

1 *Conference Proceedings Paper*

2 **The Influence of Aquifer Parameters on the Design** 3 **of Extraction and Recharge Wells for the Heat Pump** 4 **Systems**

5 **Stjepan Strelec**¹, **Filip Dodigovic**^{1*}, **Kristijan Grabar**² and **Barica Marincic-Kovacev**¹

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8 ¹ Faculty of Geotechnical Engineering University of Zagreb; ured.dekana@gfv.unizg.hr

9 ² SPP d.o.o.; spp@spp.hr

10 * Correspondence: filip.dodigovic@gmail.com; Tel.: +385-98-161-85-93

11 **Abstract:** Groundwater can be considered a non-polluting, renewable energy source. It can be used
12 as a fluid in industrial, commercial, and residential building heating and air-conditioning systems.
13 Usually the water table is deep enough, so atmospheric conditions have a negligible influence on
14 water temperature. Consequently, annual temperature variation is minor, and groundwater can
15 therefore also be considered a reliable energy source. This paper presents some aspects of the
16 groundwater heat pump (GWHP) wells design and addresses problems that can occur during their
17 exploitation. The heat pump system consists of two types of wells: extraction wells and recharge
18 wells. This paper shows that the distance between the two is a crucial parameter that affects the
19 efficiency of the whole system. An example of wells design for a production hall groundwater heat
20 pump is given. The wells are constructed is in the northern part of Croatia. Geological and
21 hydrogeological conditions at the site, regarding water temperature and soil hydraulic conductivity,
22 are highly favorable. Due to insufficient distance between wells thermal breakthrough occurred, i.e.
23 water temperature in the extraction well rose, which resulted in a lower efficiency of the GWHP
24 system.

25 **Keywords:** well design; heat pump; aquifer; groundwater; hydraulic conductivity; groundwater
26 heat pump; aquifer; thermal breakthrough

28 **1. Introduction**

29 The direct use of groundwater for heating and cooling buildings has been gaining more attention
30 recently. The reason for this is groundwater's large potential which is derived from multiple factors,
31 the most prominent of which is being environmentally friendly. Geothermal energy is a renewable
32 and sustainable energy source, 50.000 time greater than all oil and gas resources in the world [1]. As
33 a clean, reliable and abundant energy source, it seems to be an obvious solution to the problem of
34 global warming, pollution and the rising prices of fossil energy sources [2].

35 In nature, heat can be transferred from regions of higher to regions of lower temperature. A
36 system that transfers energy in the opposite direction is called a heat pump [3]. The Groundwater
37 heat pump (GWHP), a type of the ground heat pump (GHP), uses thermal energy stored in an aquifer
38 for heating and air-conditioning buildings. In general, the GWHP is comprised of an aquifer thermal
39 energy storage (ATES) system, a heat pump unit and a terminal air conditioning system. The ATES
40 usually includes one of more pairs of groundwater wells as energy sources [4]. When compared to
41 closed-loop systems, the groundwater heat pump can achieve a higher heat exchange rate (HEX). The
42 reason for this is the fact that the temperature of the groundwater circulating through the heat pump

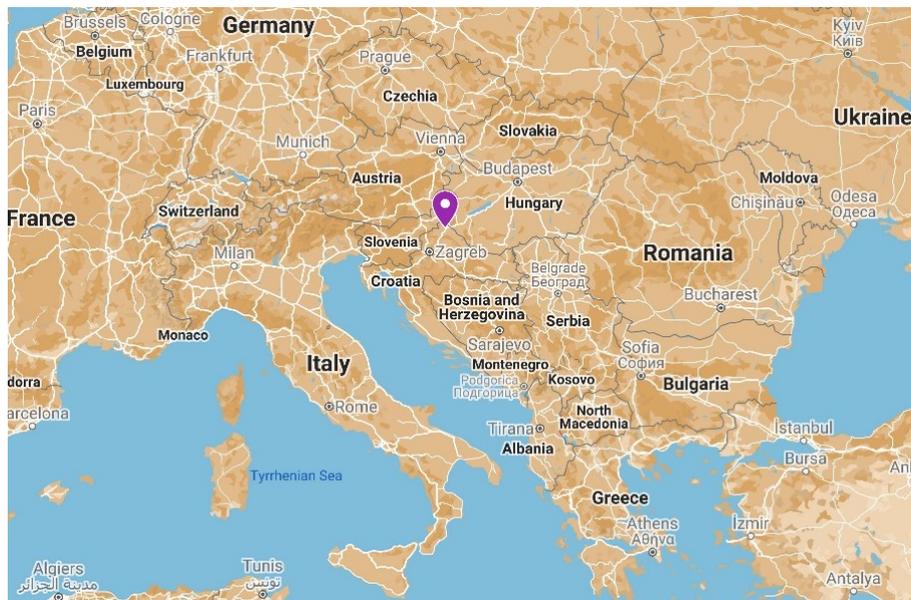
43 is closer to median groundwater temperature than in closed-loop systems [5]. Using energy stored in
 44 the ground results in 80% savings in cooling and 30% savings in heating [6]. Despite the obvious
 45 advantages, disadvantages need to be considered when designing GWHP systems, such as potential
 46 terrain settlement, clogging in the return well and groundwater contamination. Long term
 47 functionality of the system can also be affected by thermal breakthrough [7] and recharge resistance
 48 [8].

49 This paper presents an example of a GWHP system built for heating and air-conditioning a
 50 production hall with the surface area of 4700 m². During exploitation, a significant influence of the
 51 recharge well on the temperature increase in the extraction well, i.e. thermal breakthrough was
 52 detected. The temperature increase in the extraction well led to decreased efficiency of the heat pump.

53 2. Geological and Hydrogeological Characteristics of the Location

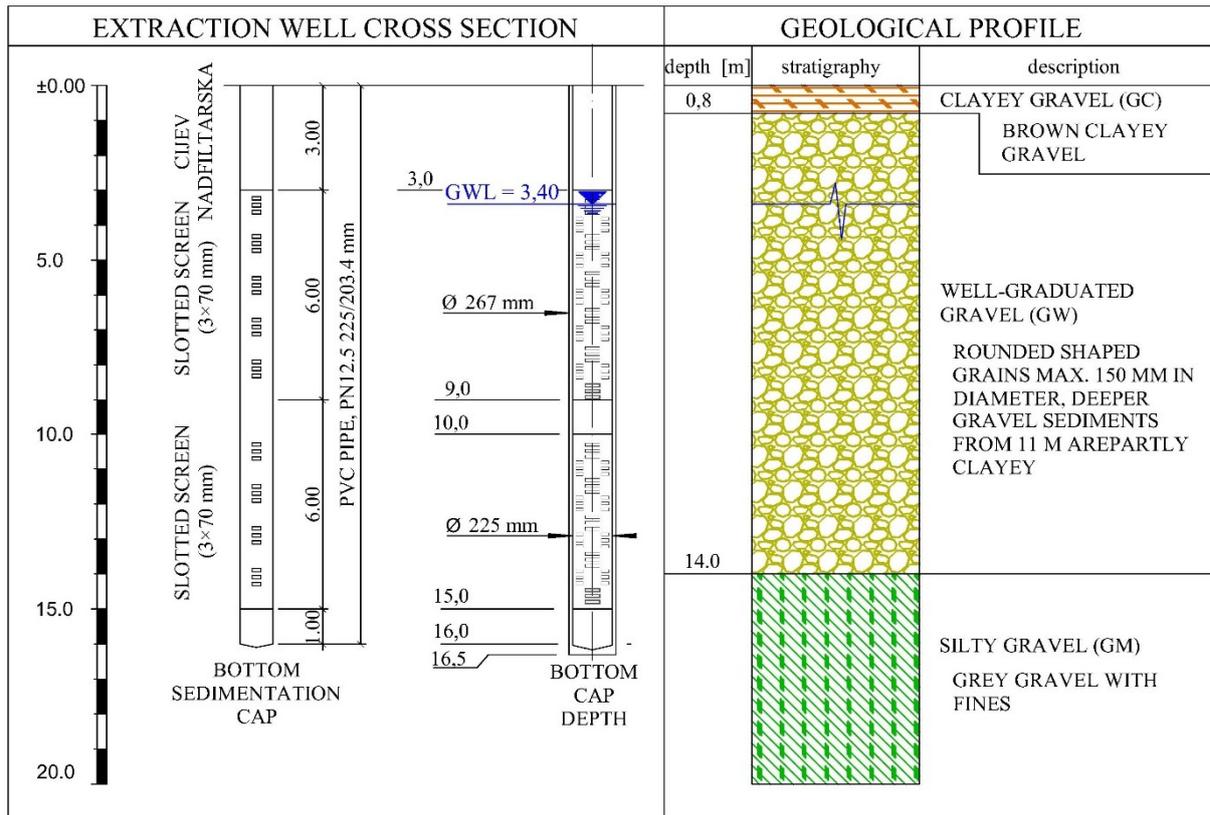
54 Designing GWHP systems requires detail knowledge of local hydrogeology, i.e. aquifer
 55 parameters. The usual aquifer parameters used in well design are porosity, hydraulic conductivity,
 56 transmissivity, storage capacity and aquifer thickness.

57 The presented hall was built in the Međimurje County in the northwest part of Croatia (Figure
 58 1). The area is almost completely surrounded by rivers: Mura in the north and east, Drava in the
 59 south, and the Šantavec creek, which forms a part of the western border with Slovenia. One of the
 60 basic geological characteristics of Međimurje is a ground surface comprised almost exclusively of
 61 sedimentary rock of Pleistocene and Holocene origin. The majority of the sediment are actually
 62 poorly graduated sand-gravels, comprised mostly of quartz conglomerates (over 90%) and sand,
 63 whose light fraction is dominated by quartz (around 50%), with muscovite (around 22%) and feldspar
 64 (around 22%) also present.



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 66 **Figure 1.** Location of the production hall.

67 The described geological structure is very favorable for the construction of GWHP systems. In
 68 order to determine the exact geological conditions of the location, investigation works were
 69 performed, comprising of test drilling and laboratory tests. The test drillings helped define the
 70 geological profile (Figure 2). The geological profile, combined with laboratory analyses, showed that
 71 geological formations with higher water permeability reach a depth of 14 m, and correspond to well-
 72 graded gravel (GW). This interval also includes thinner interlayers of silty gravel (GM). Since their
 73 influence on well efficiency is assumed to be negligible, they are not considered in further
 74 deliberation.



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Figure 2. Geological profile along with extraction well cross section.

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Based on ground granulometry, hydraulic conductivity was estimated at $k = 102 \text{ m/dan}$; its actual value is to be determined by means of a pump test. Depths exceeding 14 m included gravel with silt and clay (GM) in various ratios. Based on all the listed facts, it is concluded that ground conditions are favorable for well construction, while the geometry and other characteristics are to be adjusted to the required pump capacity, defined by the heat pump designer.

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82 3. In-situ Measurements of Aquifer Characteristics

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The important aquifer parameters used in well design are the coefficient of hydraulic conductivity, the coefficient of transmissibility and the storage coefficient.

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Soil or rock permeability is defined by the coefficient of hydraulic conductivity, which depends on multiple factors such as: the soil's granulometric composition, particle shape and texture, mineral composition, the coefficient of pores, level of saturation, the nature of fluids, temperature etc. [9]. Its value is also a function of the size and shape of pores, pore connectivity efficacy and the physical characteristics of fluids [10]. The hydrogeological parameter that also describes the aquifer is the coefficient of transmissivity (T), defined as the rate at which water can pass through the full aquifer thickness. Simply stated, it is the hydraulic conductivity multiplied by the saturated aquifer thickness [11]. Its value equals the mathematical product of hydraulic conductivity and aquifer thickness (Equation 1).

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$$T = k \cdot m [\text{m}^2/\text{day}, \text{cm}^2/\text{s}, \text{m}^2/\text{s}] \quad (1)$$

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Where: k is hydraulic conductivity coefficient, m is the thickness of aquifer

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The storage coefficient (S) or storativity is the volume of water released from storage with respect to the change in head (water level) and surface area of the aquifer. Common values for unconfined aquifers are within the 0.05 – 0.3 interval [12]. It pertains to the total thickness of the saturated part of the aquifer, and its value is the mathematical product of the specific value (S_s) and aquifer thickness (m) [10].

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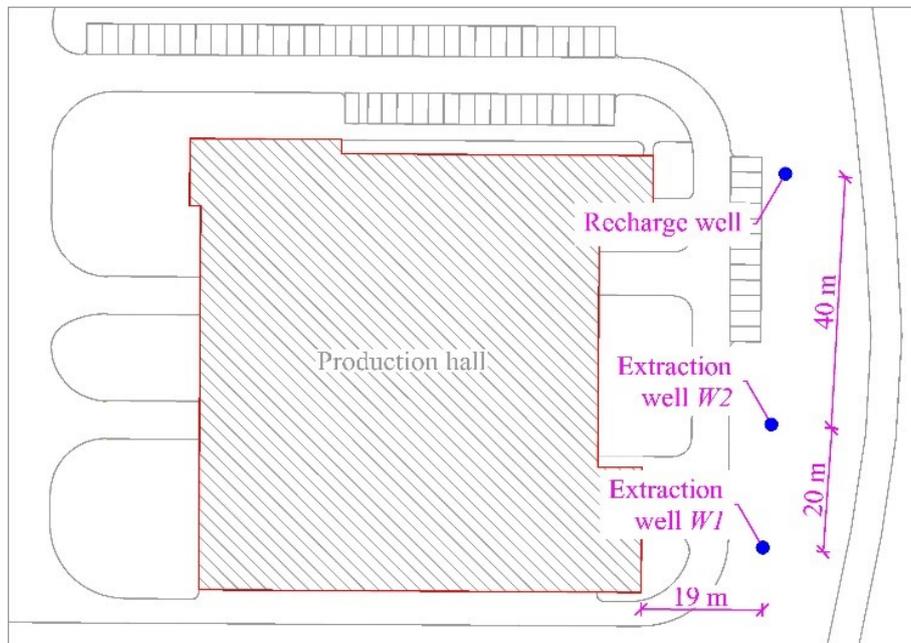
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$$S = S_s \cdot m \text{ [l]} \quad (2)$$

100 By applying the mentioned parameters, we define the distance between the wells, as well as
 101 their capacities, with the final goal of ensuring the design efficiency of the heat pump. A reliable way
 102 of determining aquifer parameters is a pumping test [13], which had two specific goals in this case:

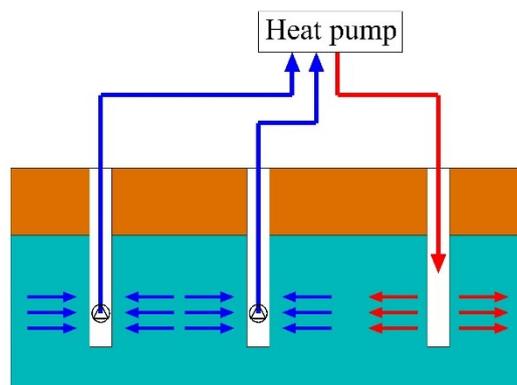
- 103 • determining aquifer parameters
 104 • measuring groundwater lowering as a consequence of pumping, in order to estimate the
 105 settlement of the surrounding terrain.



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Figure 3. Site Layout.

108 Monitoring water level lowering was done in both wells during the pumping test, as well as
 109 measurements of pumping capacity. The results of the pumping test helped define the aquifer
 110 parameters relevant for well design. The ground plan of the pumping test wells arrangement
 111 is shown in Figure 3, and a schematic showing the wells in relation to the heat pump is shown in Figure
 112 4.

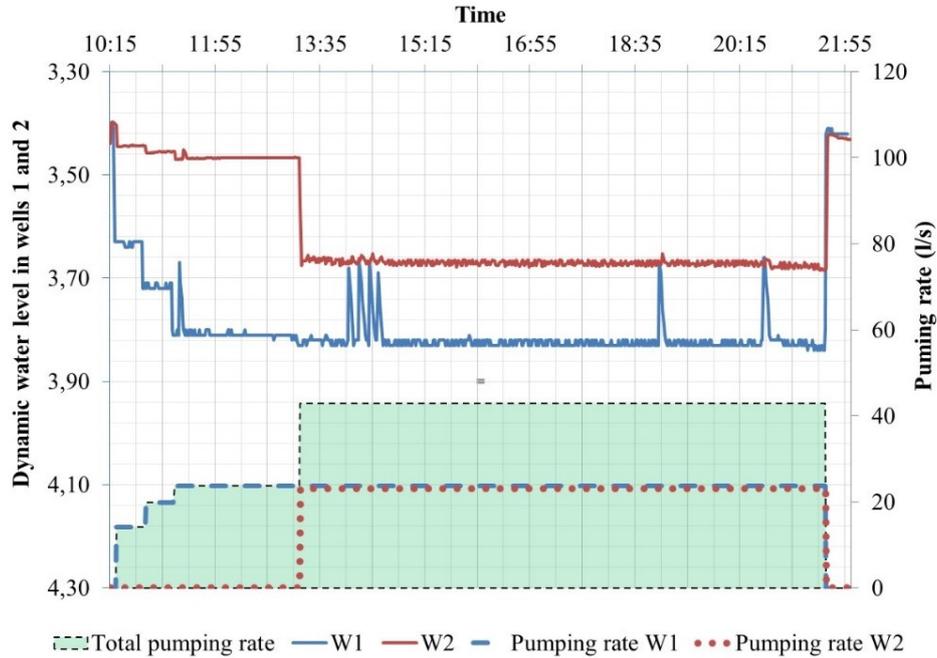


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Figure 4. Schematic view of the heat pump, two extraction wells and recharge well.

115 The total length between extraction wells W1 and W2 is 20.0 m. Before the pumping test,
 116 groundwater level was measured on 3.4 m of depth. It was done in stages with three different
 117 capacities, continually for 10 hours. Figure 4 shows the pumping test results. The maximum water
 118 level lowering was measured in pumping well W1 at the capacity of $q=24$ (l/s), and it amounted to 40

119 (cm). Well W2 showed a lowering of 30 cm at the same pumping capacity. The pumped quantities
 120 indicate favorable aquifer hydrogeological characteristics and quality well construction. During the
 121 pumping test, the lowering in the exploitation well showed minimal fluctuation in dynamic water
 122 levels, which in turn helped in quickly reaching a balance state between the pumped quantity and
 123 the inflow from the aquifer [14].



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Figure 5. Pump test results.

126 Based on the pumping test results (Figure 5), and using the *Aquifer Test Waterloo Hydrogeologic*
 127 *software*, the aquifer hydrogeological parameters were determined. The parameters were determined
 128 for two types of pumping tests: the constant test and the step test, and the results are shown in Table
 129 1.

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Table 1. Hydrogeological parameters of the aquifer.

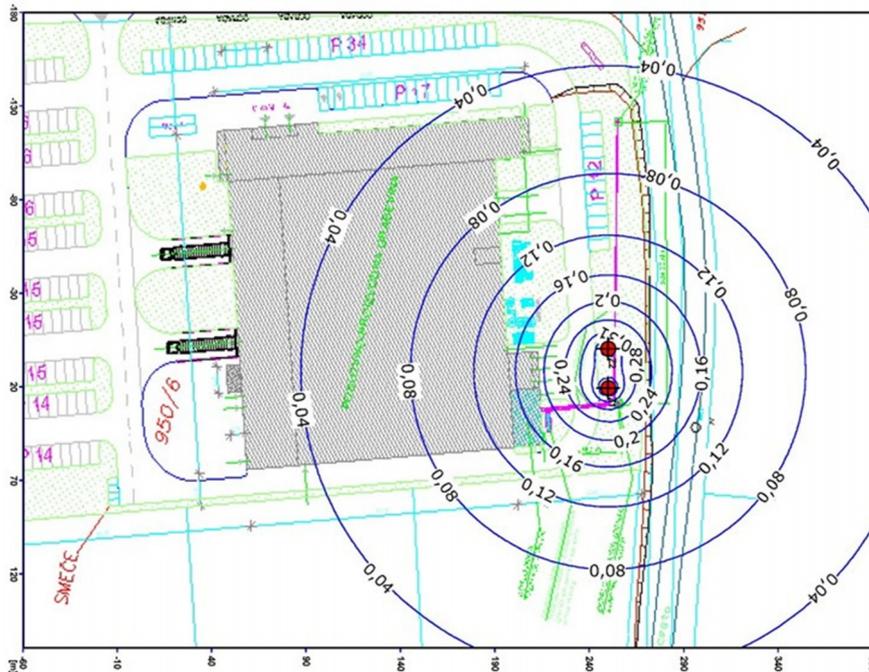
Test	Hydraulic conductivity coefficient, K [m/day]	Coefficient of transmissivity, T [m^2/day]	Storage coefficient, S
Constant test	111	3000	0.148
Step test	118	3190	0.110

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The resulting value of the hydraulic conductivity coefficient matches the values calculated from the granulometric curve (120 m/day), as well as the typical values for this sort of material. The high values of hydraulic conductivity and transmissivity ensure highly favorable conditions for pumping groundwater in the construction of GWHP systems.

Figure 6 shows the influence of pumping in wells W1 and W2 on groundwater levels. The analyses were done using the pumping test results, in the "Drawdown" software. The software solves the Theis equation [15], and provides a graph of the lowering as a function of distance or pumping time. The presented data refers to groundwater lowering caused by the maximum pumped quantity in both pumps combined, which is $q = 43$ l/s in the duration of 10 hours. The largest groundwater lowering at the construction footing is ≈ 15 cm. The groundwater lowering caused additional stress in the foundation soil as a consequence of the change in effective stress. The additional stress in this

143 specific case is $\Delta\sigma = 1.5kN/m^2$. Considering the fact that the additional stress caused by construction
 144 weight and other external factors was considerably greater, the mentioned influence can be
 145 disregarded. Taking geotechnical soil characteristics into account, we can conclude that water
 146 pumping in the described conditions causes negligible settlement of the product hall foundation.



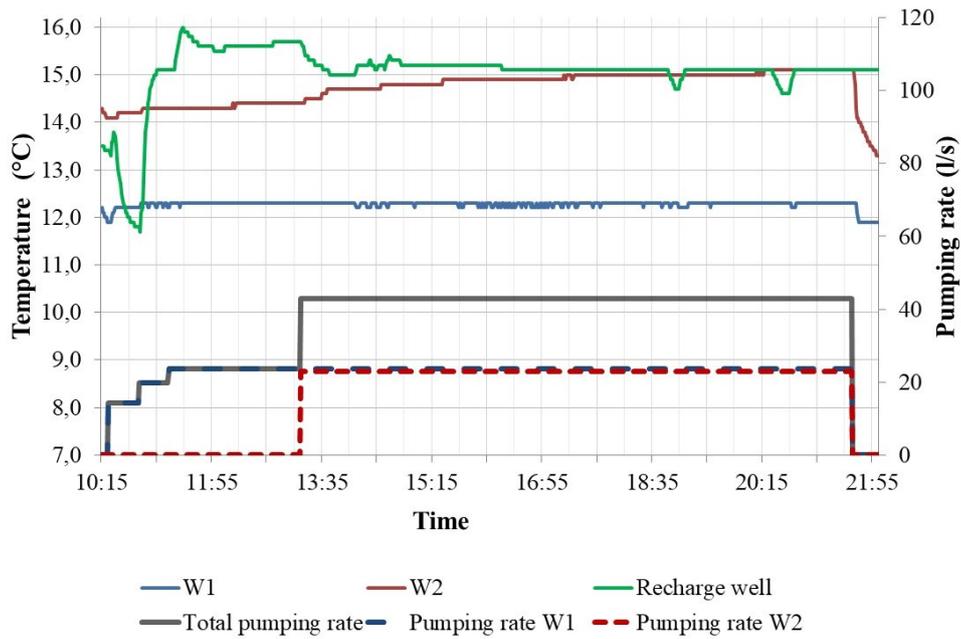
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 148 **Figure 6.** The influence of pumping on the surrounding terrain settlement.

149 3. Thermal Breakthrough

150 Water that returns into the ground through the recharge well disturbs the existing condition of
 151 the temperature field, and establishes a new, unsteady temperature field, i.e. causes the occurrence
 152 of temperature imbalance [16]. When the extraction well is influenced by the temperature imbalance,
 153 a change occurs in the temperature of the pumped water - this is called thermal breakthrough [17].

154 In the present case, a regular inspection of the heat pump system indicated flaws that
 155 significantly influenced its functionality. Besides technical flaws regarding system management, a
 156 problem was detected in extraction well W1. The temperature of the pumped water in wells W1 and
 157 W2 before heat pump operation was $\approx 12^{\circ}C$. The temperature of waters returning into the ground
 158 from the heat pump was $15-16^{\circ}C$, which led to a water temperature increase in well W1. In order to
 159 quantify the effect of the heat from the recharge well on water temperatures in W1 and W2, a pump
 160 test was conducted with a continual water temperature monitoring. The results of the pump test are
 161 shown on Figure 7. The total duration of the pump test was around 12 hours. The picture clearly
 162 indicates the effect of the recharge well water temperature on water temperature in well W2. Water
 163 temperature in W2 is in a constant increase from the start of pumping, and after 10 hours the
 164 temperature becomes equal to the water temperature in the recharge well, which is $15.3^{\circ}C$. During
 165 the pump test water temperature in W1 remained constant, i.e. no thermal breakthrough was
 166 detected.

167 All of the above facts led to a decrease in the efficiency of the heat pump, which caused an
 168 inability to cool the production hall into the temperature and humidity values intended by design.
 169 The cooling capacity of the system, i.e. the installed cooling power was decreased to 40-50% of the
 170 original, design values.



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Figure 7. Pump test results – the influence of recharge well on the water temperature in extraction well W2.

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The thermal breakthrough is a consequence of insufficient distance between well W2 and recharge well, for the given pump quantities and aquifer hydrogeological parameters. In the present case, the distance between wells was conditioned by building size and the arrangement of other objects built for hall function. Well W2 was constructed at 40 m from the recharge well, and W1 at 60 m. The thermal breakthrough can be resolved by constructing additional recharge wells at adequate distances, in order to reduce the load on the existing recharge well.

180 **5. Conclusions**

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The groundwater heat pump is an energy-efficient and environmentally friendly building heating and air-conditioning system. One of the major prerequisites effecting the functionality of such a system are the hydrogeological parameters of the aquifer. By analyzing their values an estimate can be given on the feasibility and the efficiency of the GWHP system for a specific case.

The northwest part of Croatia is rich in groundwater; along with favorable hydrogeological conditions, these facts comprise the large potential for GWHP system construction on a larger scale. Design based on quality data can ensure optimal exploitation of groundwater potential, as well as the prevention of possible unwanted side effects during exploitation. Investigative works, including pump tests and drilling, can determine the aquifer hydrogeological characteristics, as well as parameters required for the analysis of the effects of groundwater pumping on terrain settlement. During investigation works it is important to identify any changes in the geological structure of the soil, and special attention needs to be given to determining grain size and permeability. Design solutions, and consequently the final system efficiency, depend on the scope of investigation works. In order to prevent thermal breakthrough, recharge wells need to be planned at an adequate distance downstream of the extraction wells, taking into account the hydraulic gradient, hydraulic conductivity and other relevant parameters.

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Author Contributions: S.S. was in charge of geotechnical investigation works and pump test. F.D. prepared the draft of the paper and contributed to analyses and conclusion. K.G. and S.S: performed aquifer parameter analyses. B.M-K. commented results and provided theoretical background of the problem.

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Conflicts of Interest: The authors declare no conflict of interest.

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