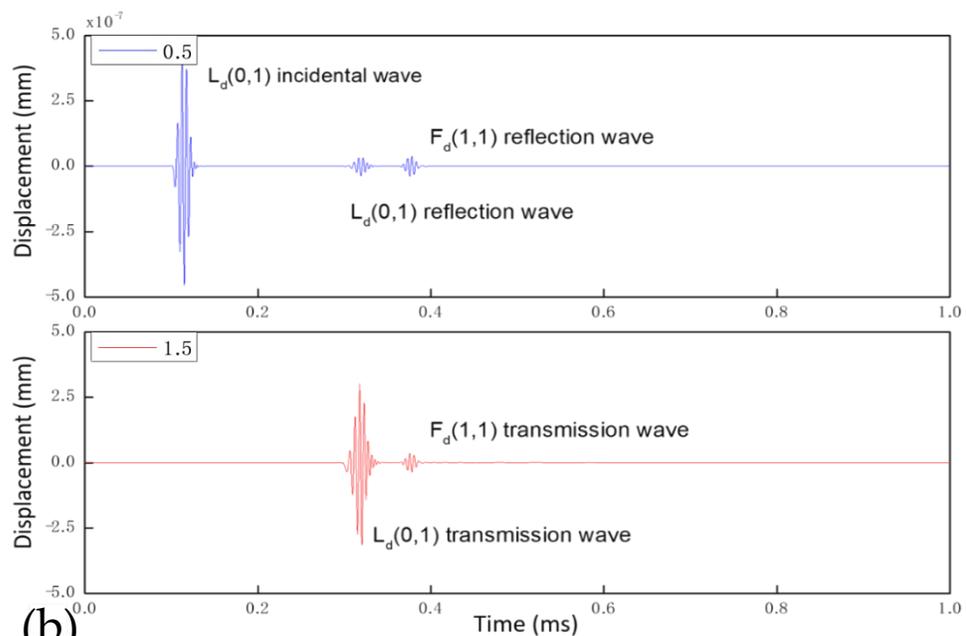
- Axial displacement response at 0.5m and 1m representing incident reflected and transmitted wave
- Energy ratio plot with power reflection and transmission coefficient



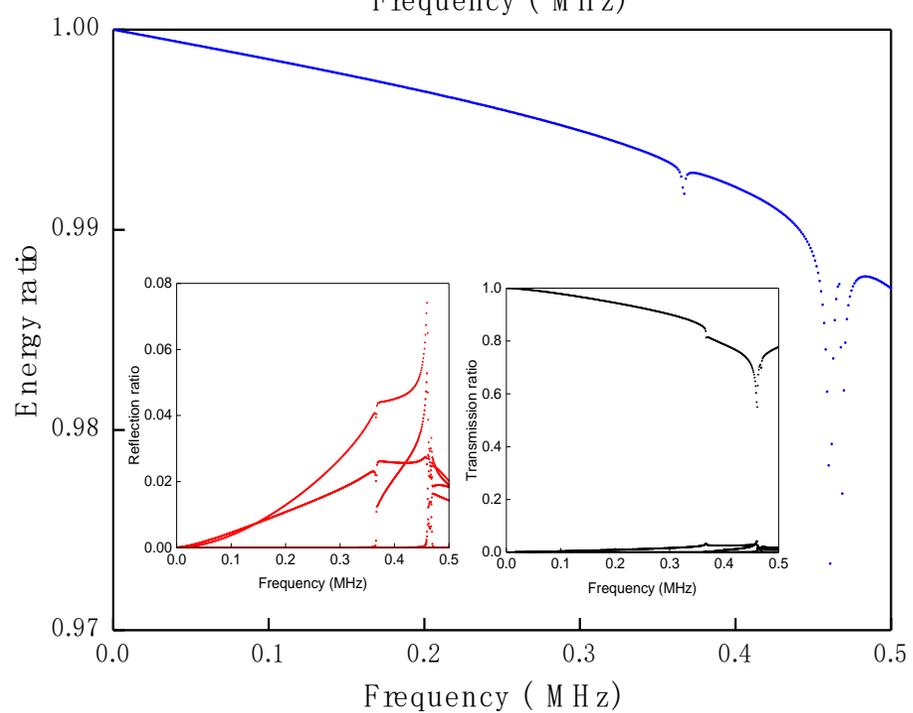
(a)



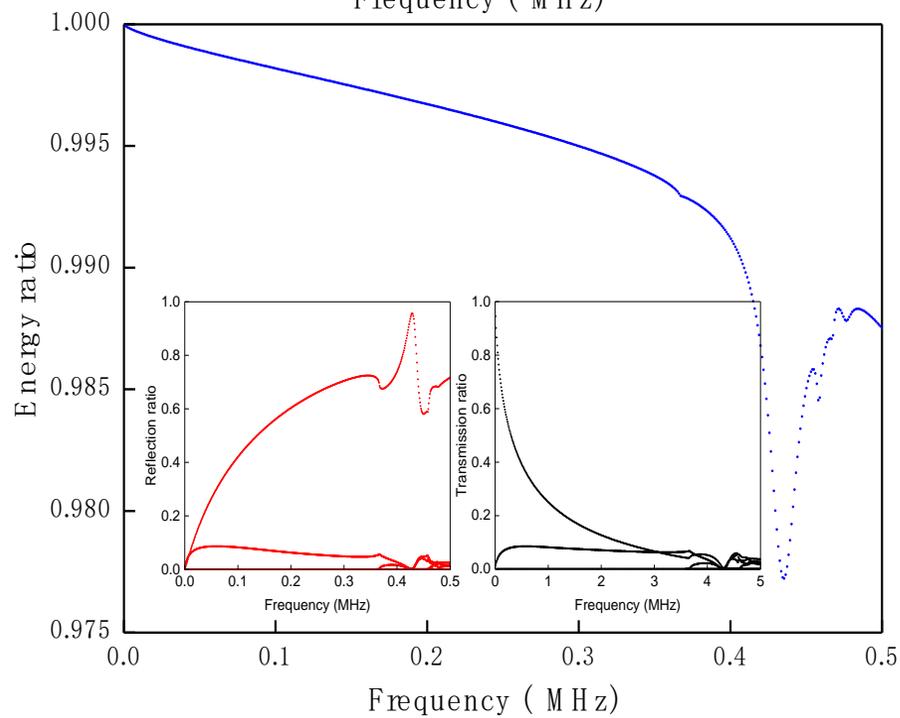
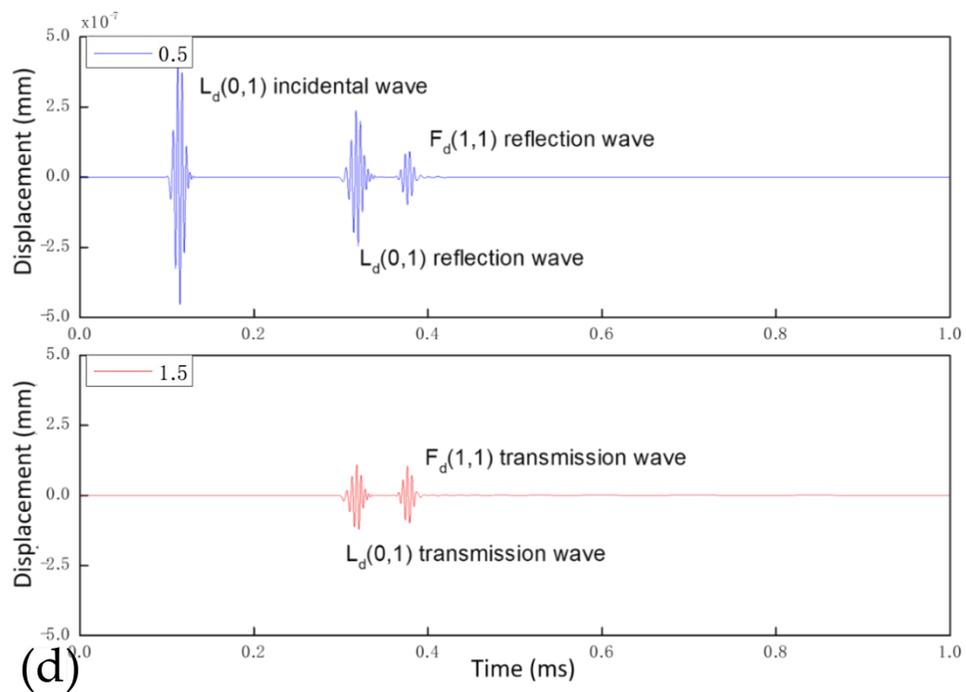
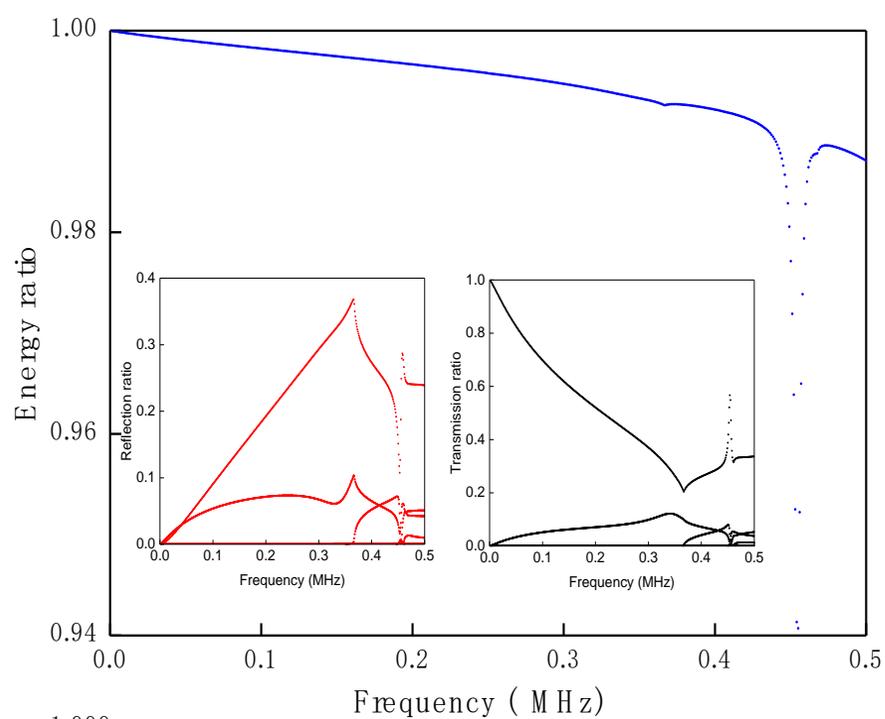
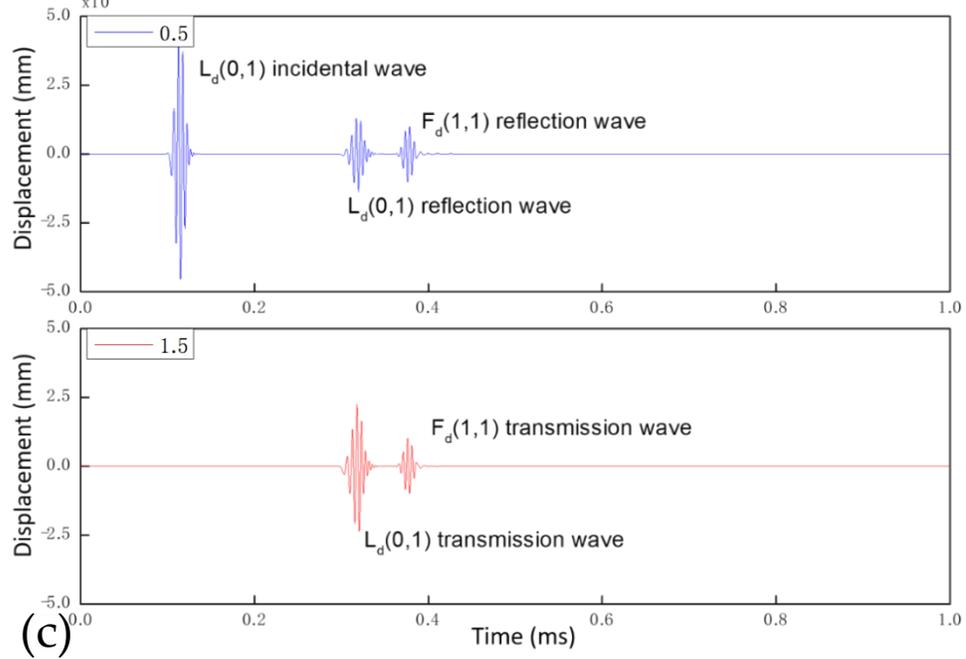
(a) for pitting model
with, $d=0; w=0$



(b)

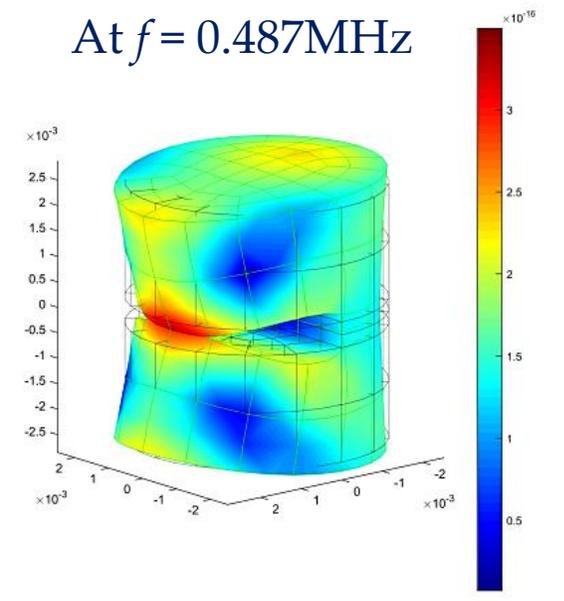
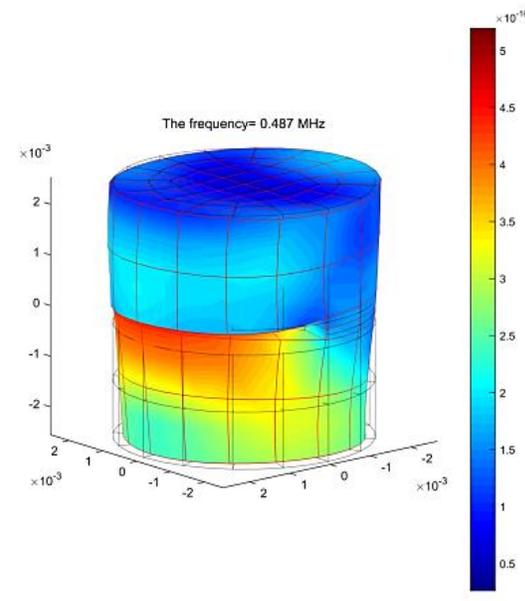
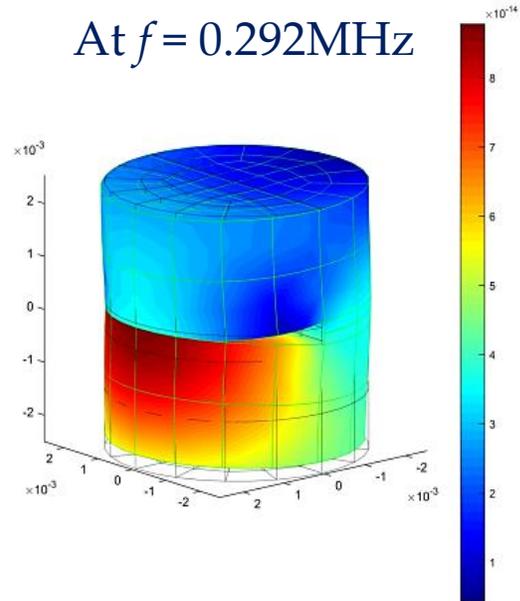
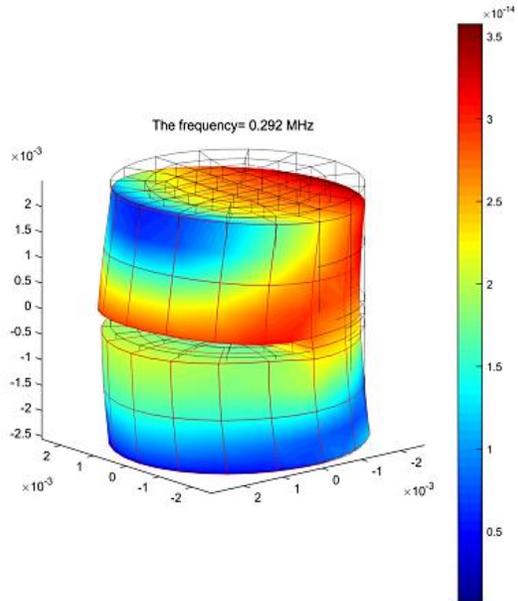
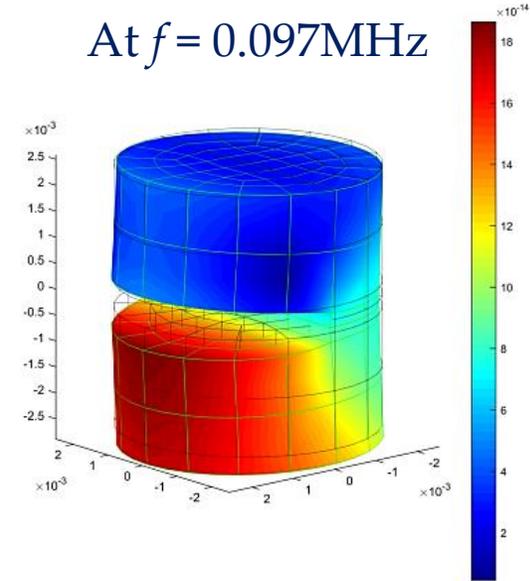
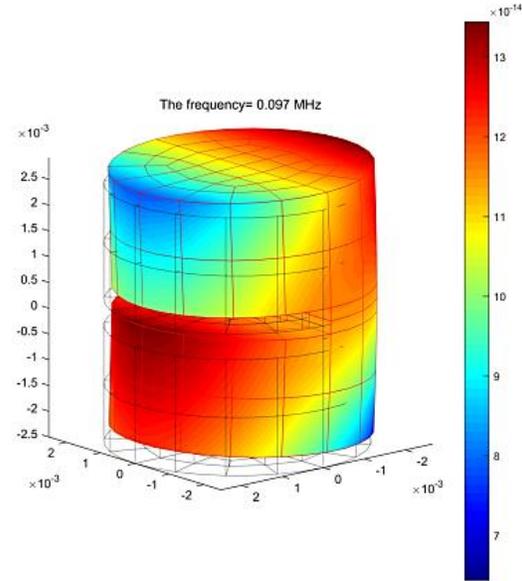


(b) $d=0.5R; w=0.2R$



3D FE region displacement response distribution for pitting corrosion model

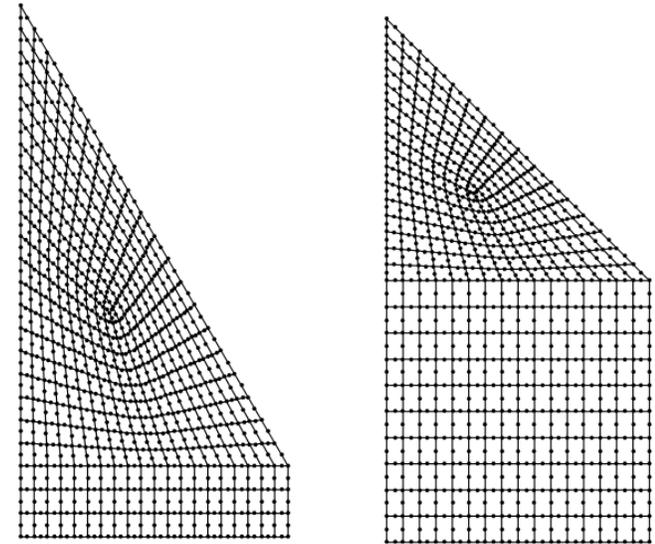
Model: $d=1.0R$; $w=0.2R$



Analysis of wave reflection

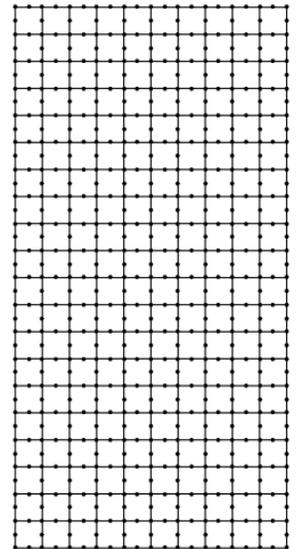
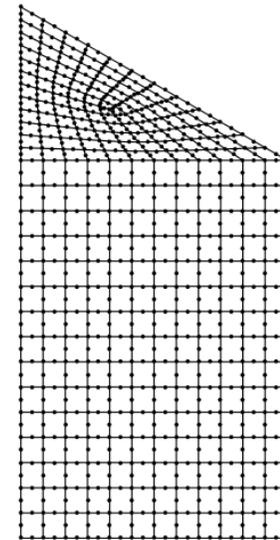
- There are two primary forms of steel wire breakage, namely, (a) due to fatigue fracture, where the broken wire is usually flat; (b) due to corrosion, the cross-section of the wire is gradually reduced.
- If the section is axisymmetric, 3D units can effectively transform the problem to 2D, reducing the calculation cost and improving efficiency and accuracy.
- Therefore, the broken wire sections are all simplified by the axisymmetric tapered section
- The 90° taper angle is the flattened condition of the steel wire caused by fatigue fracture.

Tapered steel wire model



30°

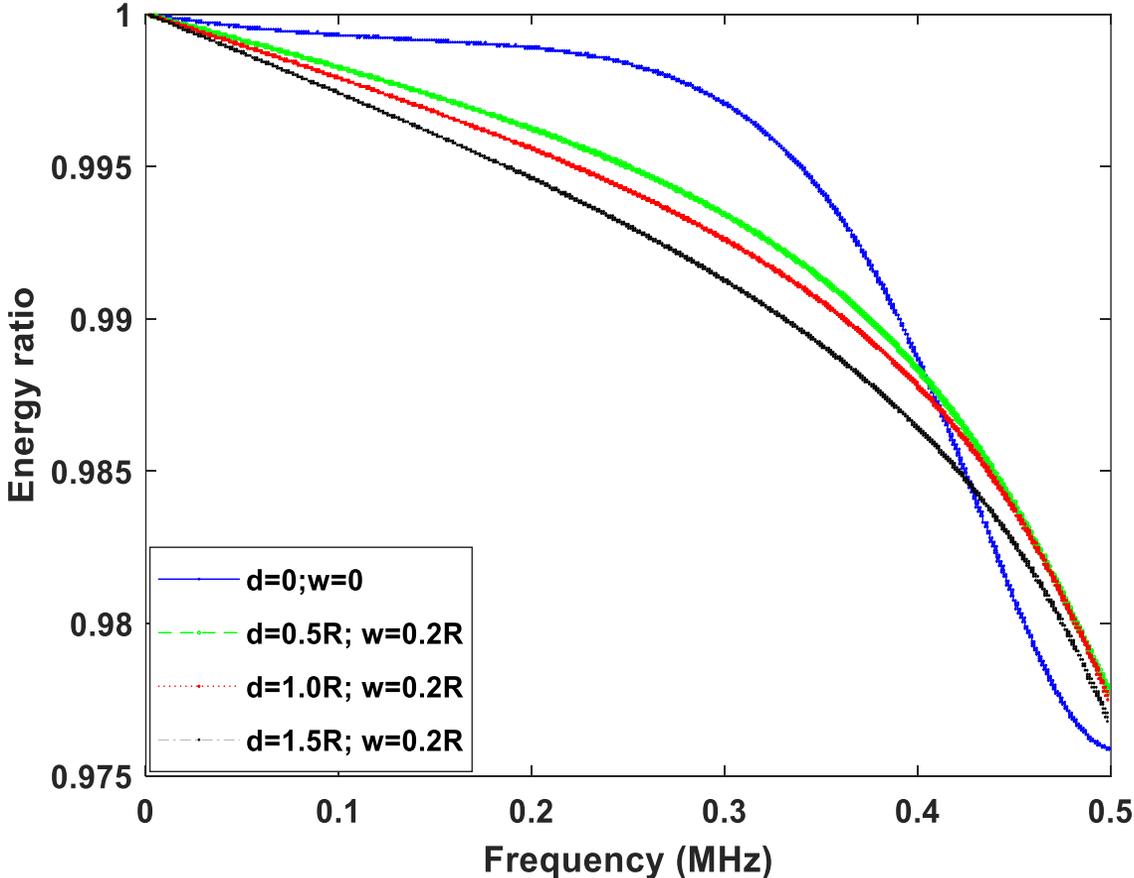
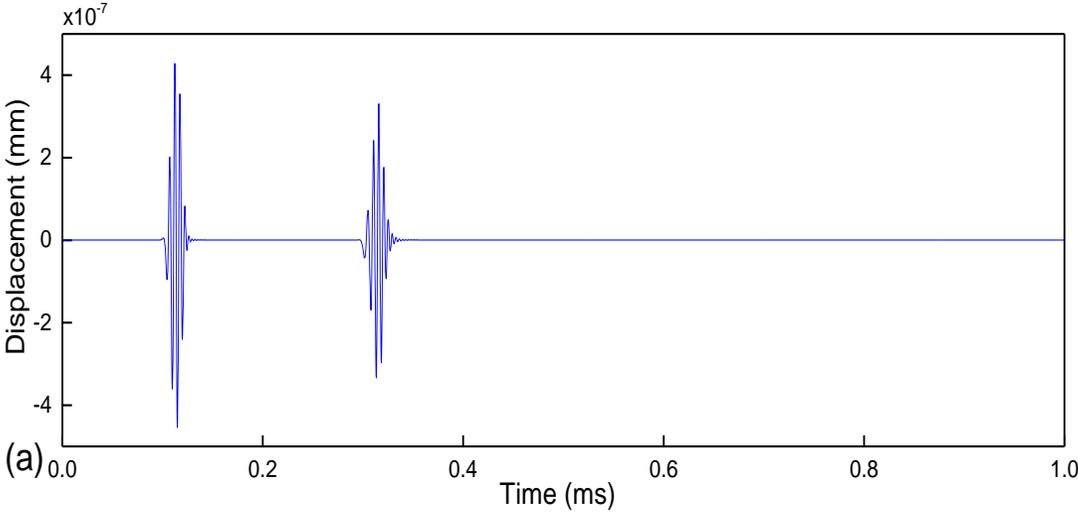
45°



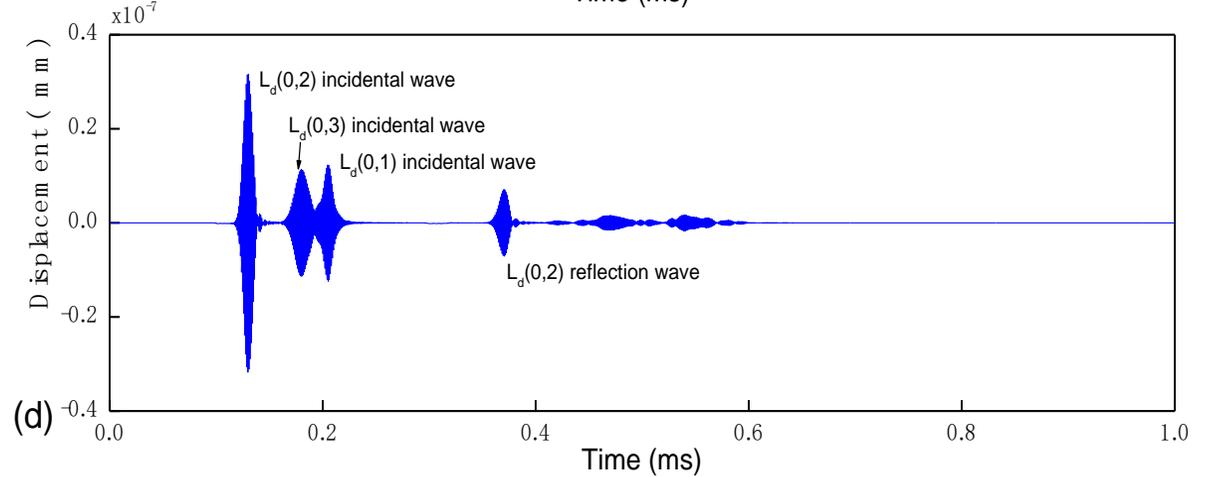
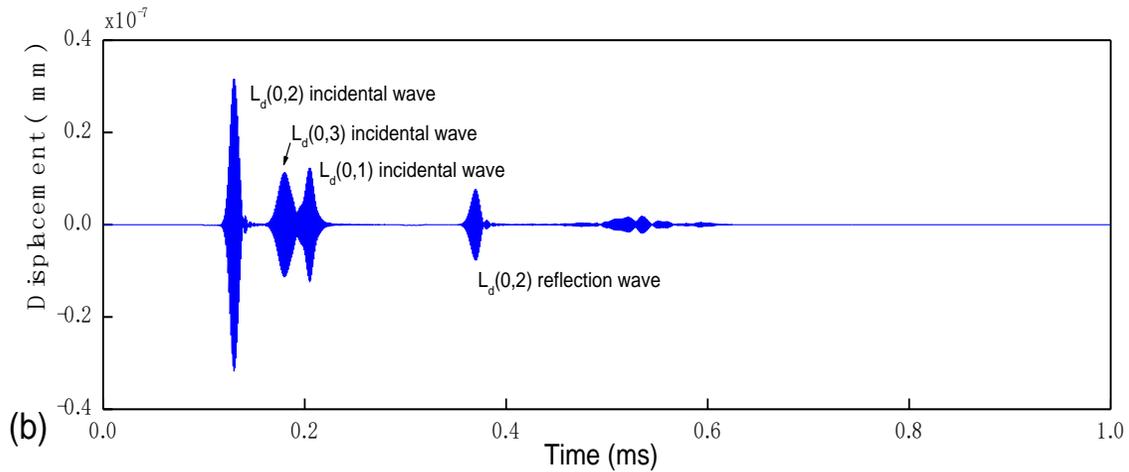
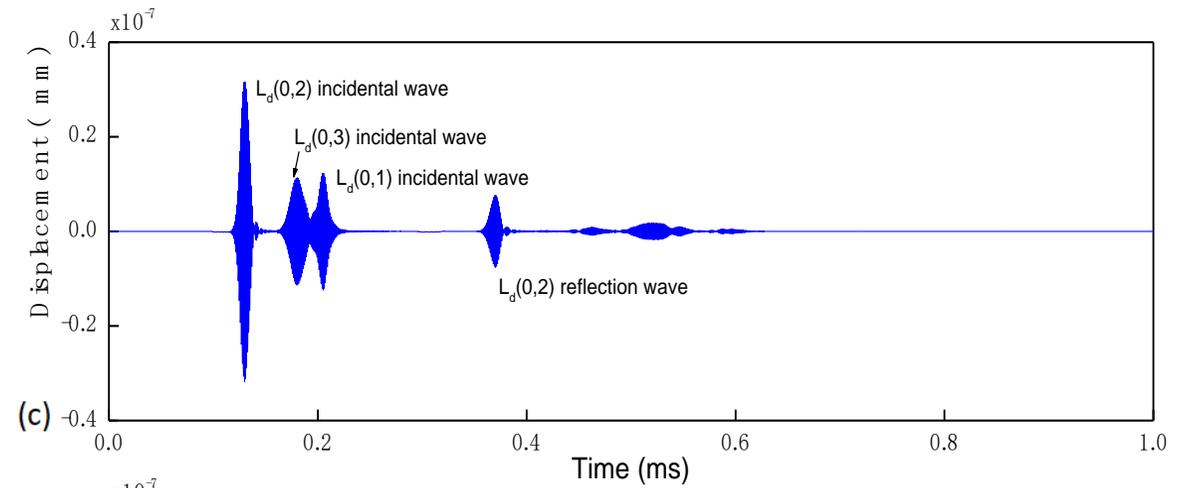
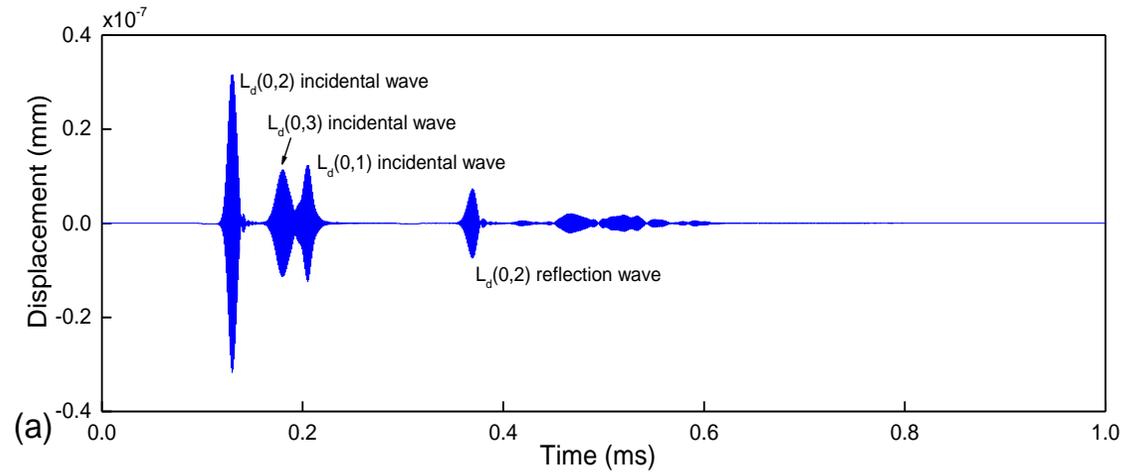
60°

90°

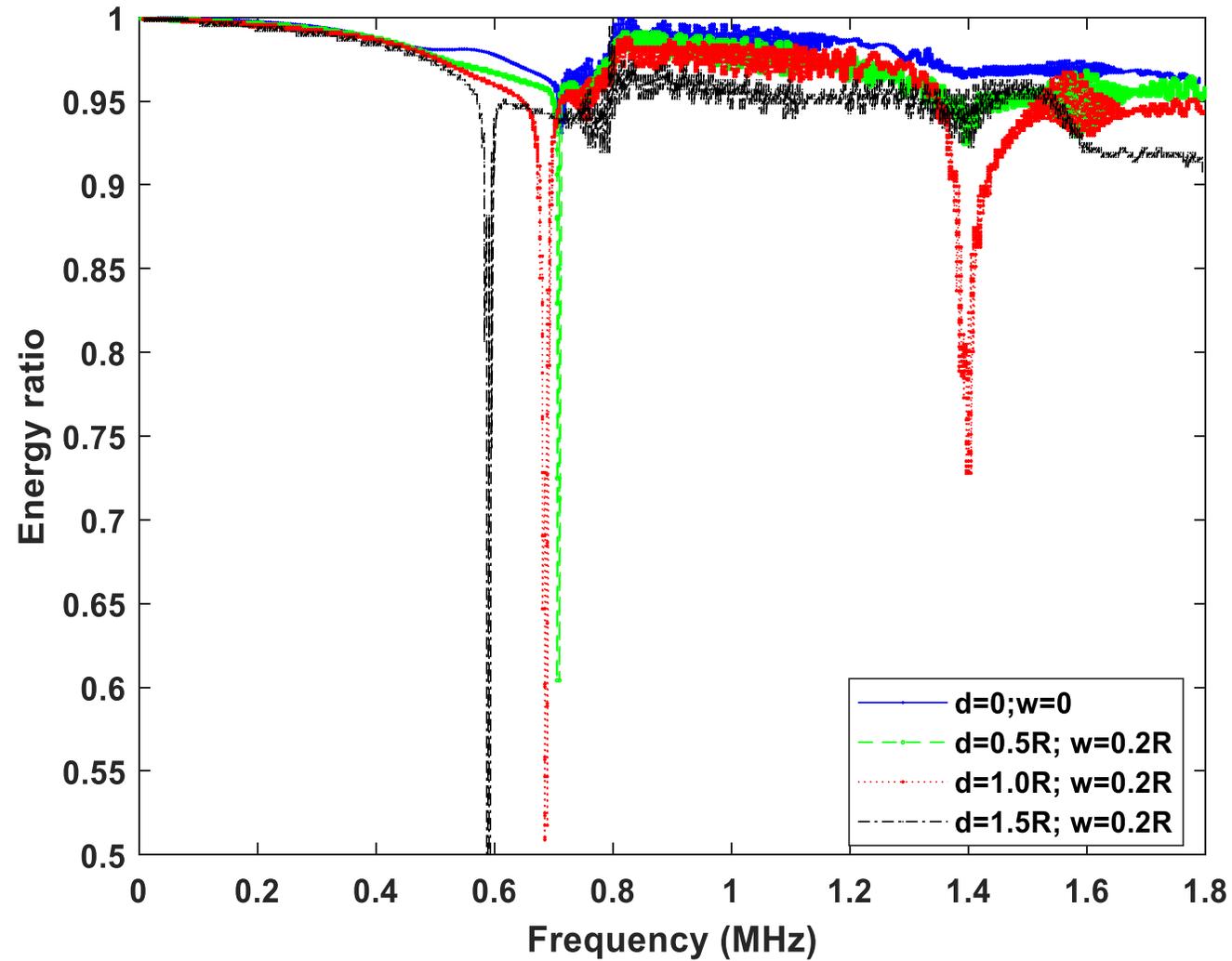
Axial displacement at 0.5m with excitation center frequency at 0.2MHz



Axial displacements at 0.5m with excitation center frequency, 1MHz for four pitting models (a-d)



Reflected energy ratio results for respective axial displacement for pitting model



Conclusions

- ✓ The **scattering response calculation** relies on the **hybrid FE-SAFE method**, and frequency domain analysis is used.
- ✓ The basic idea is to express the frequency response of the cross-section at the two ends of the **3D finite element** part as a **modal superposition** calculated by the semi-analytical method.
- ✓ It can be observed from the numerical investigations on **pitting corrosion** and free end reflection that, with considering the **material damping**, the **non-homogeneous** part will lead to the **transition between the propagation modes** and cause additional **energy dissipation**.
- ✓ For the research of **wave reflection and scattering** based on the **hybrid element method**, the algorithm using internal DOF condensation and modal acceleration method can **effectively improve the calculation efficiency**. It is suitable for models with a large number of DOF in the 3D-FE area.

Thank you for your kind attention