

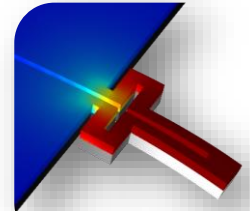
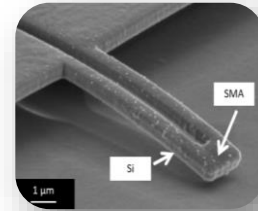
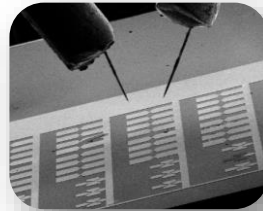
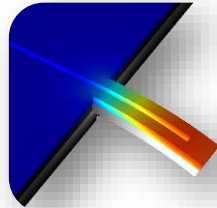
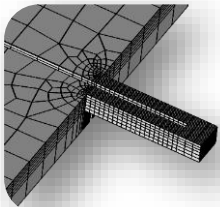


Temperature Homogenization of Co-Integrated Shape Memory – Silicon Bimorph Actuators

Gowtham Arivanandhan ¹, Zixiong Li ¹, Sabrina Curtis ², Prasanth Velvaluri ², Eckhard Quandt ², Manfred Kohl ¹

¹ Institute of Microstructure Technology, Karlsruhe Institute of Technology (KIT)

² Institute for Material Science, University of Kiel



1st International Electronic Conference on Actuator Technology: Materials, Devices and Applications (IeCAT 2020)

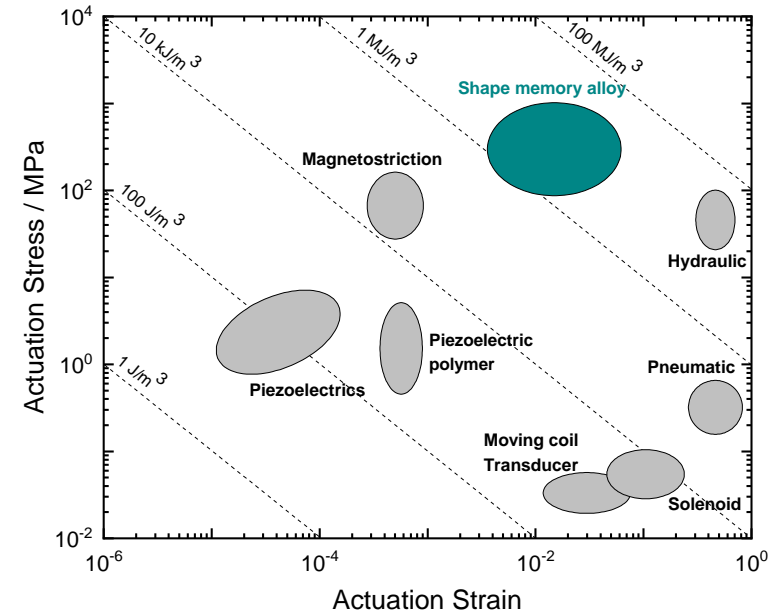
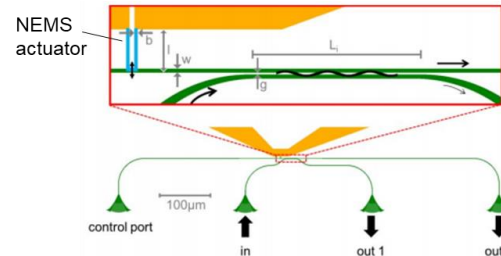
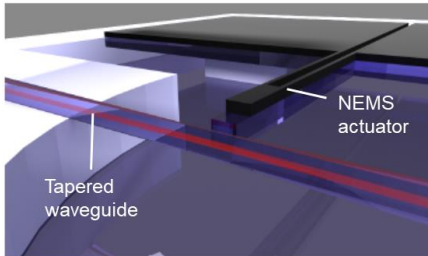
Session: Cooperative Micro-Actuator Systems
November 23rd – 27th 2020



Motivation

- Shape memory alloy
 - Beneficial downscaling (footprint of $1 \times 1 \mu\text{m}^2$)
 - Strong mechanical effects and high work density
 - Compatibility with semiconductor technology

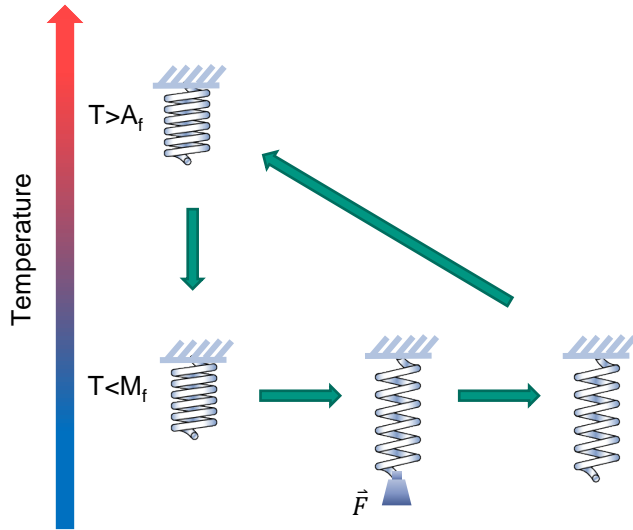
- Applications
 - Co-integration with Si mechanical structures
 - Optical switching and tuning
 - Cooperative actuators systems



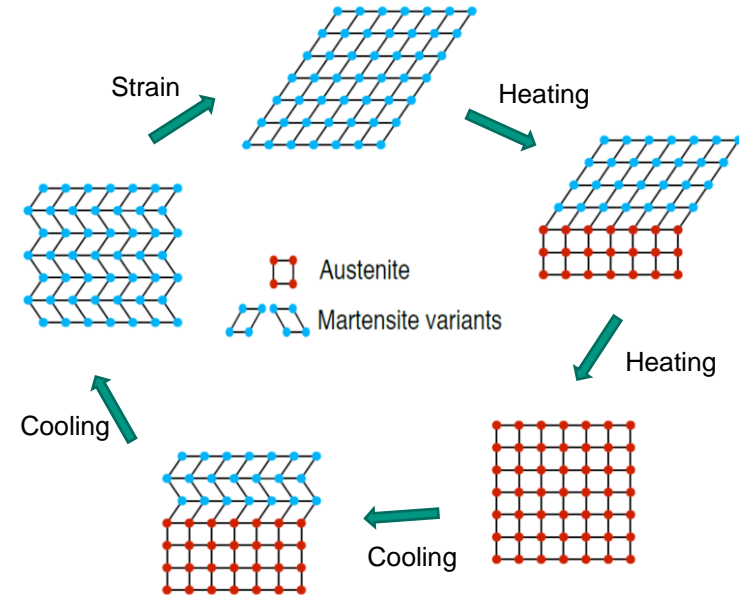
Work density for different actuation principle [1]

Background

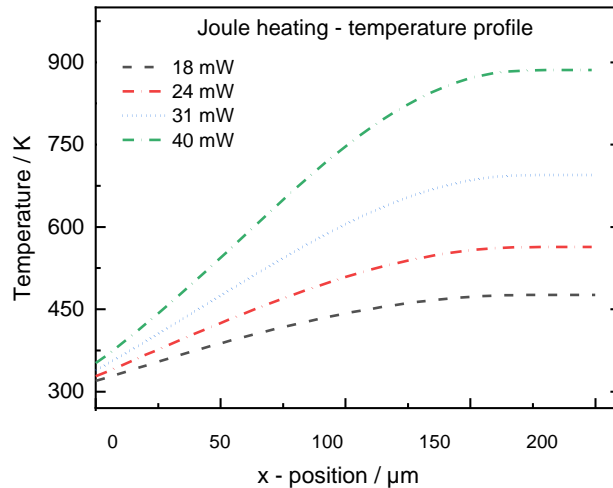
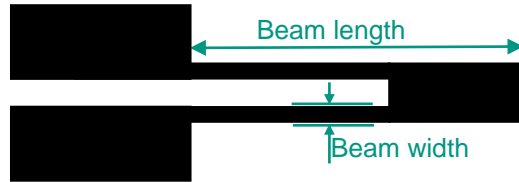
■ Shape memory effect - Overview



■ Phase transformation



Challenge: Temperature profile



- SMA/Si bimorph cantilever
 - 20 μm / 200 μm of beam width/length
 - SMA/Si each of 2 μm thickness

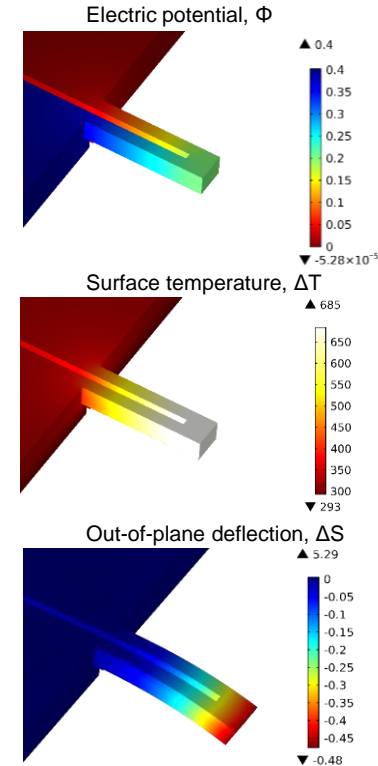
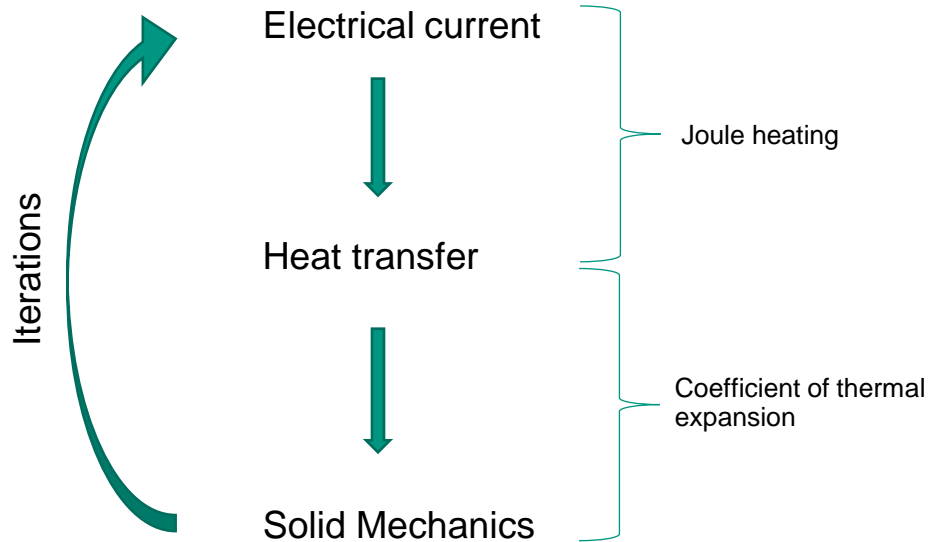
- Simulation of T-profile – thermal conductivity of materials [3]

$$\kappa_{SMA}(T) = L_0 \cdot \sigma_{SMA}(T) \cdot T$$

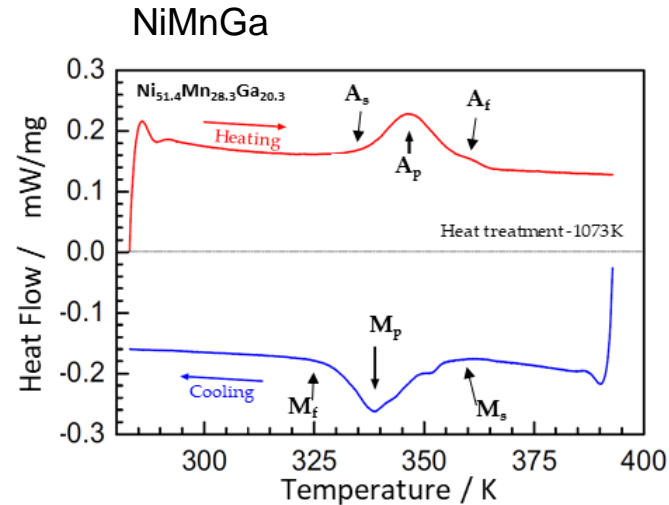
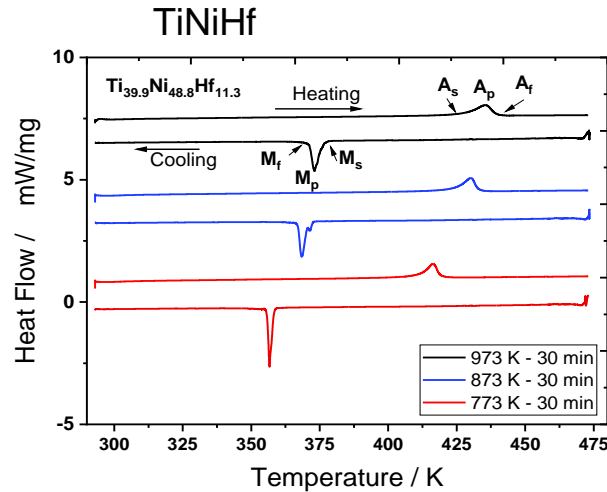
$$\kappa_{Si}(T) = \frac{5.0105 \times 10^4 \frac{W}{m}}{T} - 19.24 \frac{W}{mK}$$

- Large temperature gradients along the cantilevers
- Major effect on downscaling

Coupled Multiphysics simulation



SMA – DSC measurement



Material	Annealing Information	Af (K)	As (K)	Ms (K)	Mf (K)
TiNiHf	773 K – 30 min	419.0	412.1	357.9	356.1
	873 K – 30 min	432.9	425.1	370.7	367.1
	973 K – 30 min	439.7	428.9	376.0	371.2
NiMnGa	1073 K – 600 min	355	337	360	326

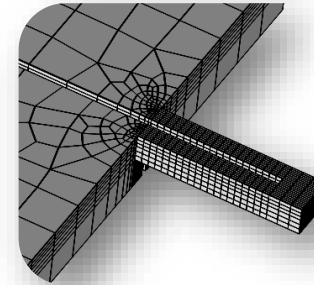
Modelling and material properties

Tanaka-type model

$$\sigma_{SMA}(T) = (1 - \xi_M(T)) \cdot \sigma_A + \xi_M(T) \cdot \sigma_M$$

$$\alpha_{SMA}(T) = (1 - \xi_M(T)) \cdot \alpha_A + \xi_M(T) \cdot \alpha_M$$

ξ_M - martensite volume fraction ($0 < \xi_M < 1$)

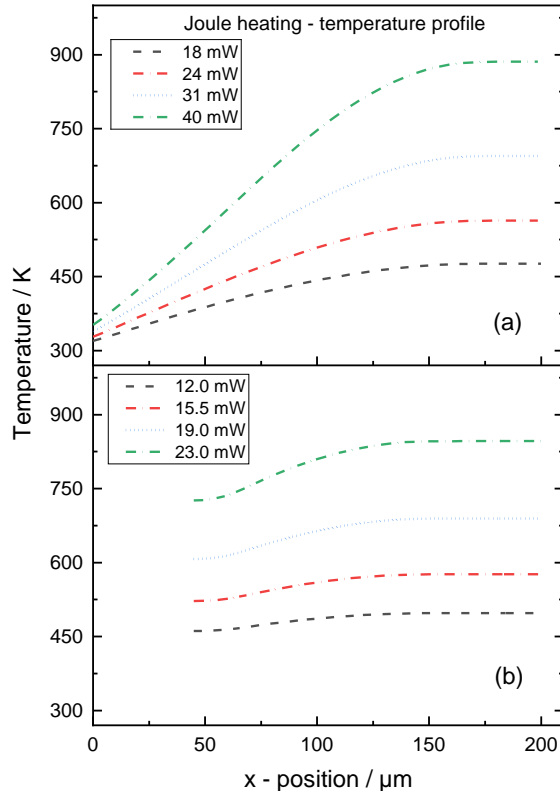


Meshing – double beam cantilever

Material properties of SMA and Si

	Si	NiMnGa	NiTi(Hf)
Electrical conductivity β_{SMA} , S/m	10	$\beta_{NiMnGa}(T)$	$\beta_{NiTi}(T)$
Thermal expansion coefficient α , 1/K	$\alpha_{Si}(T)$	$\alpha_A = 23 \times 10^{-6}$ $\alpha_M = 33 \times 10^{-6}$	$\alpha_A = 11 \times 10^{-6}$ $\alpha_M = 6.6 \times 10^{-6}$
Young's modulus E, GPa	169	E = 100	E = 87
Poisson's ratio ν	0.22	0.33	0.39

Challenge: Temperature profile

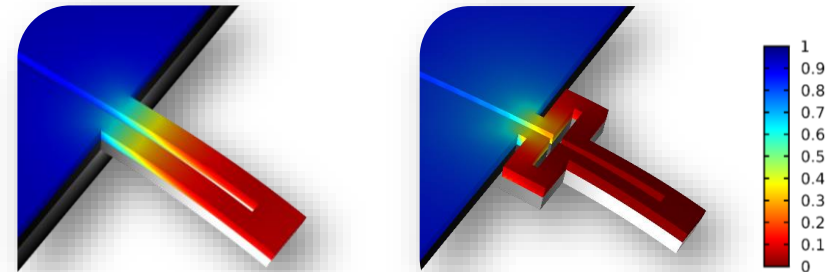
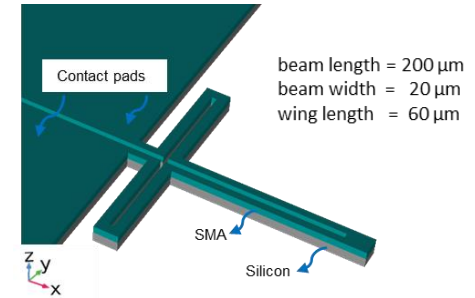


Design challenges

- Homogeneous T-profile
- Deflection should not be affected
- Power consumption

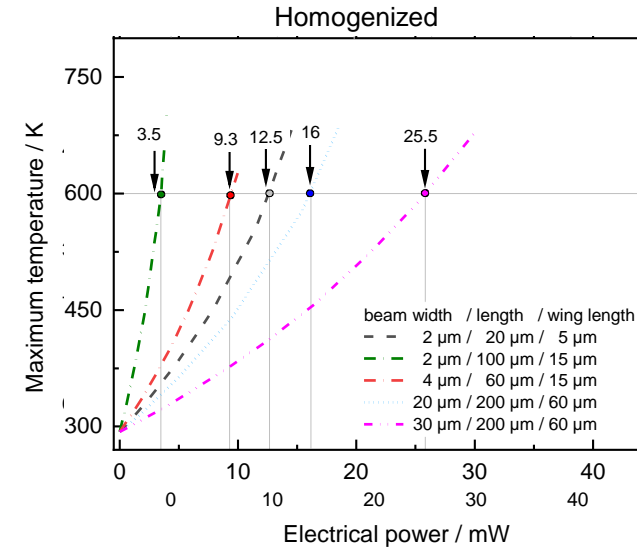
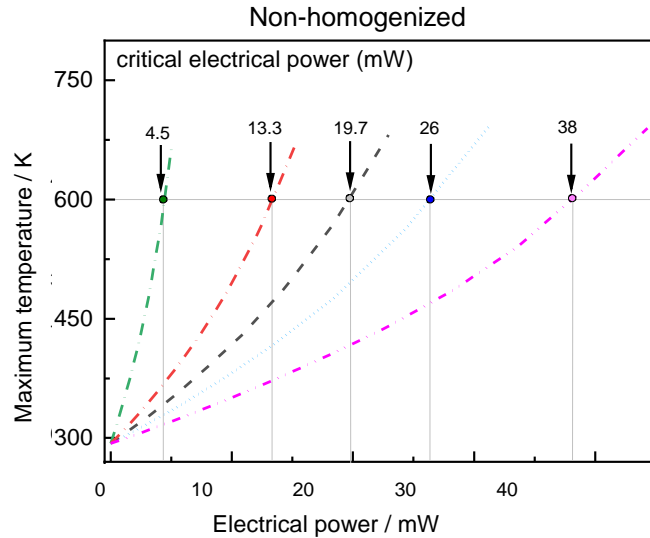
Solution: Wing like folded structures

- Homogeneous T-profile
- Uniform phase transformation



Phase fraction of Martensite

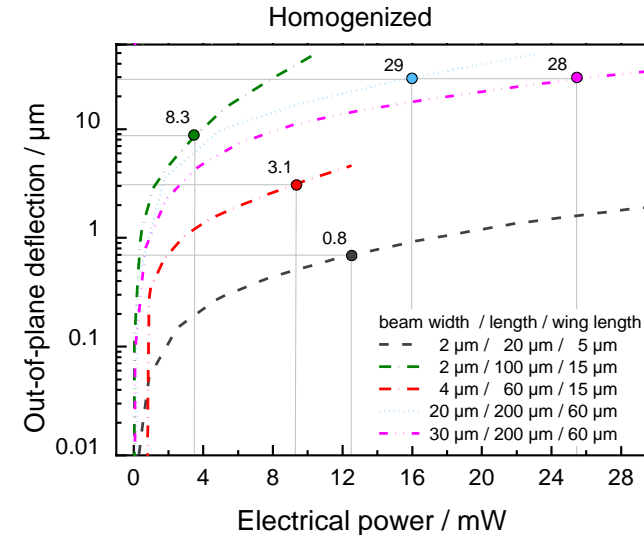
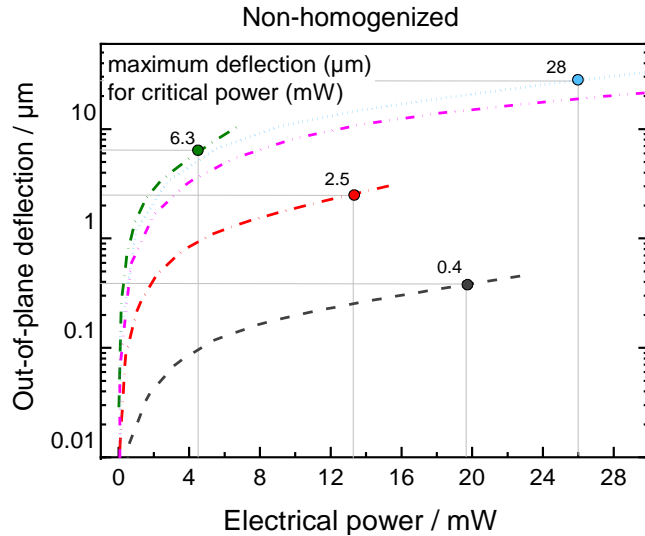
Critical Electrical Power



- Reference temperature of 600 K (operational limit of the device)
- Beam width \uparrow - needs \uparrow electrical power (#4 and #5)
- Beam length \uparrow - needs \downarrow electrical power (#1 and #2)

- With folded beam structure, less power is required to achieve maximum temperatures
- Nearly 35 % reduction in power consumption

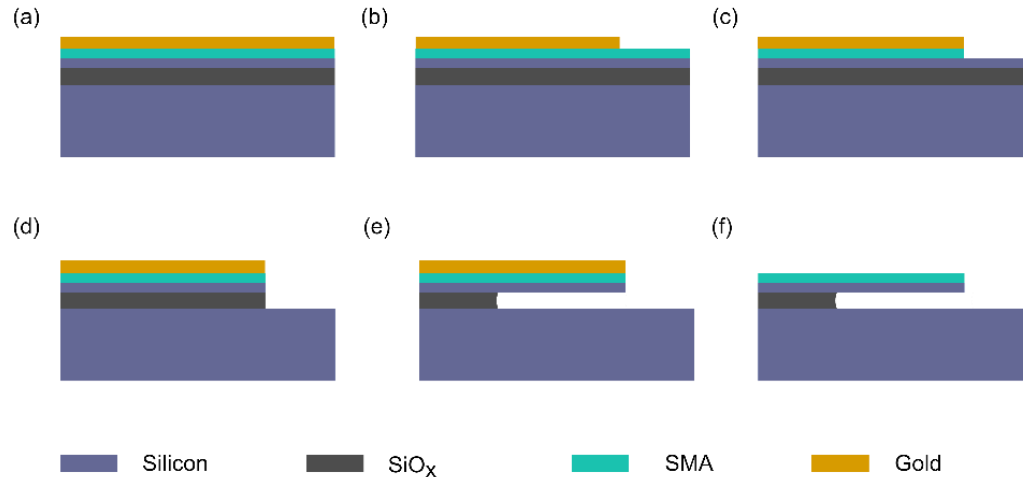
Maximum Displacement



- Maximum displacement for the critical power (at the beam tip)
- Beam width – no significant change
- Beam length \uparrow – deflection \uparrow

- Folded beam structure achieves larger deflection at lower power in all variants
- Deflection improved by factor of 2 with 2 μm /20 μm of width/length

Fabrication Process

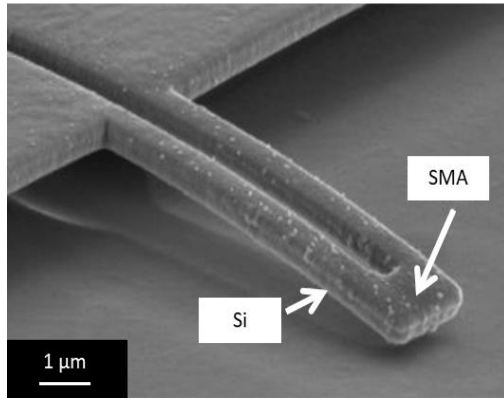


- (a) SOI wafer with SMA and Au layer
- (b) Lithography of beam structure (EBL* for nanostructures)
- (c) Wet-etching of SMA
- (d) RIE* process of Si using HBr
- (e) Isotropic HF etching of SiO₂
- (f) Free-hanging bimorph structure

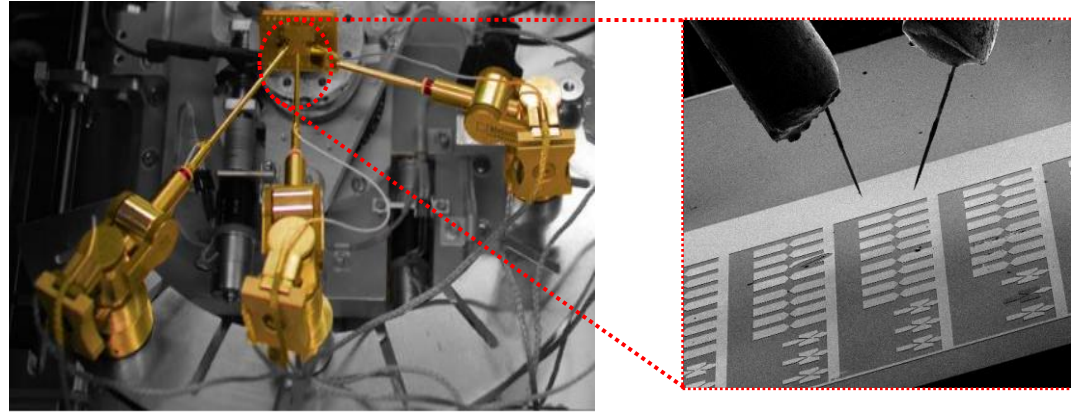
*EBL – Electron Beam Lithography
RIE – Reactive Ion Etching

Characterization

In-Situ Mechanical Characterization



SEM image of freestanding SMA-Si bimorph actuator



Nanomanipulators

Summary



- Temperature homogenization – phase transformation ↑
- Reduction of power consumption by nearly 35 %
- For beam width/length of 2/20 μm variant – deflection ↑ by factor of 2

References



- [1] F. Lambrecht, I. Aseginolaza, V. Chernenko, and M. Kohl. (2016). Integrated SMA-based NEMS actuator for optical switching. IEEE 29th International Conference on Micro Electro Mechanical Systems (MEMS). pp. 79–82; doi: 10.1109/MEMSYS.2016.7421562.
- [2] Lambrecht, Franziska Jasmin. Development of Shape Memory Alloy - Si Bimorph Nanoactuators. Karlsruher Institut für Technologie (KIT)
- [3] R. Fechner, C. Chlub, E. Quandt, and M. Kohl. (2018) .A Shape Memory Alloy 1x2 Optical Waveguide Switch. IEEE 18th International Conference on Nanotechnology (IEEE-NANO). pp. 1–3; doi: 10.1109/NANO.2018.8626320.
- [4]. M. Kohl, M. Schmitt, A. Backen, L. Schultz, B. Krevet, and S. Fähler. (2014). Ni-Mn-Ga shape memory nanoactuation. Applied Physics Letters, vol. 104, no. 4, p. 043111; doi: 10.1063/1.4863667.

Thank you for your attention!

SPP 2206 Cooperative Multistage
Multistable Microactuators Systems



Do you have any questions or feedback?

Please contact me:

Gowtham.Arivanandhan@kit.edu

Funded by

DFG Deutsche
Forschungsgemeinschaft
German Research Foundation