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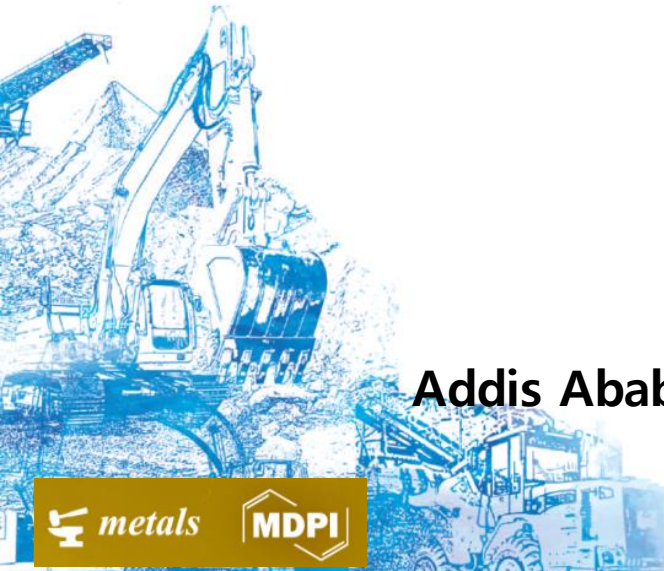


# Reliability Design Of Mechanical Systems Such as Compressor Subjected To Repetitive Stresses

2021. 02. 25

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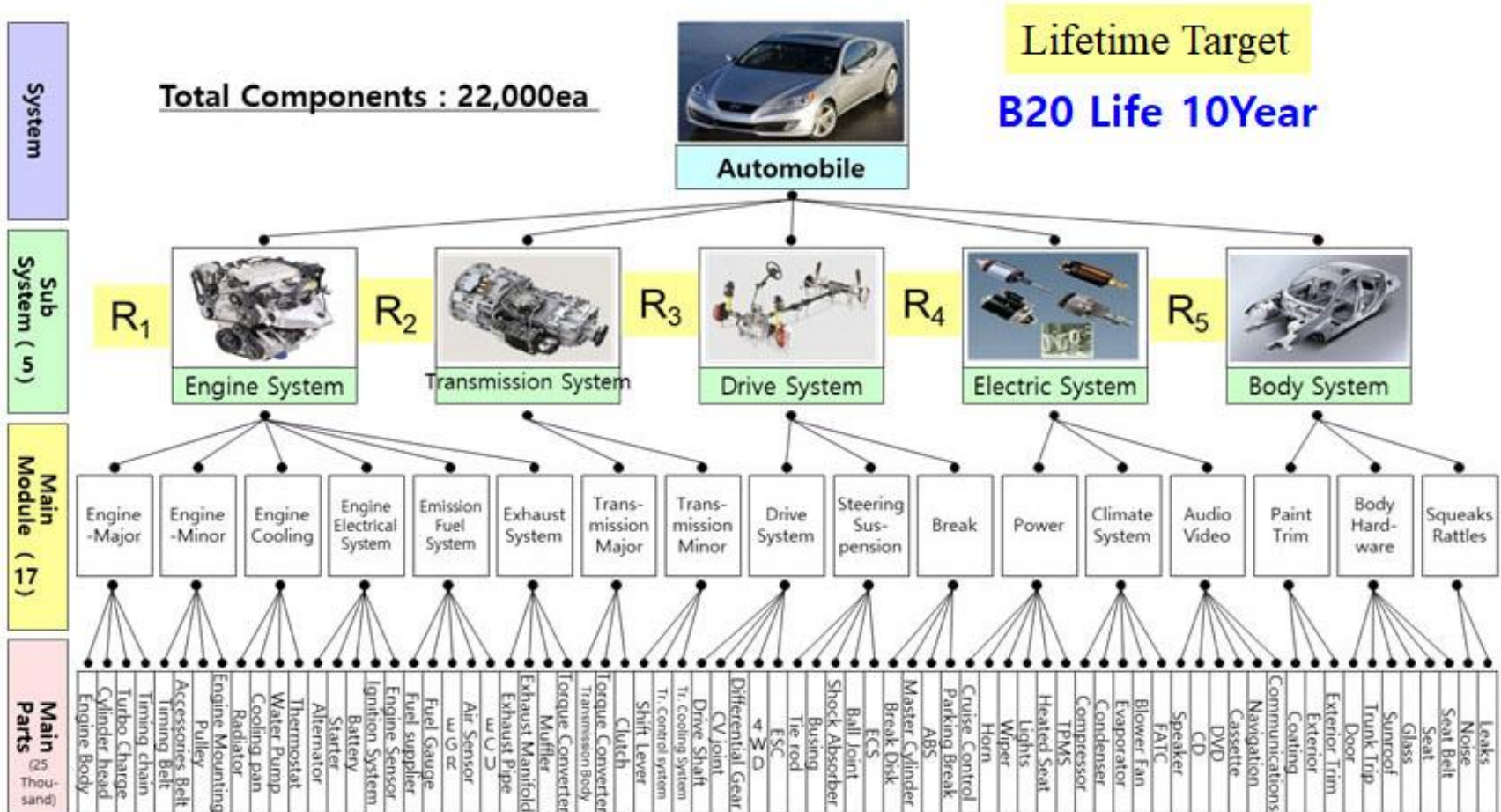
metals

MDPI



# Introduction

## □ Systems Engineering: Automobile

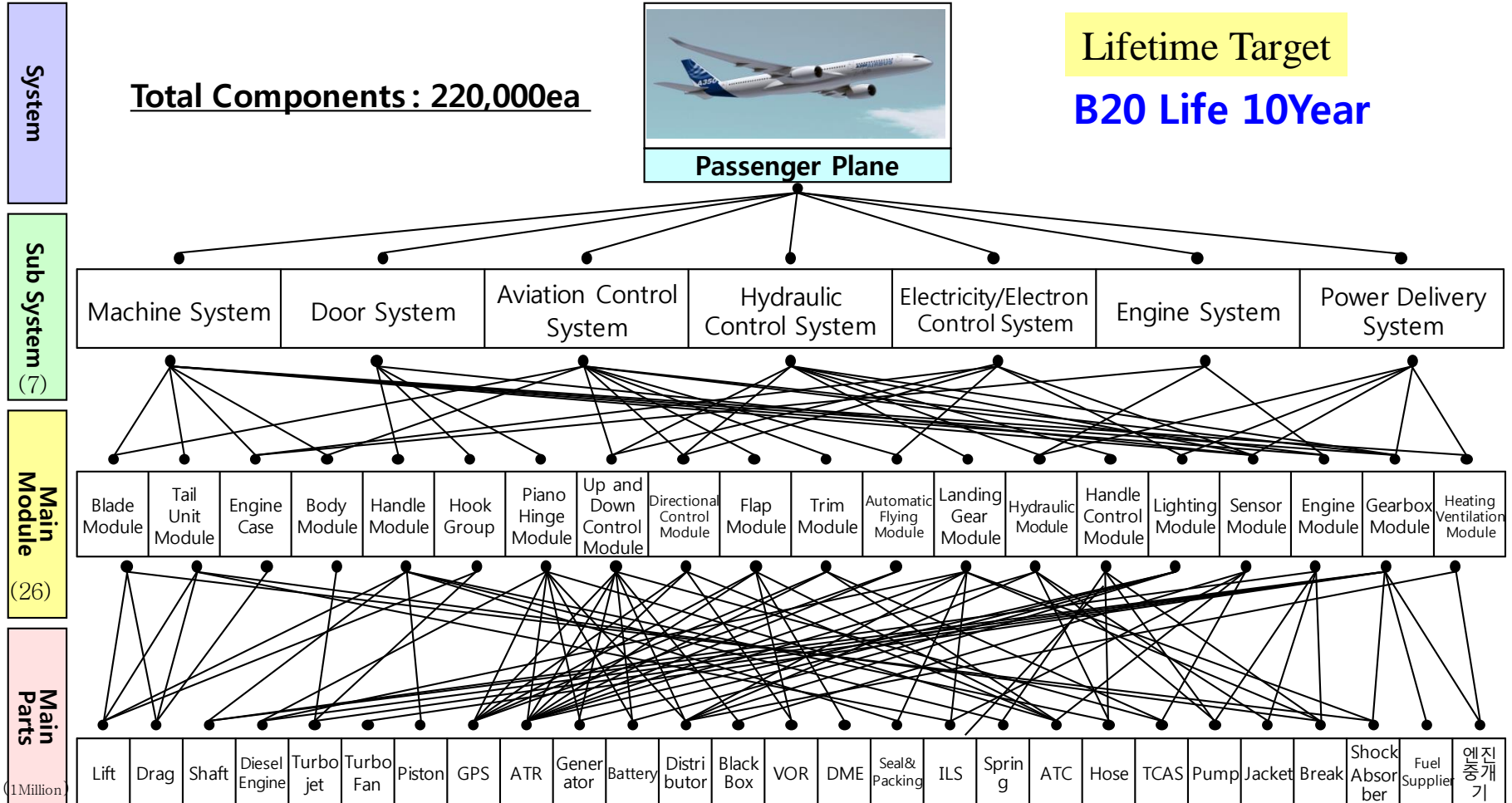


⇒ To improve performance or reducing cost, product will be designed yearly

⇒ By reliability testing, engineer should find the design flaws of product module

# Introduction

## □ Systems Engineering: Airplane



# Introduction

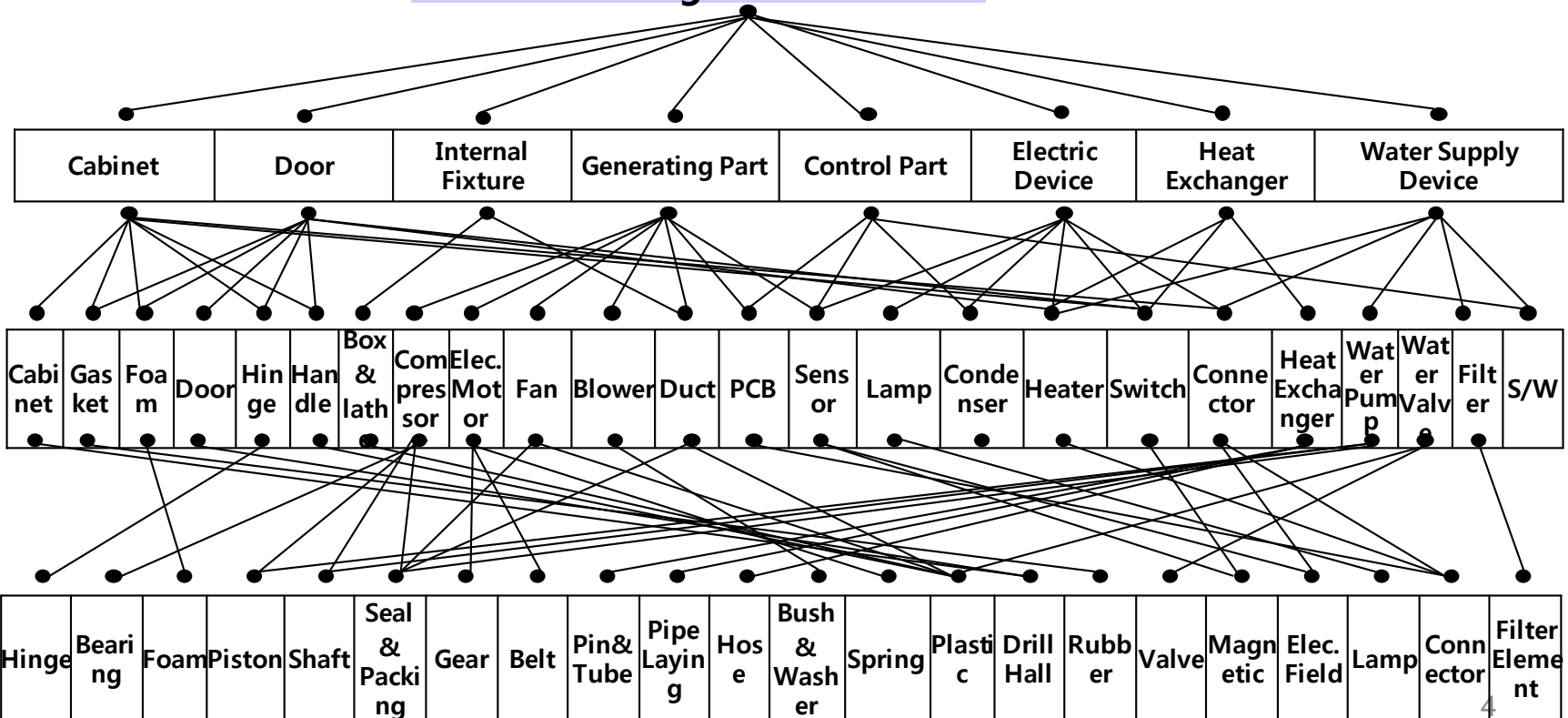
## □ Systems Engineering: Refrigerator

Total Components :  
2,200 pieces



Lifetime Target  
**B20 Life 10Year**

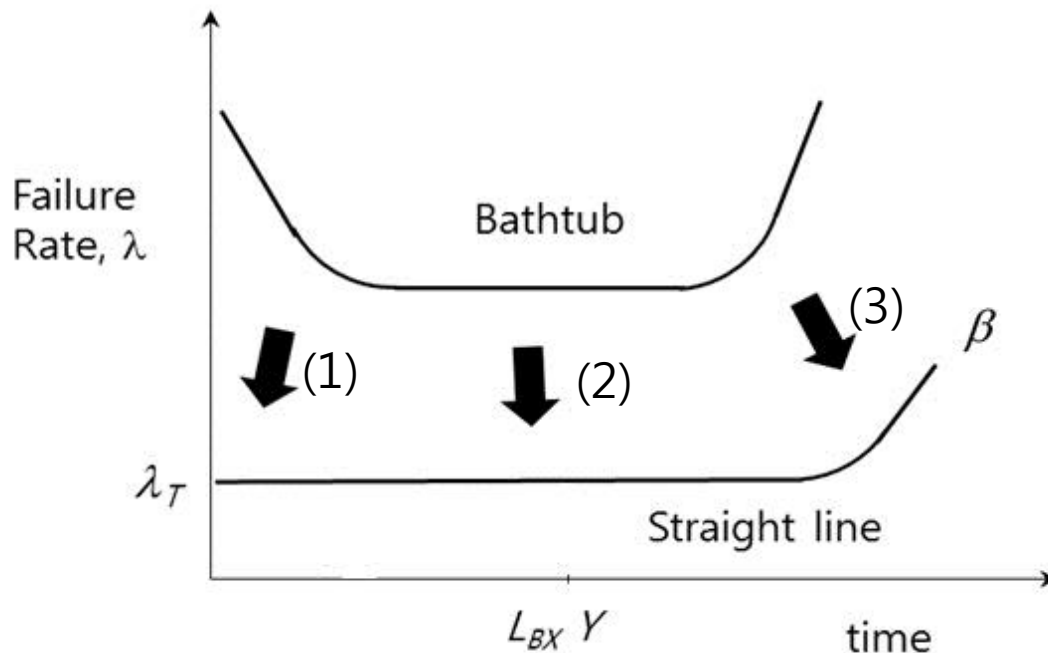
Refrigerator



# Introduction

## □ Definition of Reliability

**Ability** of an item to perform a required function under stated environmental and operational conditions for **a specified period of time**



**Bathtub Curve**

design  improvement

**Straight Line**

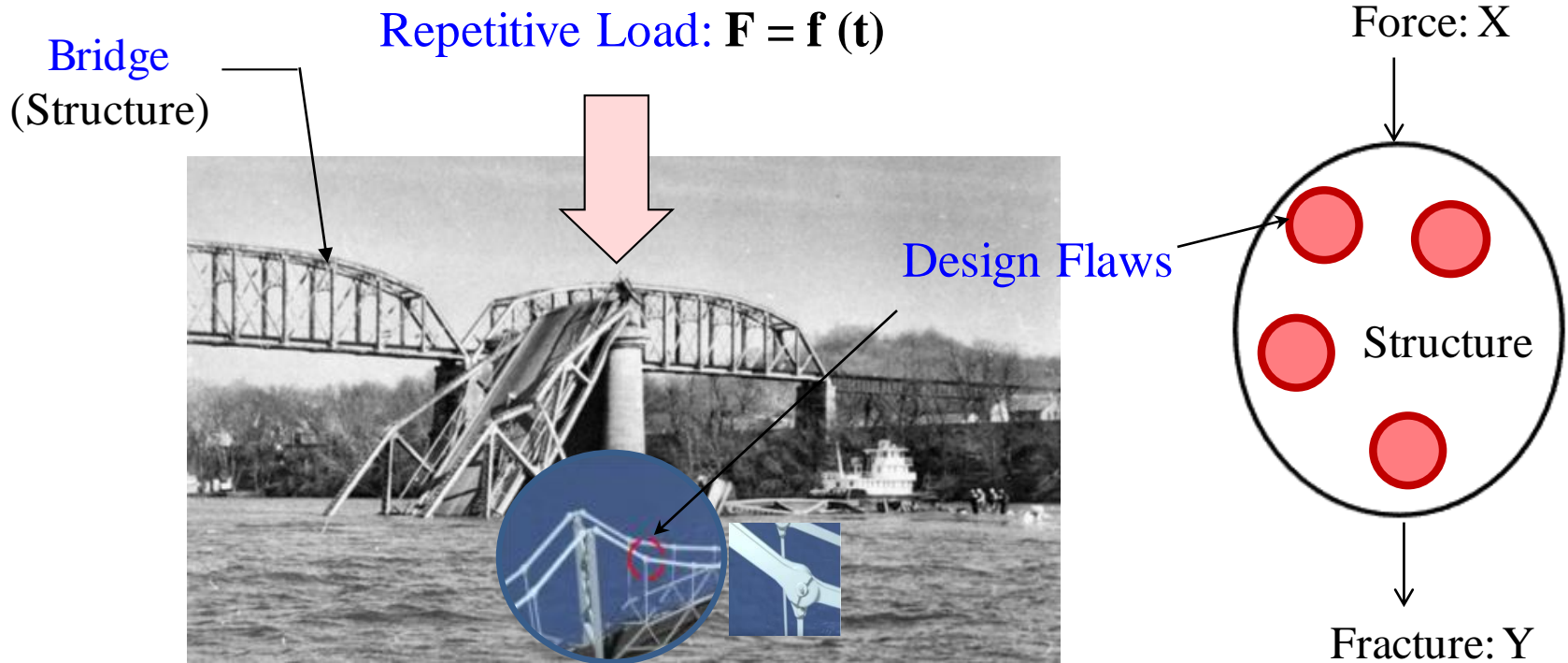
Product reliability:  $R(L_B) = 1 - F(L_B) = e^{-\lambda L_B} \cong 1 - \lambda L_B$



**Reliability can be achieved without design failures**

# Failure Mechanics and Design

## □ Failure mechanics and product designs (material/shape)



How to find the design flaws with rare probability (Poisson distribution)  
→ Solution: Reliability testing under accelerated life testing

# PARAMETRIC ACCELERATED LIFE TESTING

## ▪ Solid-state diffusion of impurities (void/hole) in silicon

- Electromigration-induced voiding / Build-up of chloride ions / Trapping of electrons or holes

$$J = [aC(x-a)] \cdot \exp\left[-\frac{q}{kT}\left[w - \frac{1}{2}a\xi\right]\right] \cdot \nu$$

[ Density / Area ] · [ Jump Probability ] · [ Jump Frequency ]

$$= -[a^2 \nu e^{-qw/kT}] \cosh \frac{qa\xi}{2kT} \frac{\partial C}{\partial x} + [2a \nu e^{-qw/kT}] C \sinh \frac{qa\xi}{2kT}$$

[ A.Grove, Physics and Technology of Semiconductor Device, p37 ]

$$\cong \Phi(x, t, T) \sinh(a\xi) \exp\left(-\frac{Q}{kT}\right)$$

$$= B \sinh(a\xi) \exp\left(-\frac{Q}{kT}\right)$$

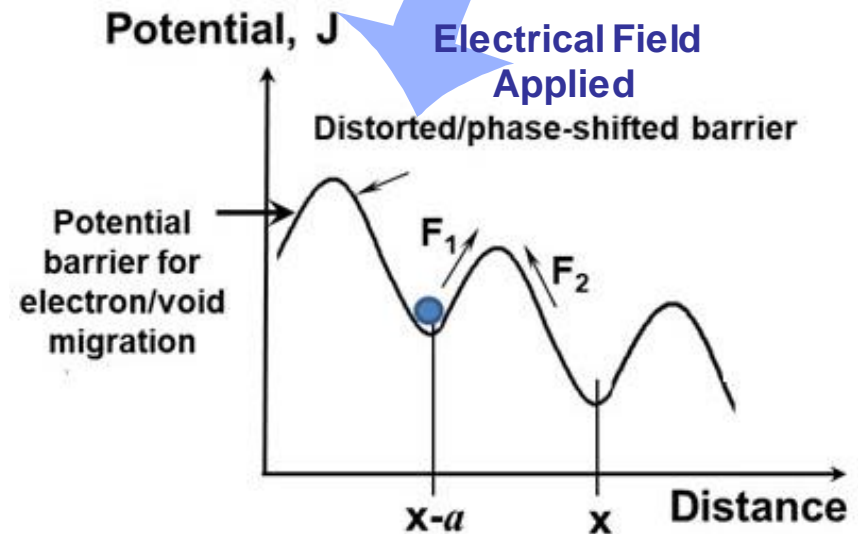
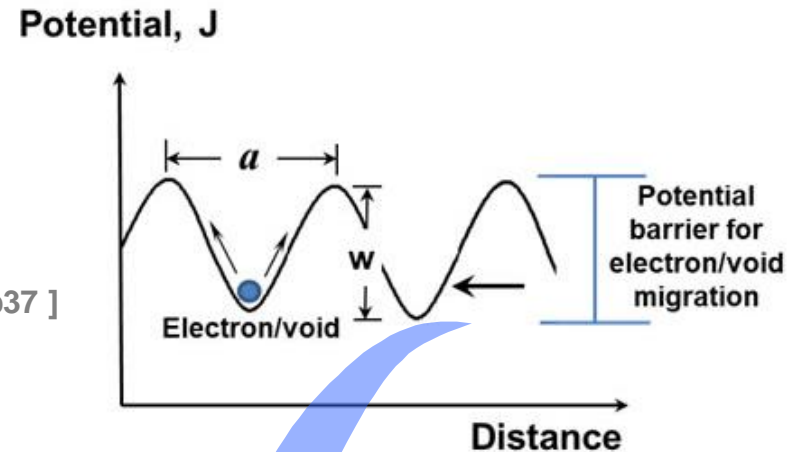
[ ASM, Electronic Materials HDBK, V1, p888 ]

## ▪ Chemical reaction dependent on speed

$$K = K^+ - K^- = a \frac{kT}{h} e^{-\frac{\Delta E - \alpha S}{kT}} - a \frac{kT}{h} e^{-\frac{\Delta E + \alpha S}{kT}} = 2 \frac{kT}{h} e^{-\frac{\Delta E}{kT}} \cdot \sinh\left(\frac{\alpha S}{kT}\right)$$

$$= B \sinh(\alpha S) \exp\left(-\frac{\Delta E}{kT}\right)$$

[ 鹽見, 故障物理入門, p79 ]



# PARAMETRIC ACCELERATED LIFE TESTING

## Acceleration Factor (AF)

### Junction energy in silicon

$$J = [aC(x-a)] \cdot \exp\left[-\frac{q}{kT}\left[w - \frac{1}{2}a\xi\right]\right] \cdot v$$

$$= B \sinh(a\xi) \exp\left(-\frac{Q}{kT}\right)$$



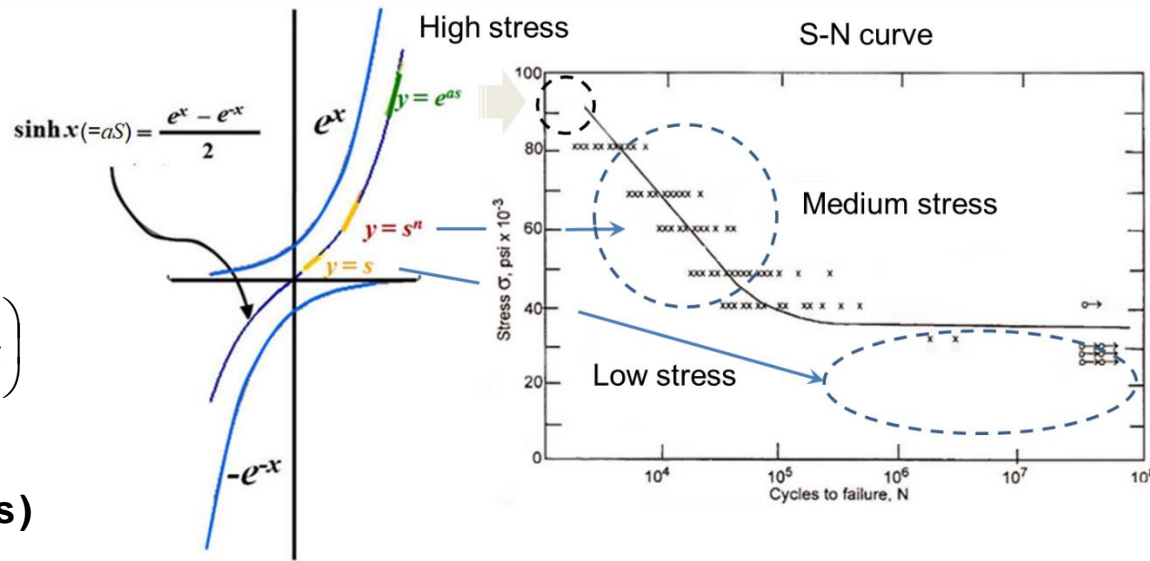
Inverse

### General stress model

$$TF = B[\sinh(aS)]^{-1} \exp\left(\frac{Q}{kT}\right)$$

- **Low Effect**,  $TF = C(S)^{-1} \exp\left(\frac{Q}{kT}\right)$
- **Medium Effect**,  $TF = A(S)^{-n} \exp\left(\frac{Q}{kT}\right)$
- **High Effect**,  $TF = D \exp(-aS) \exp\left(\frac{Q}{kT}\right)$
- **Acceleration Factor (Medium Stress)**

$$AF = \left(\frac{S}{S_o}\right)^n \exp\left[\frac{Q}{k}\left(\frac{1}{T_o} - \frac{1}{T}\right)\right]$$





# PARAMETRIC ACCELERATED LIFE TESTING

## □ Power in Multi-port System ( $P = e(t) \times f(t)$ )

: Power might be defined as the **product of effort and flow**

System Units (or Parts)	Effort, $e(t)$	Flow, $f(t)$
Mechanical translation	Force component, $F(t)$	Velocity component, $V(t)$
Mechanical rotation	Torque component, $\tau(t)$	Angular velocity, $\omega(t)$
Compressor	Pressure difference, $\Delta P(t)$	Volume flow rate, $Q(t)$
Electric	Voltage, $V(t)$	Current, $i(t)$

$$TF = A(S)^{-n} \exp\left(\frac{Q}{kT}\right) = A(e)^{-\lambda} \exp\left(\frac{Q}{kT}\right)$$

$$AF = \left(\frac{S_1}{S_0}\right)^n \left[ \frac{E_a}{k} \left( \frac{1}{T_0} - \frac{1}{T_1} \right) \right] = \left(\frac{e_1}{e_0}\right)^\lambda \left[ \frac{E_a}{k} \left( \frac{1}{T_0} - \frac{1}{T_1} \right) \right]$$

stress come from effort

# PARAMETRIC ACCELERATED LIFE TESTING

## ➤ Sample Size Equation

If product follows Weibull distribution, reliability function is defined as:

$$R(t) = 1 - x = e^{-\left(\frac{t}{\eta}\right)^\beta} \longleftrightarrow L_{BX}^\beta = \left(\ln \frac{1}{1-x}\right) \cdot \eta^\beta$$

logarithm

Characteristic life  $\eta_\alpha$  for the confidence level  $100(1 - \alpha)$ :

$$\eta_\alpha^\beta = \frac{2r}{\chi_\alpha^2(2r+2)} \cdot \eta_{MLE}^\beta = \frac{2}{\chi_\alpha^2(2r+2)} \cdot \sum_{i=1}^n t_i^\beta$$

Testing data

where  $\eta_{MLE}$  from the Maximum Likelihood Estimation  $\eta_{MLE}^\beta = \sum_{i=1}^n \frac{t_i^\beta}{r}$

Assessed  
BX Life:

$$L_{BX}^\beta = \frac{2}{\chi_\alpha^2(2r+2)} \cdot \left(\ln \frac{1}{1-x}\right) \cdot \sum_{i=1}^n t_i^\beta$$

# PARAMETRIC ACCELERATED LIFE TESTING

## ➤ Sample Size Equation from approximation of BX life

$$\text{BX life: } L_{BX}^\beta = \frac{2}{\chi_\alpha^2(2r+2)} \cdot \left( \ln \frac{1}{1-x} \right) \cdot \sum_{i=1}^n t_i^\beta \geq \frac{2}{\chi_\alpha^2(2r+2)} \cdot \left( \ln \frac{1}{1-x} \right) \cdot (n-r) \cdot h^\beta$$

1) Chi-square Approx.:  
For C.L.=60% and  $r < 4$

2) Logarithmic Approx.:  
Cumulative Failure  $x \leq 20\%$

$r$	$\frac{\chi_\alpha^2(2r+2)}{2(a)}$	$1-\alpha$
0	<b>1</b>	0.63
1	<b>2</b>	0.59
2	<b>3</b>	0.58
3	<b>4</b>	0.57

$$* \frac{\chi_\alpha^2(2r+2)}{2} = (r+1)$$

$$L_{BX}^\beta = \frac{1}{(r+1)} \cdot x \cdot n \cdot h^\beta$$

Rearrange

Sample Size Equation:

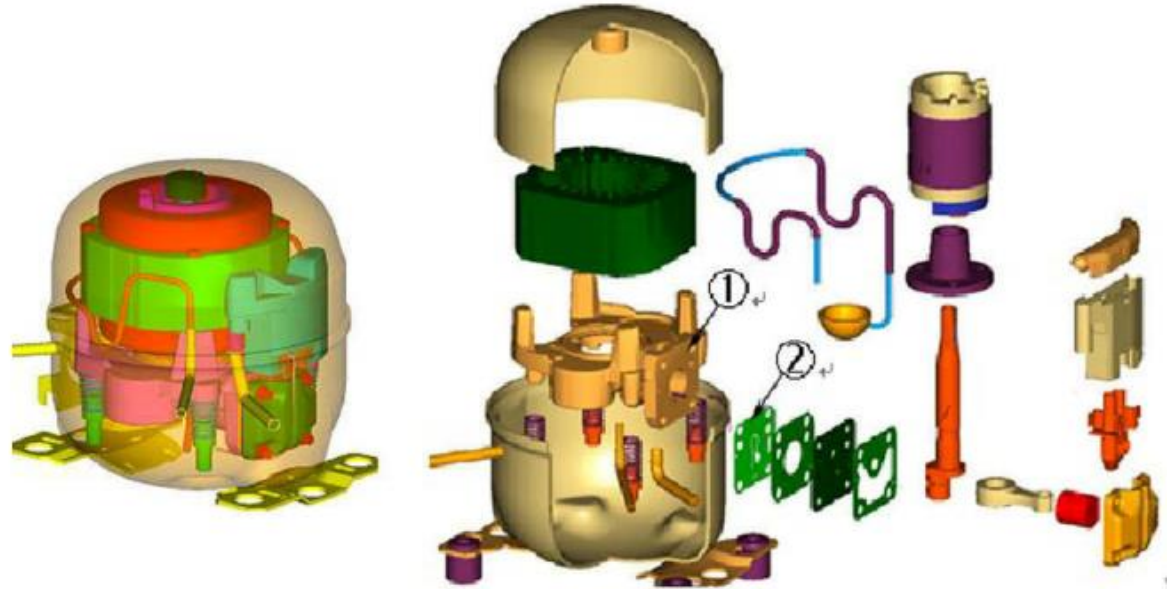
$$n \geq (r+1) \cdot \frac{1}{x} \cdot \left( \frac{L_{BX}}{AF \cdot h_a} \right)^\beta + r$$

# Case Study: Domestic Compressor

## ➤ Refrigerator and redesigned compressor



Refrigerator



Compressor System

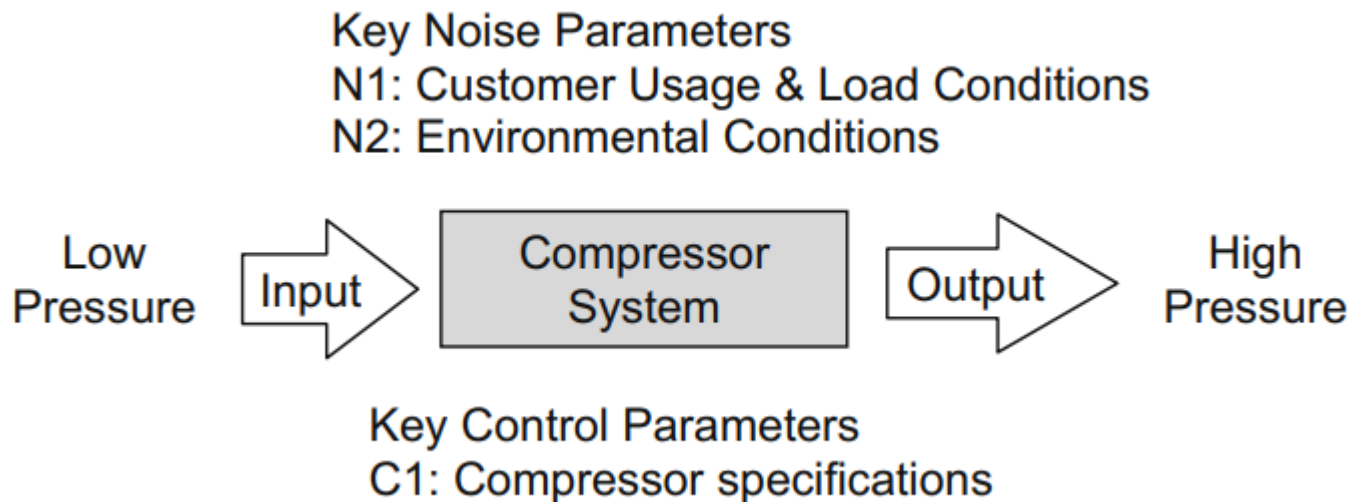
There are design faults in compressor, but we don't know which parts are

⇒ Compressor lifetime depends on the **design faults of parts**

⇒ To finding them, it require new reliability methodology

# Case Study: Domestic Compressor

## ➤ Parametric design schematics



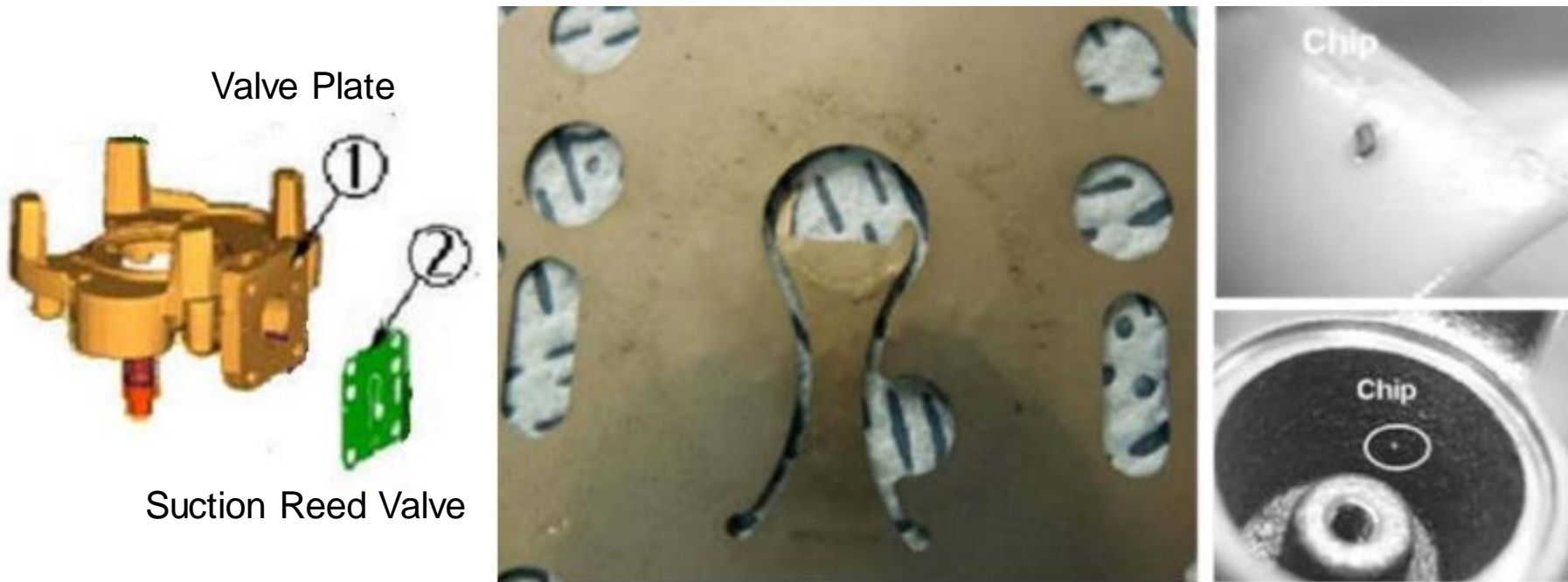
⇒ Reliability methodology: 1) failure analysis for returned product

⇒ 2) Parametric ALT and its design modification

⇒ 3) Finally, checking if the lifetime target is achieved

# Case Study: Domestic Compressor

## ➤ Damaged products in field



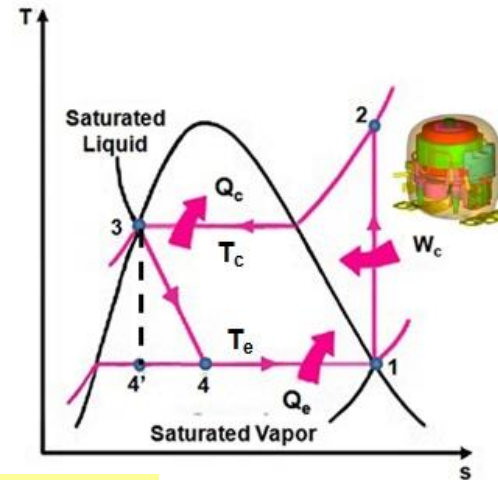
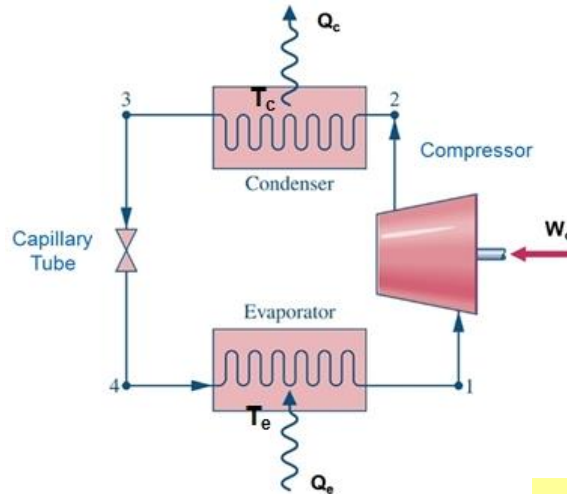
**There were a lot of cracks on compressor part**

⇒ It came from fragile structure (design flaws)

⇒ By reproducing by parametric ALT, we can correct them

# Case Study: Domestic Compressor

## ➤ Load Analysis for Accelerated Testing



Conservation of mass in capillary

$$\dot{m} = \dot{m}_{\text{cap}}$$

Energy balance in the condenser

$$Q_c = \dot{m}(h_2 - h_3) = (T_c - T_o) / R_c \Rightarrow T_e$$

Energy balance in the evaporator

$$Q_e = \dot{m}(h_1 - h_4) = (T_i - T_e) / R_e \Rightarrow T_c$$

Determine

$\dot{m}$

$T_e$

$T_c$

Time to Failure

$$TF = A(S)^{-n} \exp\left(\frac{E_a}{kT}\right) = A(\Delta P)^{-\lambda} \exp\left(\frac{E_a}{kT}\right)$$

where

$$\Delta P = P_{\text{dis}} - P_{\text{suc}} \cong P_c - P_e \quad \text{and}$$

$$P_e = f(T_e) \text{ or } P_c = f(T_c)$$

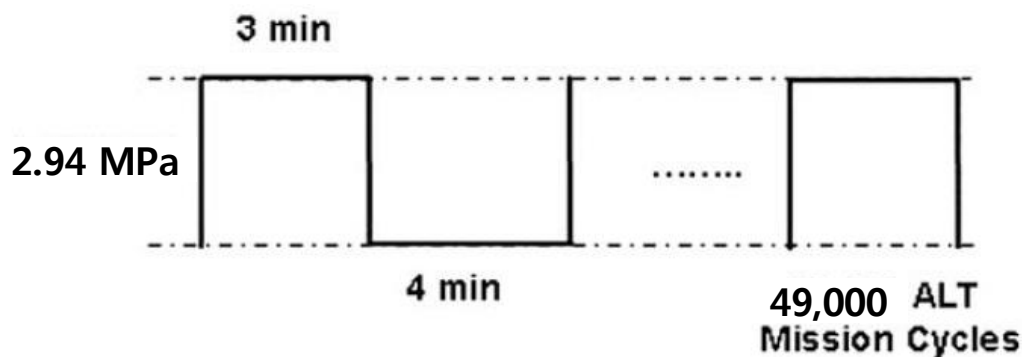
# Case Study: Domestic Compressor

## ➤ Accelerated Factor

$$AF = \left(\frac{S_1}{S_0}\right)^n \left[ \frac{E_a}{k} \left( \frac{1}{T_0} - \frac{1}{T_1} \right) \right] = \left(\frac{\Delta P_1}{\Delta P_0}\right)^\lambda \left[ \frac{E_a}{k} \left( \frac{1}{T_0} - \frac{1}{T_1} \right) \right]$$

System Conditions		Worst Case	ALT	AF ( $\lambda=2$ )
Pressure (MPa)	High-side	1.27	2.94	<b>5.36</b> ①
	Low-side	0.0	0.0	
	$\Delta P$	1.27	2.94	
Temperature (°C)	Dome	90	120	<b>1.37</b> ②
Total AF (=①×②)				<b>7.32</b>

## ➤ By applying duty cycle F on compressor



⇒ Search out the design failure



# Case Study: Domestic Compressor

## ➤ Calculation of the mission cycle, $h_a$

Lifetime target of domestic compressor: **B<sub>1</sub> life 10 years**

$$n \geq (r + 1) \cdot \frac{1}{x} \cdot \left( \frac{L_{BX}^*}{AF \cdot h_a} \right)^\beta + r$$

(1)  $x = 0.01$  (B1 life)  
(2)  $r = 0$  (No Failure)  
(3)  $AF = 7.32$

Total sample size of domestic compressor:  $n=100$

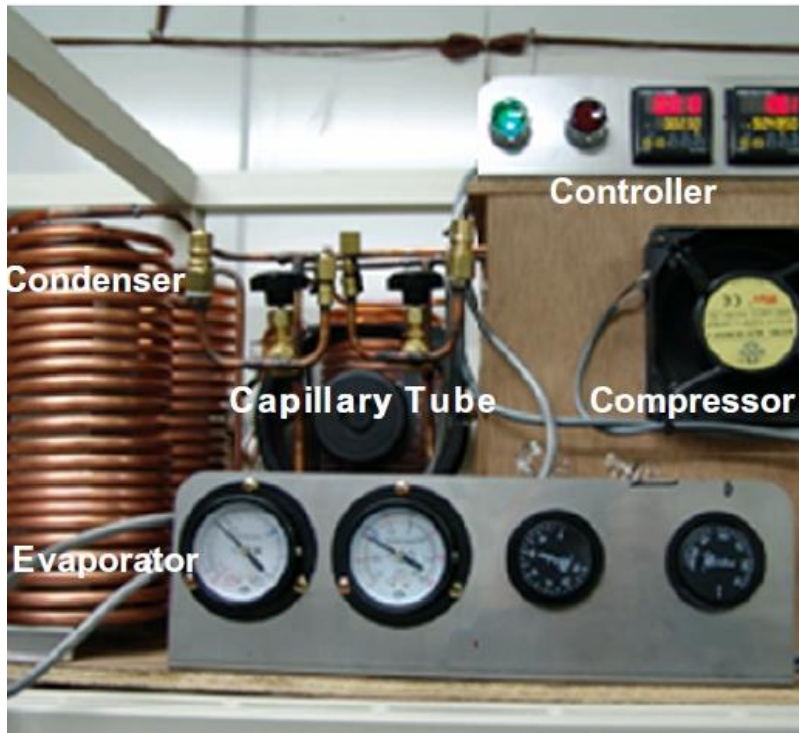
Compressor Lifetime:  $98 \text{ cycles/day} \times 365 \text{ day/year} \times 10 \text{ years} = 357,6700 \text{ cycles}$

⇒ Specification( $h_a$ ): if there is no problem in **49,000 cycles**,

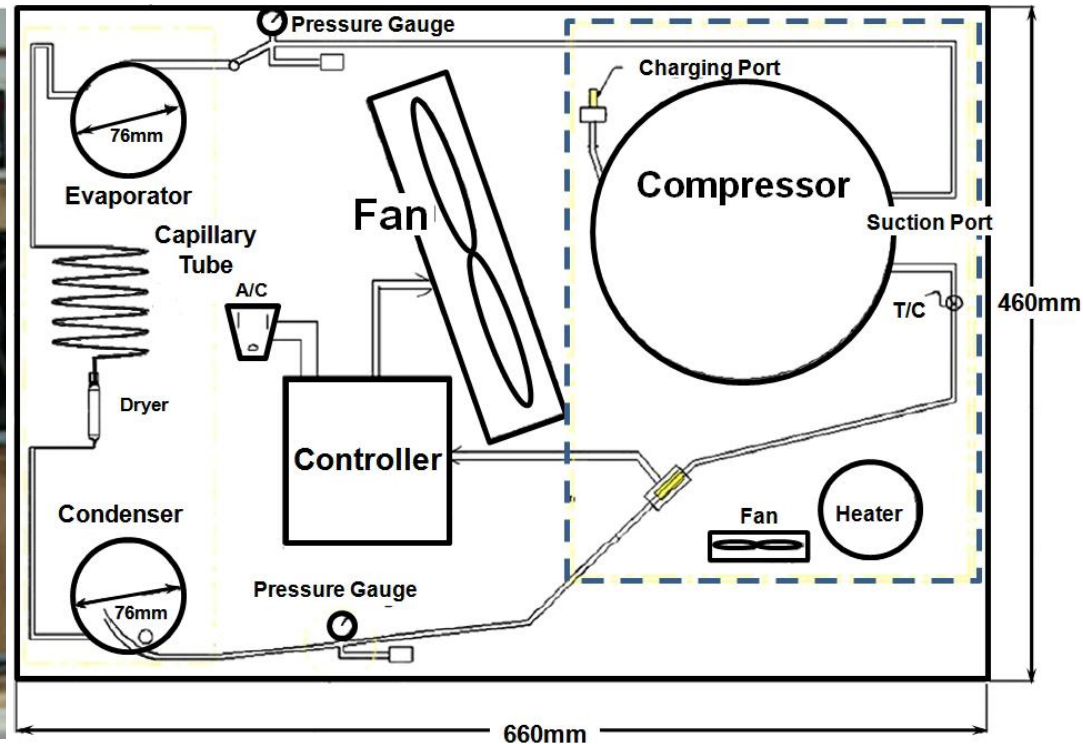
⇒ We can guarantee compressor lifetime target: **B1 life 10 years**

# Case Study: Domestic Compressor

## ➤ Equipments used in accelerated life testing



Testing Zig



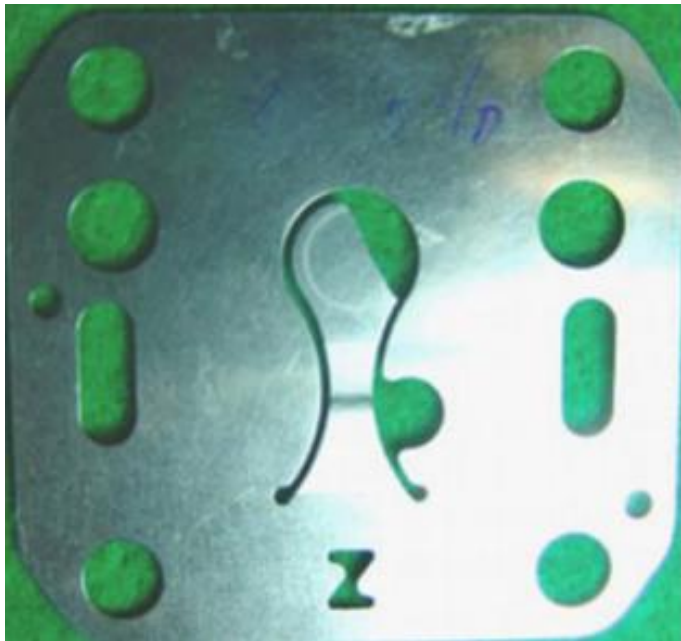
Schematic Diagram

⇒ We can proceed the parametric ALT with equipment

# Case Study: Domestic Compressor

## ➤ Results of 1<sup>st</sup> ALT

: Compressor locked due to the fractured suction reed valve at 10,500 cycles



Field



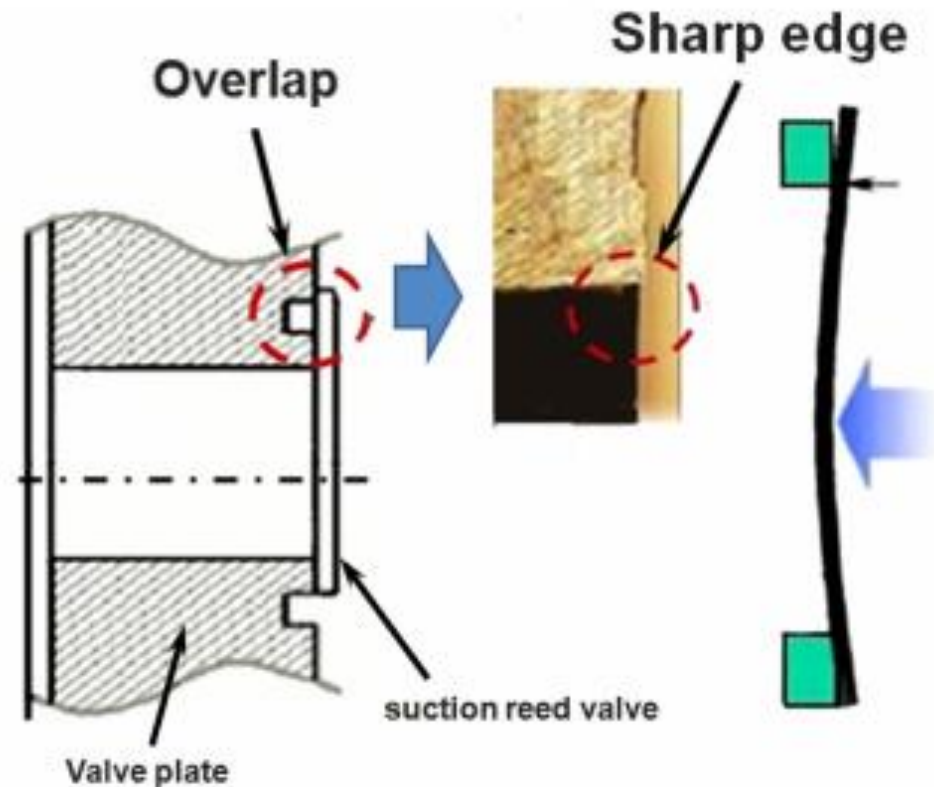
1<sup>st</sup> ALT

By parametric ALT, we could reproduce the compressor failure in field

# Case Study: Domestic Compressor

## ➤ Results of 1<sup>st</sup> ALT


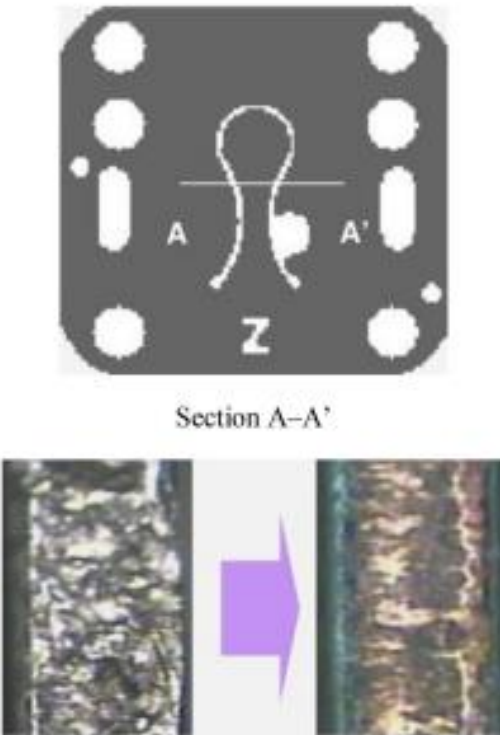
Fractured suction reed valve



**Root causes: a) Overlapped suction reed valve b) valve plate with sharp edge**

# Case Study: Domestic Compressor

- Redesigned valve plate and suction reed valve

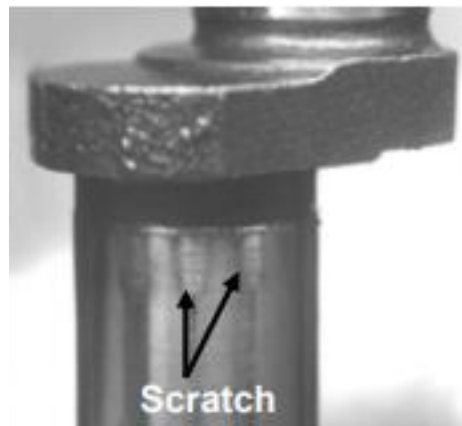
Valve plate	Suction reed valve
 <p>The image shows the redesign of a valve plate. On the left, a photograph of the valve plate has a central hole labeled 'Trespan'. To its right, a diagram shows a cross-section of the hole before and after a blue arrow indicating an increase in diameter. Below this, a photograph shows a ball peen tool being used on a metal surface, with a circular inset labeled 'Ball Peen' showing the resulting surface texture.</p>	 <p>The image shows the redesign of a suction reed valve. At the top, a photograph of the valve plate has a central reed valve assembly with a horizontal line labeled 'A' and 'A'' and a vertical line labeled 'Z'. Below this, the text 'Section A-A'' is centered. At the bottom, two photographs show the surface texture of the valve plate before and after a tumbling process, with a purple arrow pointing from the left image to the right image.</p>
C1: Trepan: 0.73 mm → 1.25 mm	C3: 0.178t → 0.203t (SANDVIK 20C thickness)
C2: Ball peening and brush process	C4: Tumbling process time: 4 h → 14 h

# Case Study: Domestic Compressor

## ➤ Results of 2<sup>nd</sup> ALT

: Compressor locked at 17,000 cycles .

Root cause  
: Crankshaft  
material



Redesigned crankshaft

Old Design

FCD500 + No Heat Treatment



New Design

FCD500 + Heat Treatment

By parametric ALT, we can modify the problematic crankshaft in compressor

# Case Study: Domestic Compressor

## ➤ Summary of Parametric ALT Results

Parametric ALT	1st ALT	2nd ALT	3rd ALT
	Initial Design	Second Design	Last Design
In 49,000 cycles, there are no problems in the compressor	10,500 cycles: 1/100 locking	17,000 Cycles: 3/100 locking	49,000 cycles: 100/100 OK

Structure



Action plans

C1: Trepan size: 0.73  
mm→1.25 mm

C2: Adding ball peening  
and brush process

C3: SANDVIK 20C:  
0.178t→0.203t

C4: Extending tumbling:  
4 h→14 h

C5: FCD500 + No Heat Treatment

→ FCD500 + Heat Treatment on  
the crank shaft

- Because there is no problem to 49,000 cycles,
- Compressor achieves the lifetime target – B1 life 10 years

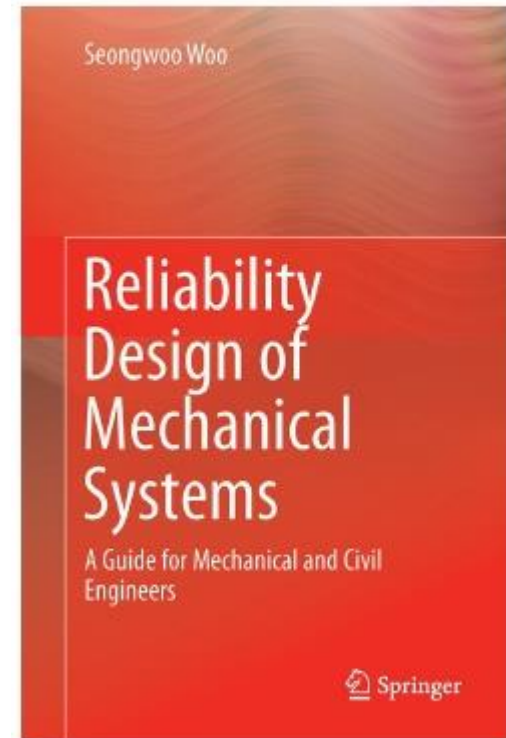
# Conclusion

S. Woo

## Reliability Design of Mechanical Systems

A Guide for Mechanical and Civil Engineers

- ▶ It enables mechanical and civil engineers to find the designs flaws and achieve the targeted product reliability. It also suggests a variety of case studies on the mechanical system. Presents Taguchi method's alternative experimental Methodology. Describes new parametric ALT methods for reliability quantitative test specifications (RQ).



1st ed. 2017, XII, 310 p. 249 illus., 132 illus. in color.



Thank You!

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